SIS100 impact

< □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > <

# SIS100 Dipole Magnets Field Measurements and Representation

#### Pierre Schnizer<sup>1</sup>, Bernhard Schnizer<sup>2</sup>, Egbert Fischer<sup>1</sup>, Anna Mierau <sup>1</sup>

<sup>1</sup>Gesellschaft für Schwerionenforschung Planckstraße 1, D-64291 Darmstadt <sup>2</sup>Institut für Theoretische Physik Technische Universität Graz Petersgasse 16, A-8010 Graz

Beam Dynamics meets Magnets II 1 – 4 December 2014 @ PSI

2

Theory 0000000000000 SIS100 impact

Conclusion

▲□▶ ▲圖▶ ▲臣▶ ▲臣▶ ―臣 … のへで

#### Outline



Theory
Coordinate systems
Toroidal multipoles

3 SIS100 impact



SIS100 impact

< □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > <

### Where to find

- Theory overview: "Cylindrical Circular and Elliptical, Toroidal Circular and Elliptical Multipoles Fields, Potentials and their Measurement for Accelerator Magnets", Pierre Schnizer, Egbert Fischer, Bernhard Schnizer, arXiv:1410.8090, submitted to PR STAB.
- "Theory and application of plane elliptic multipoles for static magnetic fields" Pierre Schnizer, Bernhard Schnizer, Egbert Fischer, Pavel Akishin, NIMA, vol 607, 2009, p 505-516

SIS100 impact

< □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > <

#### Acknowledgement

- The results presented today were achieved within a short time scale.
- This is to thank all people for their dedication: Alexander Bleile, Peter Borisch, Holger Brand, Antonio Coronato, Isabel deCaluwe, Eric Floch, Walter Freisleben, Anke Gottsmann, Florian Henkel, Franz Klos, Thomas Knapp, Kerstin Knappmeier, Boris Korber, Henning Kummerfeldt, Thomas Mack, Ron Mandel, Sven Meyer, Vassili Maroussov, Fahrid Marzouki, Thorsten Miertsch, Henning Raach, Christian Roux, Claus Schroeder, Gerd Schulz, Andrzej Stafiniak, Kei Sugita, Piotr Szwangruber, Vasileios Velonas, Detlef Theuerkauf, Franz Walter, Mischa Weipert, Harald Weiss, Horst Welcker
- together with the ones not even mentioned!

SIS100 impact

イロト イ理ト イヨト イヨト

æ

Conclusion



SIS100 impact

Conclusion

▲ロト ▲帰ト ▲ヨト ▲ヨト 三日 - の々ぐ

### Achieved Results

- Starting from fall last year:
  - test station upgrade
    - $\bullet\,$  upgrade of the power converter (22 V / 20 kA)
    - HTS current leads (tested up to 15.7 kA)
    - overlapping coil probe measurement  $\rightarrow$  analysis software developed
  - SIS100 FoS dipole magnet development:
    - high current coil
    - isotropic low loss iron yoke
    - shimming inserts

SIS100 impact

Conclusion

#### Magnet Power Test



◆□ > ◆□ > ◆豆 > ◆豆 > ̄豆 \_ のへぐ

Theory 000000000000000 SIS100 impact

Conclusion

◆□▶ ◆□▶ ◆三▶ ◆三▶ 三三 のへぐ

#### Minimum Cycle test

- 1.1 seconds reached → machine operation cycle
- minimum cycle  $\rightarrow$  to be determined

Theory 00000000000000 SIS100 impact

Conclusion

#### AC Loss test



- loss considerably lower: 50 W measured ↔ 70 W expected
- reduces load on cryoplant (otherwise @ limit)

(日)、

э

Introduction 0000●

Theory 000000000000 SIS100 impact

Conclusion

◆□▶ ◆□▶ ◆臣▶ ◆臣▶ 臣 のへぐ

### SIS100 FOS Magnet: Site Acceptance test

	specified	tested	
current $I_{max}$ (DC) $(dI/dt)_{max}$	13.1 kA 26.2 kA/s	15.7 kA 27 kA/s	$I_{max} = 14$ kA
AC Loss triangular cycle shortest op. cycle	70 W 1.1 s	50 W 1.1 s	

SIS100 impact

Conclusion

◆□▶ ◆□▶ ◆三▶ ◆三▶ 三三 のへぐ

### 4 Coordinate systems: The systems

Cylindric circular Cylindric ellliptic	standard approach field description using elliptic coordinates		
Toroidal circular	solved by R-separation: trans- formation of differential equa- tion		
Toroidal ellliptic	solved by R-separation: trans- formation of differential equa- tion		
Global Toroidal	see LBNL (and others?)		

Theory o●ooooooooooo SIS100 impact

Conclusion

#### 4 Coordinate systems: geometry







< □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □ > < □

 SIS100 impact

Conclusion

#### 4 Coordinate systems: geometry









90

Theory 0●00000000000 SIS100 impact

Conclusion

#### 4 Coordinate systems: geometry





◆□>

Ε

Theory oo●ooooooooo SIS100 impact

Conclusion

#### **Basis Equation**

$$\begin{aligned} \frac{d^2H}{d\eta^2} &- \gamma \ H = 0 \quad \text{and} \quad \frac{\partial^2 \bar{\Psi}}{\partial \psi^2} + \gamma \ \bar{\Psi} = 0. \\ \Psi(\eta, \psi)/\Psi_0 &= \frac{a_0}{2} + \sum_{n=1}^{\infty} \left[ a_n \ \frac{\cosh(n\eta)}{\cosh(n\eta_0)} \ \cos(n\psi) + b_n \ \frac{\sinh(n\eta)}{\sinh(n\eta_0)} \ \sin(n\psi) \right], \\ \mathbf{B} &= B_y(\eta + \mathbf{i}\psi) + \mathbf{i}B_x(\eta + \mathbf{i}\psi) = \frac{\mathbf{E}_1}{2} + \sum_{n=2}^{\infty} \mathbf{E}_n \ \frac{\cosh[(n-1)(\eta + \mathbf{i}\psi)]}{\cosh((n-1)\eta_0)}. \end{aligned}$$
$$\mathbf{n} &= \frac{1}{\pi} \ \int_{-\pi}^{\pi} \mathbf{B}_0 \left( \mathbf{z} = e \cosh(\eta_0 + \mathbf{i}\psi) \right) \ \cos((n-1) \ \psi) \ d\psi, \\ &= \frac{1}{2\pi} \ \int_{-\pi}^{\pi} \left[ \mathbf{B}_0 \left( \mathbf{z} = e \cosh(\eta_0 + \mathbf{i}\psi) \right) + \mathbf{B}_0 \left( \mathbf{z} = e \cosh(\eta_0 - \mathbf{i}\psi) \right) \right] \ e^{\mathbf{i}(n-1)\psi} \ d\psi. \end{aligned}$$
(1)

◆□▶ ◆□▶ ◆臣▶ ◆臣▶ 臣 のへぐ

### Fields with elliptic coordinates

- our original proposal [1]: Cartesian field components  $B_y + iB_x$  on elliptic coordinates  $\eta, \psi$
- (Classical) vector analysis: elliptic field components, elliptic coordinates, metric elements, vector operators...
- how do they relate: apply local tangents to transform ...
   [2]

Introduction	

SIS100 impact

Conclusion

## Relation Elliptic / Cylindric

- given in NIMA [1]
- alternative recursive method by Franchetti / Pena) [3]
- or even simpler Chebyshev polynoms :

$$T_n(x) = \cos(n \arccos x)$$
 für  $x \in [-1, 1]$   
 $T_n(x) = \cosh(n \operatorname{arcosh}(x))$  für  $|x| > 1$ 

(courtesy of V. Marousov)

• or : integral [4, 5],

$$\cosh(n\mathbf{w}) = 2^{(n-1)}\cosh^n \mathbf{w} + \sum_{m=1}^{\lfloor n/2 \rfloor} (-1)^m \frac{n}{m} \binom{n-m-1}{m-1} 2^{(n-2m-1)}\cosh^{n-2m} \mathbf{w}$$

• always a finite sum: m elliptic  $\rightarrow$  n + 1 circular

Theory 00000●000000 SIS100 impact

Conclusion

#### Elliptic multipoles on elliptic coordiantes

Field  $\eta + i\psi = \mathbf{w}$ : Tangents:

$$B_{\psi} + iB_{\eta} = e \underbrace{\frac{\sinh w}{\sqrt{\cosh^2 \eta - \cos^2 \psi}}}_{h_t} (By + iB_x)$$
(2)

$$h_t \left( B_{\psi} + i B_{\eta} 
ight) = \left( \hat{B}_{\psi} + i \hat{B}_{\eta} 
ight) = \hat{\mathbf{B}}(\mathbf{w})$$

$$\hat{\mathbf{B}}(\mathbf{w}) = e \sinh[\mathbf{w}] \left[ \frac{\hat{\mathbf{E}}_1}{2} + \sum_{m=2}^{M-1} \cosh\left[(m-1)\mathbf{w}\right] \right]$$
(3)

Potential by integration in  ${\bf w}$  or in  $\eta,\psi$ 

$$\Phi^{\mathbf{e}}(\mathbf{w}) = -\frac{e}{2} \left[ \hat{\mathbf{E}}_{1} \cosh \mathbf{w} + \frac{1}{2} \hat{\mathbf{E}}_{2} \cosh(2\mathbf{w}) + \sum_{m=2}^{M-1} \hat{\mathbf{E}}_{m+1} \left( \frac{1}{m+1} \cosh[(m+1)\mathbf{w}] - \frac{1}{m-1} \cosh[(m-1)\mathbf{w}] \right) \right]. \quad (4)$$

Similar results as for differential forms [2]

### Elliptic multipoles on elliptic coordiantes: $E_1$

That's why metric still considered important ...

For  $E_1 \rightarrow$  direct translation from elliptic to circular harmonics:

$$B_{\psi} + iB_{\eta} = e \frac{\sinh w}{h_t} (By + iB_x)$$
  
=  $\frac{e \sinh w}{h_t} \mathbf{E}_1$   
=  $e \frac{\sinh w}{\sqrt{\cosh^2 \eta - \cos^2 \psi}} (B_1 + iA_1)$ 

Degenerates line for  $\eta = 0$  Poles  $\pm i: B_x = \pm B_\eta, B_y = \pm B_\psi$ 



▲ロト ▲帰ト ▲ヨト ▲ヨト 三日 - の々ぐ

 Introduction
 Theory
 SIS100 impact
 Conclusion

 Elliptic multipoles on elliptic coordiantes:
 E1

etric still considered

ect translation from Ilar harmonics:

 $\frac{\frac{\sinh w}{h_t}(By + iB_x)}{-\cos^2 \psi} (B_1 + iA_1)$ 

ne for  $\eta = 0$  Poles  $_\eta$ ,  $B_y = \pm B_\psi$ 



Theory 0000000●0000 SIS100 impact

Conclusion

### Elliptic multipoles

- elliptic coordinates
- but cylindric field components  $B_y(\eta + i\psi) + iB_x(\eta + i\psi)$
- $B_y + iB_x \Leftrightarrow h_t(\hat{B}_{\psi} + i\hat{B}_{\eta})$ , both analytic complex functions Cauchy Riemann  $\Leftrightarrow \Delta \Phi = 0$  (as defined in Cartesian Coordinates)
- can be calculated by Fourier Transform
- Translation to circular using analytical matrix

## Toroidal Circular Multipoles

- Local toroidal coordinates [6, 4], R-separable
- Transform  $\Phi \rightarrow \sqrt{h}\Phi$ ;  $h = 1 + \varepsilon \rho \cos \vartheta = 1 + x R_C$ ,  $eps = R_{Ref}/rc$  neglect  $\varepsilon^2 \rightarrow Laplace$  Operator of polar coordinates
- solve field expressions: 
  $$\begin{split} \mathbf{B}^{\mathbf{t}}(\mathbf{z}) &= \sum_{m=1}^{M} \left[ R_m \ \mathbf{T}_m^n(\mathbf{z}) \ + \mathbf{i} \, S_m \ \mathbf{T}_m^s(\mathbf{z}) \right] \, . \\ & \left( \mathbf{T}_m^n(\mathbf{z}) \right) = \left( \frac{\mathbf{z}}{R_{Ref}} \right)^{m-1} \left( 1 \varepsilon_{\frac{1}{2}} \frac{\operatorname{Re}(\mathbf{z})}{R_{Ref}} \right) \varepsilon_{\frac{1}{2m}} \left( \begin{array}{c} \operatorname{Im} \left[ \left( \frac{\mathbf{z}}{R_{Ref}} \right)^m \right] \mathbf{i} \\ \operatorname{Re} \left[ \left( \frac{\mathbf{z}}{R_{Ref}} \right)^m \right] \end{array} \right) \, . \end{split}$$
- different basis functions for *normal* and *skew* field expansions

 $R_C$  torus larger radius,  $R_{Ref}$  reference radius, z = x + iy

Theory ○○○○○○○○○○ SIS100 impact

Conclusion

### Coil probe within torus



Theory ○○○○○○○○○○○ SIS100 impact

Conclusion

### Coil probe within torus: Conversion

$$\begin{pmatrix} \vec{R_{\mu}} \\ \vec{S_{\mu}} \end{pmatrix} = \begin{pmatrix} \underline{G_{\nu,\mu}^{nn}} & \underline{G_{\nu,\mu}^{ns}} \\ \overline{G_{\nu,\mu}^{sn}} & \overline{G_{\nu,\mu}^{ss}} \end{pmatrix} \begin{pmatrix} \vec{B_{\nu}} \\ \vec{A_{\nu}} \end{pmatrix} .$$
(5)  
$$\begin{pmatrix} G^{nn} \\ G^{ns} \\ G^{sn} \\ G^{ss} \end{pmatrix} = I + \mathcal{L}^{dr} + \varepsilon \left( -U + \mathcal{L}^{L} - \mathcal{L}^{sk} + i\mathcal{L}^{R2} \right) + \varepsilon \begin{pmatrix} \operatorname{Re} \left[ \mathcal{L}^{R2_0} \right] \\ - \operatorname{Im} \left[ \mathcal{L}^{R2} \right] \end{pmatrix}$$
(6)

$$\begin{split} & \text{feed down...} \mathcal{L}_{\nu,\mu}^{dr} = \binom{\nu-1}{\mu-1} \left( \frac{\mathbf{d}_{z}}{R_{Ref}} \right)^{\nu-\mu} * \mathcal{L}_{\nu,\mu} - I \\ & \text{feed down 2...} \mathcal{L}_{\nu,\mu}^{dr} = R_{Ref} \frac{\mathbf{d}}{\mathbf{d}_{z}} \mathcal{L}^{dr}, \, \mathbf{d}_{z} = (d_{x} + \mathbf{i}d_{y})/R_{Ref} \\ & \mathcal{L}_{\nu,\mu}^{L} = \frac{L^{2}}{3R_{Ref}^{2}} \mathcal{L}^{dr2} \\ & \mathcal{L}_{\nu,\mu}^{sk} = \frac{1}{4(\mu+1)} * \frac{K_{\mu+2}}{K_{\mu}} * \mathcal{L}^{dr2} \\ & \mathcal{L}_{\nu,\mu}^{R2} = \frac{1}{4\nu} \left( \frac{\nu\mu}{\nu-\mu+1} * \mathcal{L}_{\nu,\mu} + \delta_{\mu,1} \right) * \left[ \frac{d_{y}}{R_{Ref}} - \left( \frac{2-\mu+2\nu}{\mu} * \mathcal{L}_{\nu,\mu} - \nu\delta_{\mu,1} \right) \mathbf{i} \frac{d_{x}}{R_{Ref}} \right] * \left( \mathcal{L}^{dr} + I \right) . \\ & \mathcal{L}_{\nu,\mu}^{R20} = \frac{1}{2\nu} \left( \frac{\mathbf{d}_{z}}{R_{Ref}} \right)^{\nu} \delta_{\mu,1}. \end{split}$$

SIS100 impact

### Summary

- elliptic multipoles:
  - Cartesian vector field on elliptic coordinates, complex representation,
  - $\leftrightarrow$  mapping to  $B_{\eta}, B_{\psi}$ ;
  - $\hat{\mathbf{B}}(w)/ht$  relation to real space coordinates!  $\eta_0$ :  $B_y = \pm B_\psi$
- Local Toroidal multipoles: approximate solution:  $\lim_{\varepsilon \to 0} cylindric circular multipoles$
- good for machines like SIS100, SIS300
- allows estimate rotating coil probe artefacts, deducing reasonable coil probe length

Theory 00000000000000 SIS100 impact

Conclusion

#### Measuring: mole $\leftrightarrow$ mapper



◆□ > ◆□ > ◆豆 > ◆豆 > ̄豆 \_ のへぐ

SIS100 impact

#### Correcting coil measurements





200

Theory 000000000000 SIS100 impact

Conclusion

1500 A

### End field comparison



 $\begin{array}{ll} B_y & \Delta B_y \\ \text{solid lines...mapper, dashed lines...coil,} \\ \text{blue...y} = + \ 10 \ \text{mm, green...y} = 0, \ \text{red...y} = - \ 10 \ \text{mm} \\ \bullet \ \text{Data quite matching:} \end{array}$ 

• taking different coordinate systems into account

• inverting  $\Delta B_y$ , searching (twisted cable on patch panel) "injection field level"

SIS100 impact

Conclusion

#### First allowed harmonics



Theory 00000000000000 SIS100 impact

Conclusion

# I/IV

### Not allowed Harmonic



Sac

### Conclusion

#### • Theory:

- Alternative coordiante systems
- elliptic multipoles: allow description of fields within elliptic beam pipe
- Local toroidal coordinates: follow particle trajectory within a bent
- approximation: simpler systems than Global toroidal ones (if approximation acceptable)
- can deduce measurements for rotating coil probes
- Application
  - on SIS00 magnet:
    - detected skew harmonics
    - $\bullet\,$  gave reliable results  $\leftrightarrow$  an error that could have been missed

SIS100 impact

Conclusion

◆□▶ ◆□▶ ◆臣▶ ◆臣▶ 臣 のへぐ

P. Schnizer, B. Schnizer, P. Akishin, and E. Fischer. Theory and application of plane elliptic multipoles for static magnetic fields.

Nuclear Instruments and Methods in Physics Research Section A: Accelerators, Spectrometers, Detectors and Associated Equipment, 607(3):505 – 516, 2009.

- B. Auchmann, N. Kurz, and S. Russenschuck. Plane field harmonics in accelerator magnets. In COMPUMAG, 2011.
- F. R. Peña and G. Franchetti. Elliptic and circular representation of the magnetic field for SIS100.

Technical report, GSI, 2008.

P. Schnizer, B. Schnizer, and E. Fischer.

Cylindrical circular and elliptical, toroidal circular and elliptical multipoles, fields, potentials and their measurement for accelerator magnet.

arXiv preprint physics.acc-ph, October 2014.

- S.I. Gradshteyn and I.M. Ryzhik. Table of Integrals, Series and Products. Academic Press, 1965.
- P. Schnizer, B. Schnizer, P. Akishin, and E. Fischer. Theoretical field analysis for superferric accelerator magnets using plane elliptic or toroidal multipoles and its advantages.

In *The 11<sup>th</sup> European Particle Accelerator Conference*, pages 1773 – 1775, June 2008.