

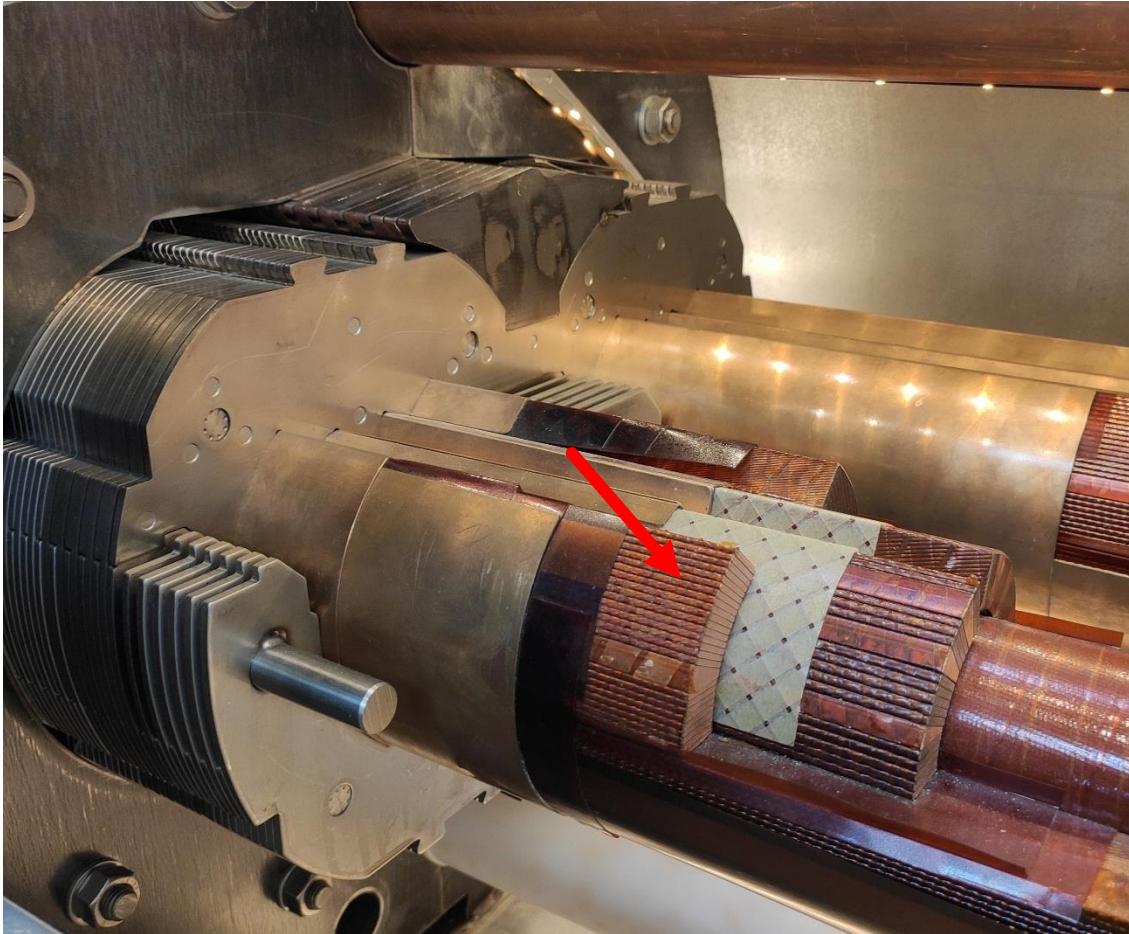


Towards epoxy resins for cryogenic applications

CHART workshop
June 9th, 2022

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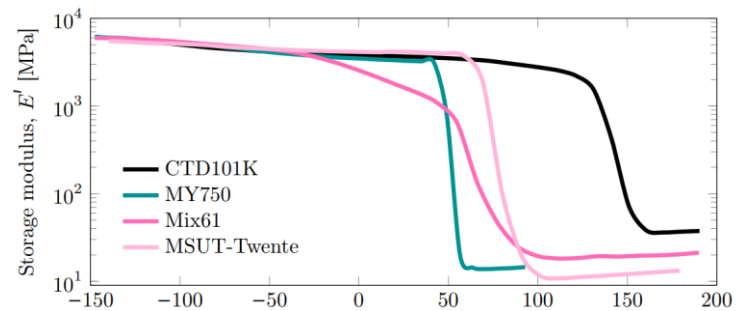
Superconducting electromagnets



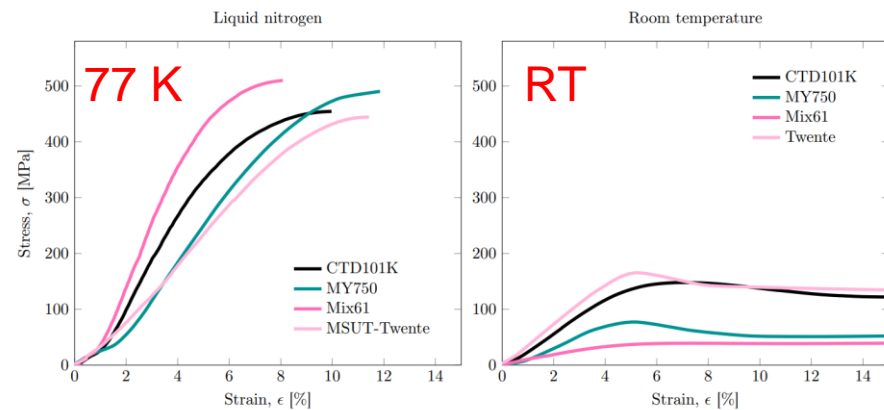
- Stresses in epoxy insulation
 - Thermal stresses
 - Lorentz forces
- Cracking / Delamination / Yielding → Quenching of magnet
- Goal: Develop a new epoxy resin
 - Longer pot-life than current resins
 - Good fracture resistance at 4 K (tested at 77 K)
 - Solid at room temperature
- Develop an understanding
 - Relation between toughness and structure
 - Adhesive properties

Previous Research (André Brem et al.)

- 4 resin systems
 - Elastic modulus

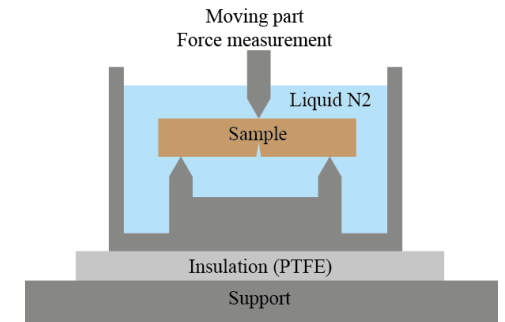
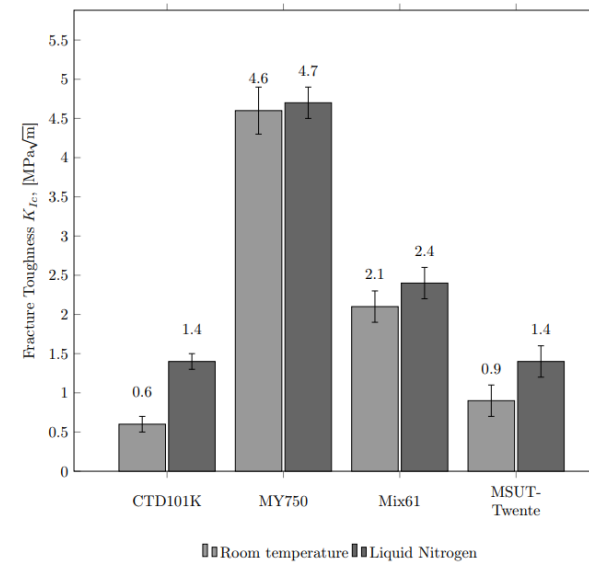


- Yield in compression



- Fracture toughness

- Large differences, even at 77K

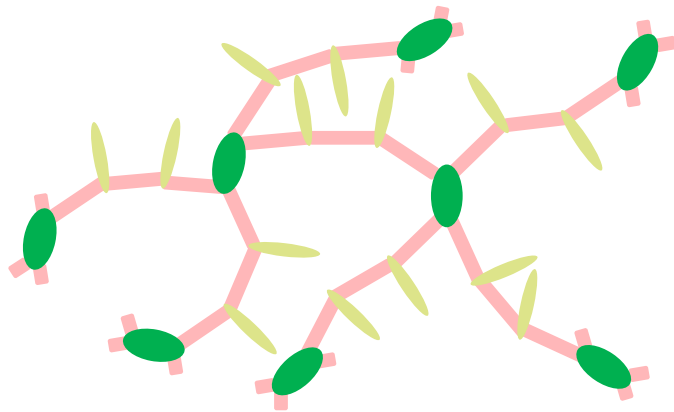


Network design parameters

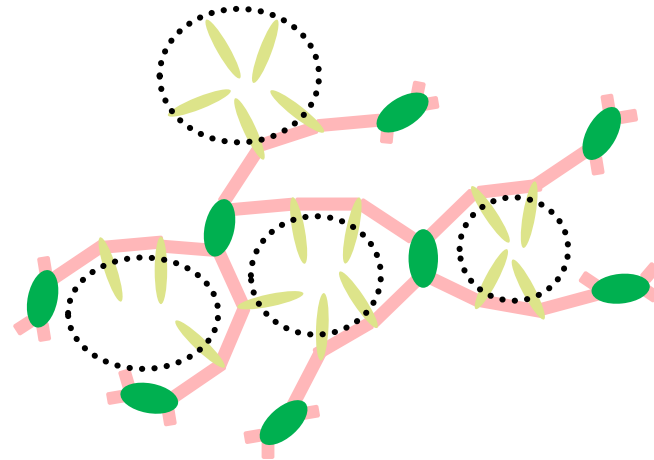
- $F = 4$ Functionality of hardener
- $R = 3:2$ Ratio DGEBA:Aliphatic amine

$F \in \{4, 3, 2\}$
 $R \in \{1:0, 5:4, 9:8\}$

Example: $F=4$, $R = 3:2$



1st hypothesis: Nanodomains



Are there nanodomains and
are they responsible for
improved properties?

Monomers and reaction mechanism

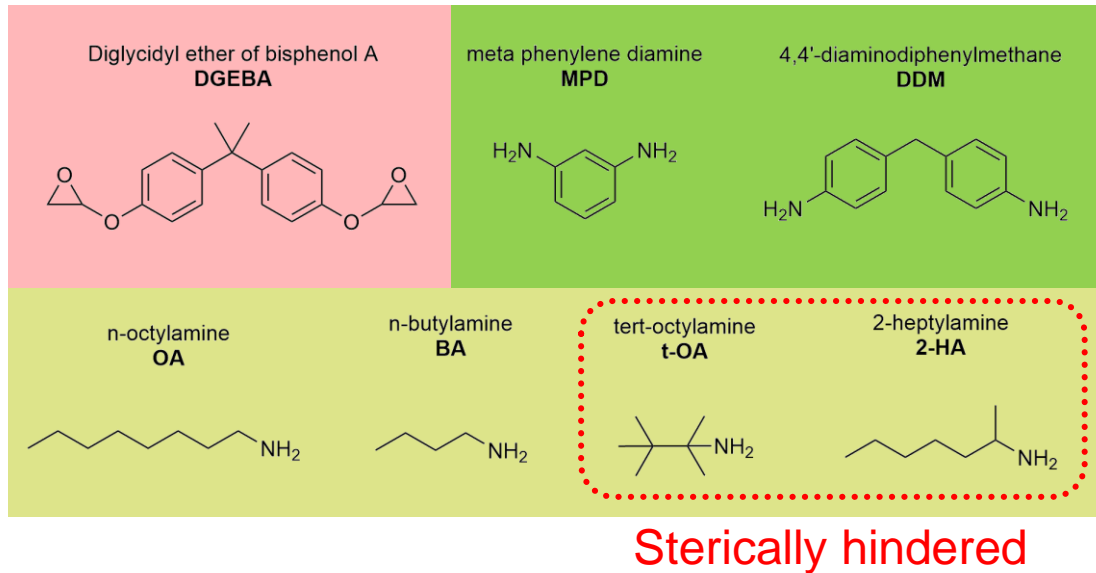
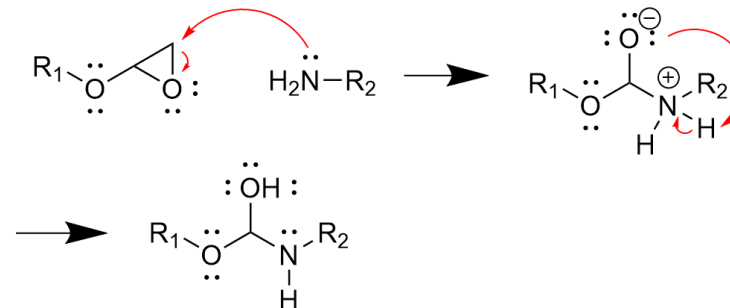


Table 1

Monomers used for synthesizing the epoxy resins. F denotes the functionality of the component. EEW denotes the epoxide equivalent weight (g/mol).

| Name | Abbreviation | F | EEW |
|------------------------------|--------------|---|------|
| bisphenol A diglycidyl ether | DGEBA | 2 | 172 |
| meta phenylene diamine | MPD | 4 | 27.0 |
| 4,4'-diaminodiphenylmethane | DDM | 4 | 49.6 |
| n-octylamine | OA | 2 | 64.6 |
| n-butylamine | BA | 2 | 36.6 |
| tert-octylamine | t-OA | 2 | 64.6 |
| 2-heptylamine | 2-HA | 2 | 57.6 |



Sample overview

Table 2
Sample overview

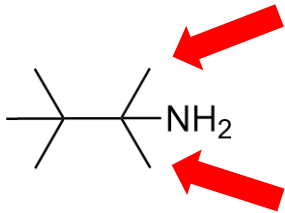
| | System | ID | R | f | KIC (RT) | KIC (LN2) | Tg (max tand) | Density |
|----------------|------------------|-----------|-----|---|-----------|-----------|---------------|---------|
| Var. R | DGEBA, MPD | Base | 1:0 | 4 | 0.8 ± 0.1 | 2.0 ± 0.1 | 160.1 | 1.217 |
| | DGEBA, BA, MPD | BA-4-5:4 | 5:4 | 4 | 1.2 ± 0.2 | 3.5 ± 0.6 | 68.3 | 1.153 |
| Var. f | DGEBA, BA, MPD | BA-4-9:8 | 9:8 | 4 | 1.5 ± 0.1 | 4.1 ± 0.6 | 61.4 | 1.145 |
| | DGEBA, BA, MPD | BA-2-9:8 | 9:8 | 2 | 1.9 ± 0.2 | 5.3 ± 0.4 | n.a. | 1.145 |
| Var. sidechain | DGEBA, BA, MPD | BA-3-9:8 | 9:8 | 3 | 1.6 ± 0.1 | 5.0 ± 1.1 | 73.0 | 1.147 |
| | DGEBA, OA, MPD | OA-3-9:8 | 9:8 | 3 | 1.8 ± 0.1 | 4.4 ± 0.5 | 54.4 | 1.109 |
| | DGEBA, t-OA, MPD | tOA-3-9:8 | 9:8 | 3 | 1.0 ± 0.1 | 2.7 ± 0.4 | 100.7 | 1.108 |
| | DGEBA, 2-HA, MPD | 2HA-3-9:8 | 9:8 | 3 | 1.8 ± 0.1 | 4.7 ± 0.3 | 72.4 | 1.115 |
| | DGEBA, BA, MPD | BA-3-5:4 | 5:4 | 3 | 1.6 ± 0.2 | 4.7 ± 0.3 | n.a. | 1.153 |
| | DGEBA, OA, MPD | OA-4-5:4 | 5:4 | 4 | 1.5 ± 0.2 | 4.6 ± 0.4 | n.a. | 1.115 |

- Addition of Butylamine, Octylamine or 2-Heptylamine → Improved toughness at 77 K!
- Due to nanophase separation?

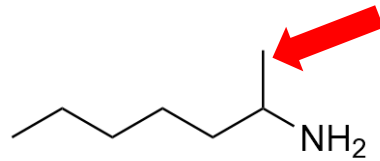
First result: Improved pot-life by sterical hindrance

- Methyl group in β -position \rightarrow sterical effect!

tert-octylamine
t-OA



2-heptylamine
2-HA



- **Significantly longer pot-life with 2-Heptylamine or tert-Octylamine**

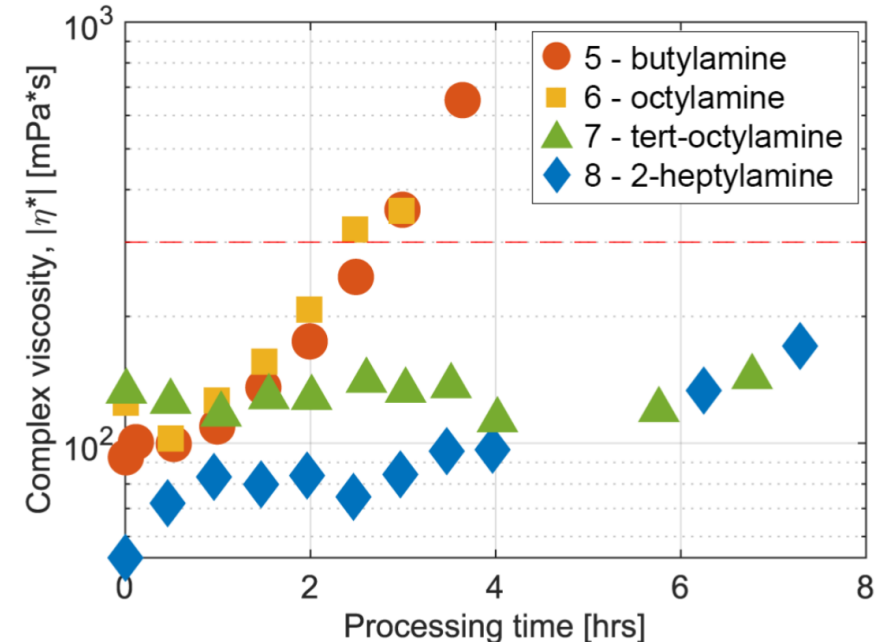
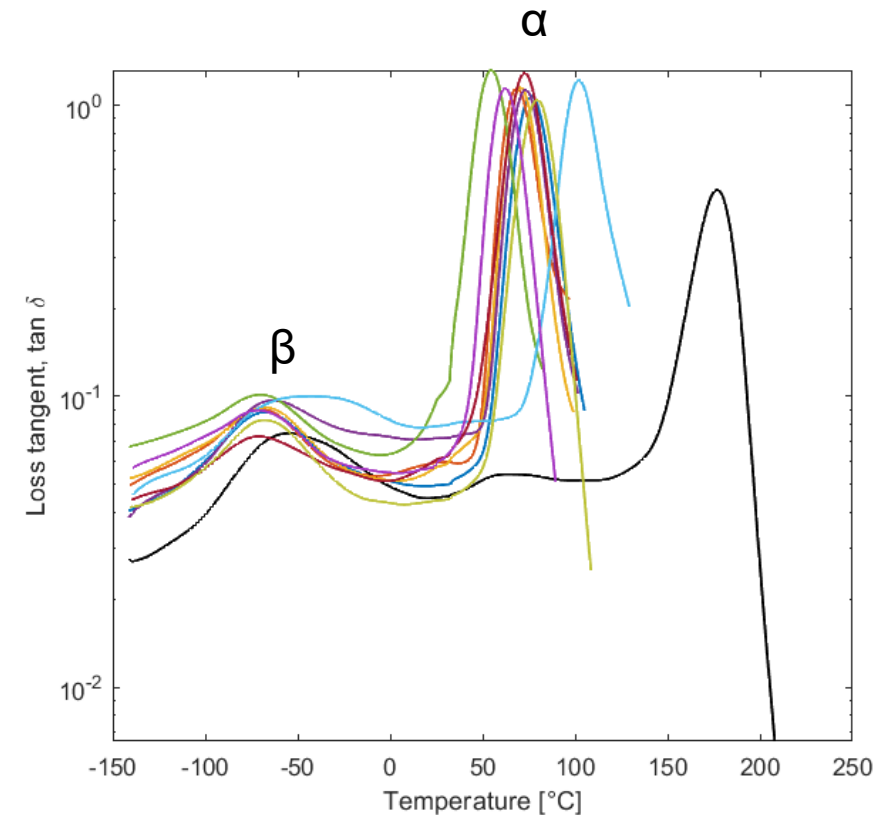
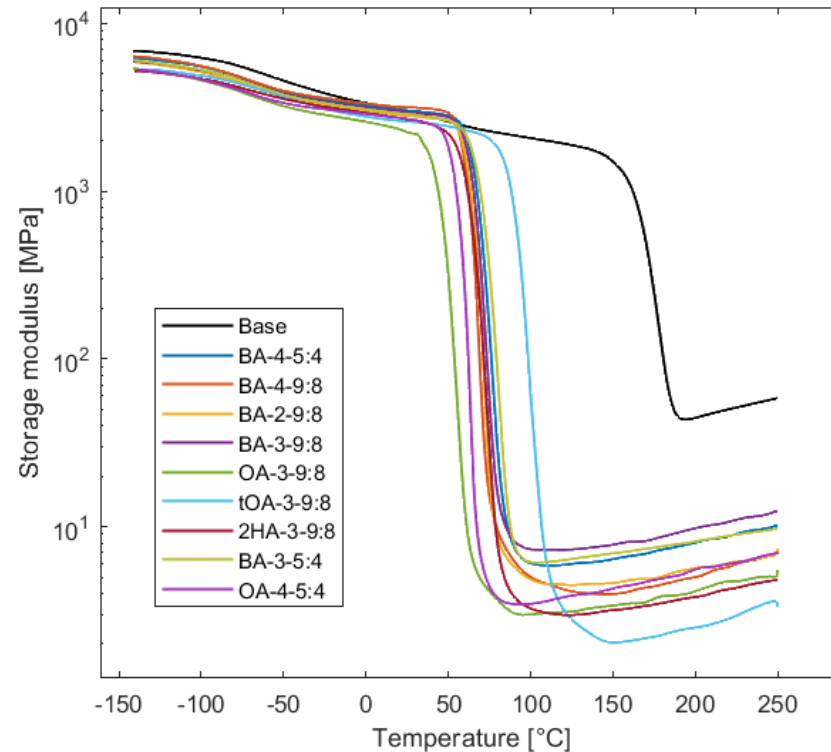


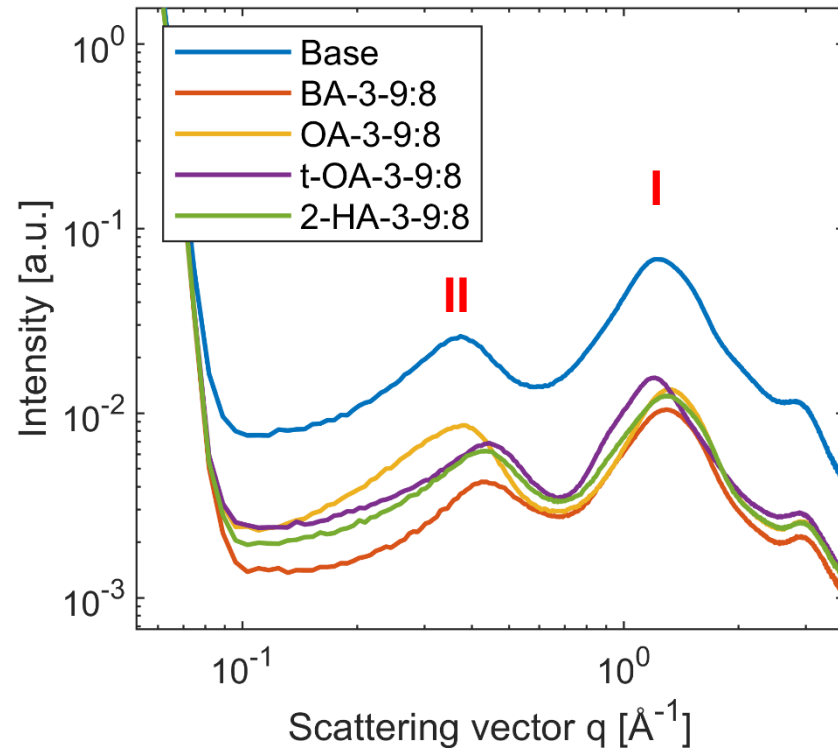
Figure 3: Time dependence of the complex viscosity of as-prepared mixtures stored at 22.5 °C for specified amounts of time. The measurements were done at 22.5 °C.

DMTA – No proof for nanophase separation

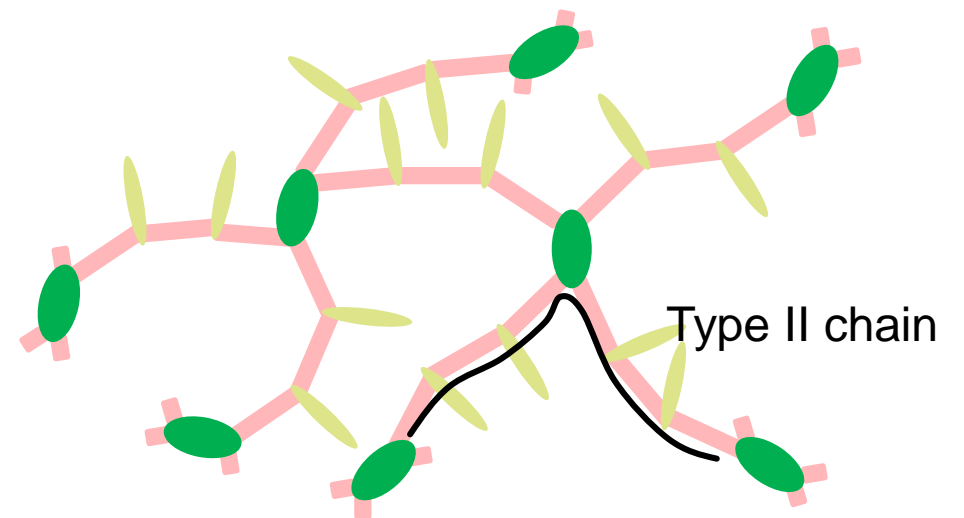


- Tougher systems seem to have less broad β -relaxation
- No other relaxations detected – inconclusive with respect to nanophase separation

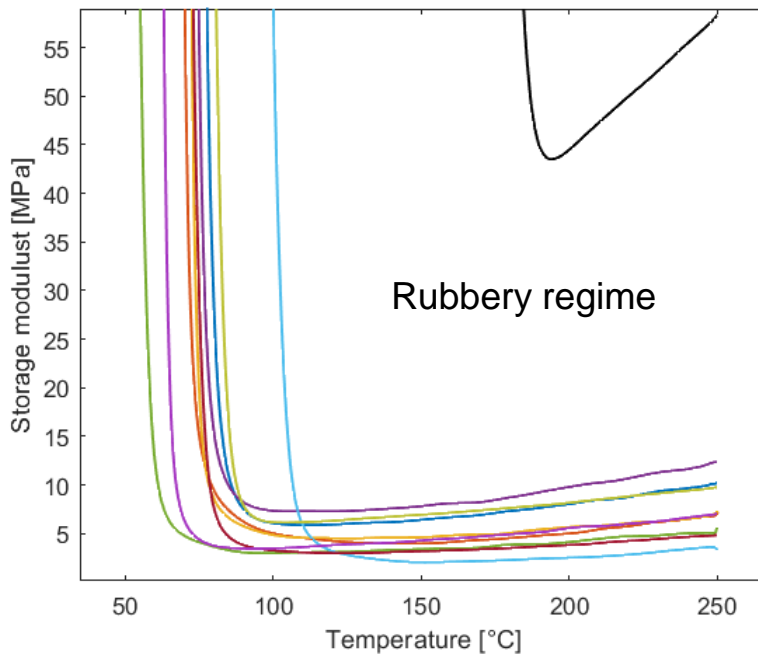
WAXS scattering – Influence of sidechain-type



- **Peak I:** 1.25 \AA^{-1} / 5 \AA
 - Amorphous halo (VdW interactions)
- **Peak II:** 0.4 \AA^{-1} / 15 \AA
 - Also visible in Base system, ascribed to Type-II chains in the network (Lovell, 1989)
 - Not enough evidence for nanophase separation



DMTA – Extraction of crosslink density



➤ From rubber elasticity theory:

$$M_C^{-1} \propto \left(\frac{G_R}{T} \right) \frac{1}{g\rho R} \quad \xrightarrow{\rho_C = M_C^{-1} \rho} \quad \rho_C \propto \left[\left(\frac{G_R}{T} \right) \frac{1}{gR} \right]$$

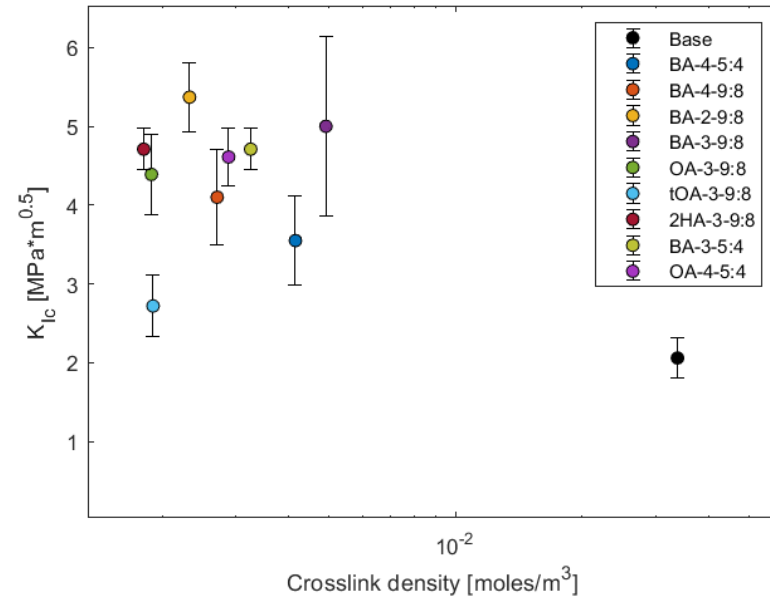
fit from data

➤ Variables:

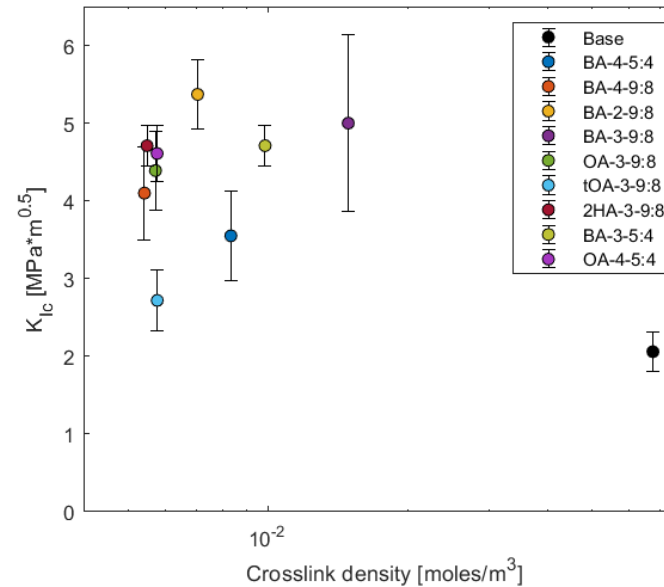
- M_C Molecular weight between crosslinks [g/mol]
- g Factor accounting for crosslink mobility
 - $g=1$ Immobile crosslinks
 - $g=(f_c-2)/f_c$ Mobile crosslinks
- ρ density [g/cm³]
- R Ideal gas constant
- G_R Rubbery modulus [N/mm²]
- T Temperature [K]
- ρ_C Crosslink density [mol/cm³]

Dependence of K_{IC} at 77K on measured crosslink density

$g=1$



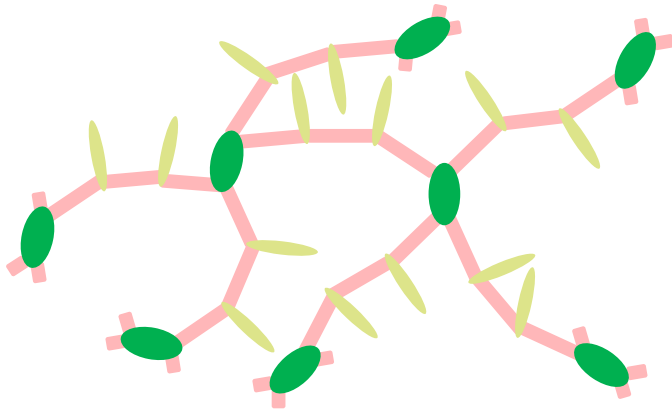
$g=(f_c-2)/f_c$



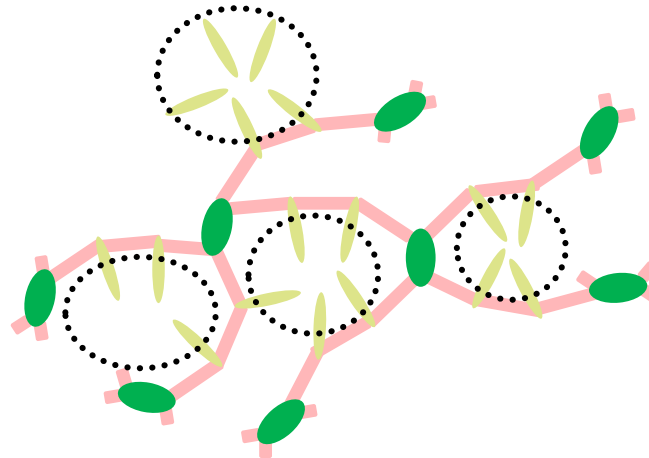
- The correlation is very weak
- Crosslink density as reason for improved toughness is also not confirmed

New hypothesis for improved properties

Example: $F=4$, $R = 3:2$



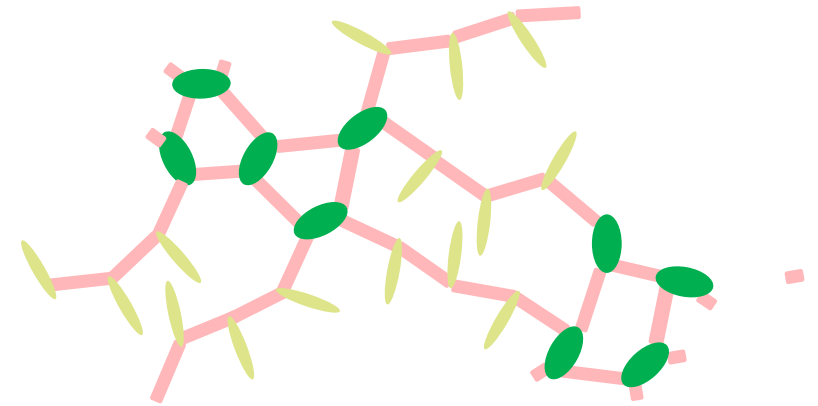
1st hypothesis: Nanodomains



No proof

1. No additional relaxation
2. Very similar WAXS pattern

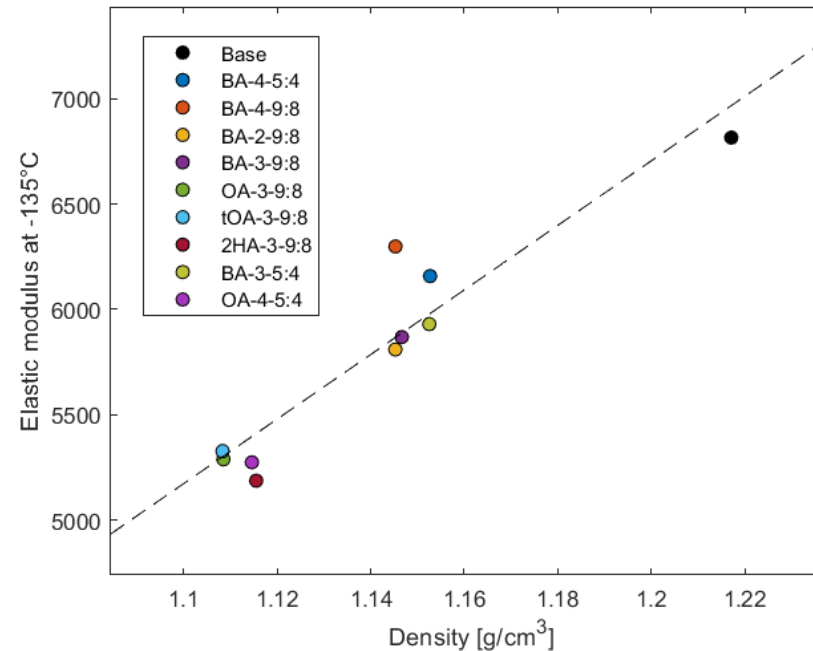
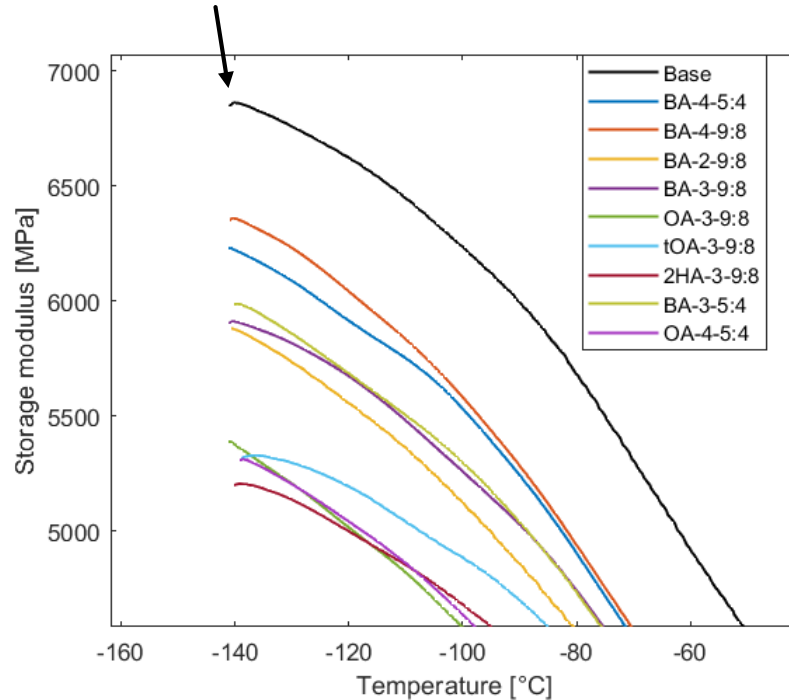
2nd hypothesis: Large scale inhomogeneities



→ SAXS / USAXS measurements planned

Dependence of E' at -140°C on measured density

Extraction of moduli



- Lower modulus with more aliphatic side-chains
 - Polyethylene-like chains decrease cohesive energy density

Grüneisens 1st rule
(Isotropic van der Waals materials)

$$E_{0K} = 3(1 - v) \frac{mn}{4} \frac{E_{\text{coh}}}{V_{0K}}$$

Conclusions

- New, **tough** epoxy resin formulation with **long pot-life**
 - Long pot-life
 - Low viscosity
 - Lower elastic modulus
 - Thermal expansion yet to be measured
- Structure-property relationship for toughness not yet established