LTS & Hybrid Roadmap Outlook

PAUL SCHERRER INSTITUT







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Stress-Managed Asymmetric Common-Coils (SMACC) Conceptual Design

3rd Joint Common-Coils Meeting

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In respect to a standard common-coils magnet, we would like to propose improvements on how to:

- deal with high Lorentz forces
- simplify the common-coils architecture for accelerator magnets allowing a full common coils architecture and reacting & winding





Let's consider two typical common-coils turns distribution, with racetracks on the top and bottom of apertures for field quality correction (a and b). C shows a third design without racetracks / clover-leaf coils, with an additional common-coil on the hard-way bend direction.

y, [mm] y, [mm] x, [mm] x, [mm]

a: racetracks / clover-leaf coils and wide blocks b: racetracks / clover-leaf coils and thin blocks

c: only common-coils and thin blocks



Stress-management with spars, but high vertical load

Stress-management with spars and ribs

Asymmetric design D. M. Araujo Page 4



We can further simply option C, by having only easy-way bend common-coils Layers 1 and 2 with 21 x 1.1 mm RRP[®] strand cu/noCu 0.9 and layers 3 to 6 with 18 x 1.0 mm RRP[®] strand cu/noCu 1.3 for protection purpose.



b3 & a2 compensation



Magnet Parameters

Ribs and spar thickness were optimized for mechanics and to have the same margin in layers 1, 2 and 3. Field quality is < 15 units spread between injection and 14 T (10% margin at 4.2 K) nominal field operation and < 15 units at nominal (to be further optimized after the final cable definition).





The asymmetric common-coils magnet was designed with a intra-beam distance of 300 mm, 50 mm bore, yoke diameter of 740 mm and 30 mm thick stainless steel shell.

The magnet has 4 different types of coils (layer 1, layer 2, layer 3,4 and layer 5,6) and 12 coils in total (for a double aperture magnet). The coils are placed in the stress-management formers. The preload is transferred towards the inner-most layers through the ribs.

The massive **iron pole**, combined with the asymmetric concept, helps on the balance vertical force balance.

The load, due to Lorentz forces, is distributed between pads and shell, which limits the thickness of the shell.

The magnet concept is based on bladder & keys technology for room temperature preload. The structure is loaded, but thanks to the stress-management formers, the coil stress after loading and after cooling is < 40 MPa.









Pre-load with 0.5 mm interference on the keys. Low stress on coils: 37 MPa 424 MPa (compression) on the pads



ANSYS 2021 R1 Build 21.1 NODAL SOLUTION STEP=1 SUB =1 TIME=1 SEQV (AVG) **PowerGraphics** EFACET=1 AVRES=Mat DMX =.552E-04 SMN =71189.2 SMX =.368E+08 71189.2 .415E+07 .823E+07 .123E+08 .164E+08 .205E+08 .245E+08 .286E+08 .327E+08 .368E+08





Technology

Pre-load with 0.5 mm interference on the keys and cooling-down. Low stress on coils: 37 MPa

647 MPa (compression) on the pads

Von-Mises



ANSYS 2021 R1 Build 21.1 NODAL SOLUTION STEP=2 SUB =1 TIME=2 SEQV (AVG) **PowerGraphics** EFACET=1 AVRES=Mat DMX =.603E-03 SMN =4687.66 SMX =.365E+08 4687.66 .406E+07 .812E+07 .122E+08 .162E+08 .203E+08 .244E+08 .284E+08 .325E+08 .365E+08





Pre-load with 0.5 mm interference on the keys and cooling-down. Stress on iron: **487 MPa in one node,** other else < 200 MPa



ANSYS 2021 R1 Build 21.1 NODAL SOLUTION STEP=2 SUB =1 TIME=2 SEQV (AVG) PowerGraphics EFACET=1 AVRES=Mat DMX =.919E-03 SMN =836.328 SMX = .487E+09 836.328 .541E+08 .108E+09 .162E+09 .216E+09 .270E+09 .325E+09 .379E+09 .433E+09 .487E+09

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ANSYS 2021 R1 Build 21.1 NODAL SOLUTION STEP=2 SUB =1 TIME=2 S1 (AVG) **PowerGraphics** EFACET=1 AVRES=Mat DMX =.919E-03 SMX =.109E+09 0 .121E+08 .242E+08 .362E+08 .483E+08 .604E+08 .725E+08 .846E+08 .966E+08 .109E+09

Cool-down

Maximum principal stress



14 T operation (10% margin at 4.2 K) Stress on coils: **128 MPa on corners,** other else < 100 MPa

15.1 T operation (10% margin at 1.9 K)Stress on coils: 143 MPa on corners, other else< 110 MPa





ANSYS 2021 R1 Build 21.1 NODAL SOLUTION STEP=3 SUB =1 TIME=3 SEQV (AVG) **PowerGraphics** EFACET=1 AVRES=Mat DMX =.648E-03 SMN =492913 SMX = 128F+09492913 146E+08 .288E+08 .429E+08 .570E+08 712E+08 .853E+08 994E+08 .114E+09 .128E+09 D. M. Araujo



14 T operation (10% margin at 4.2 K) Stress on coils: **128 MPa on corners,** other else < 100 MPa < 30% engineering margin on the peak of stress regions.



Von-Mises



ANSYS 2021 R1 Build 21.1 NODAL SOLUTION STEP=3 SUB =1 TIME=3 SEQV (AVG) PowerGraphics EFACET=1 AVRES=Mat DMX =.648E-03 SMN =492913 SMX =.128E+09 492913 .146E+08 .288E+08 .429E+08 .570E+08 .712E+08 .853E+08 994E+08 .114E+09 .128E+09 D. M. Araujo





15.1 T operation Peak of **692 MPa** on the formers Stress on iron: **526 MPa in one node,** other else < 350 MPa

Von-Mises



ANSYS 2021 R1 Build 21.1 NODAL SOLUTION STEP=3 SUB =1 TIME=3 SEQV (AVG) **PowerGraphics** EFACET=1 AVRES=Mat DMX =.001104 SMN =.724E-07 SMX =.692E+09 .724E-07 .769E+08 .154E+09 .231E+09 .307E+09 .384E+09 .461E+09 .538E+09 .615E+09 .692E+09





ANSYS 2021 R1 Build 21.1

STEP=3 SUB =1 TIME=3

S1

NODAL SOLUTION

(AVG)

PowerGraphics EFACET=1 AVRES=Mat DMX =.001061

SMX =.257E+09

.285E+08 .570E+08 .855E+08

.114E+09 .143E+09 .171E+09 .200E+09 .228E+09

.257E+09



Summary

Introduction of

- ... Stress-Managed Common-Coils Concept
- ... Asymmetric Common-Coils Concept

Possible advantages are

 Lower margin operation due to the low stress on high-field regions
Pure common-coils (no need for racetrack / clover-leaf/... correctors)
Possibility of implementing Reaction & Winding technique

