

**PSI** Center for  
Photon Science

# Bulk High Temperature Superconducting Undulator

## Pole optimization and Shimming

Carlos Gafa', Alexandre Arsenault, Marco Calvi, John Durrell,  
Anthony Dennis, Nicholas Sammut, Andrew Sammut

# Agenda



- 1 Introduction
- 2 Modelling framework
- 3 Ferromagnetic pole optimization
- 4 Ferromagnetic pole shimming
- 5 Conclusion

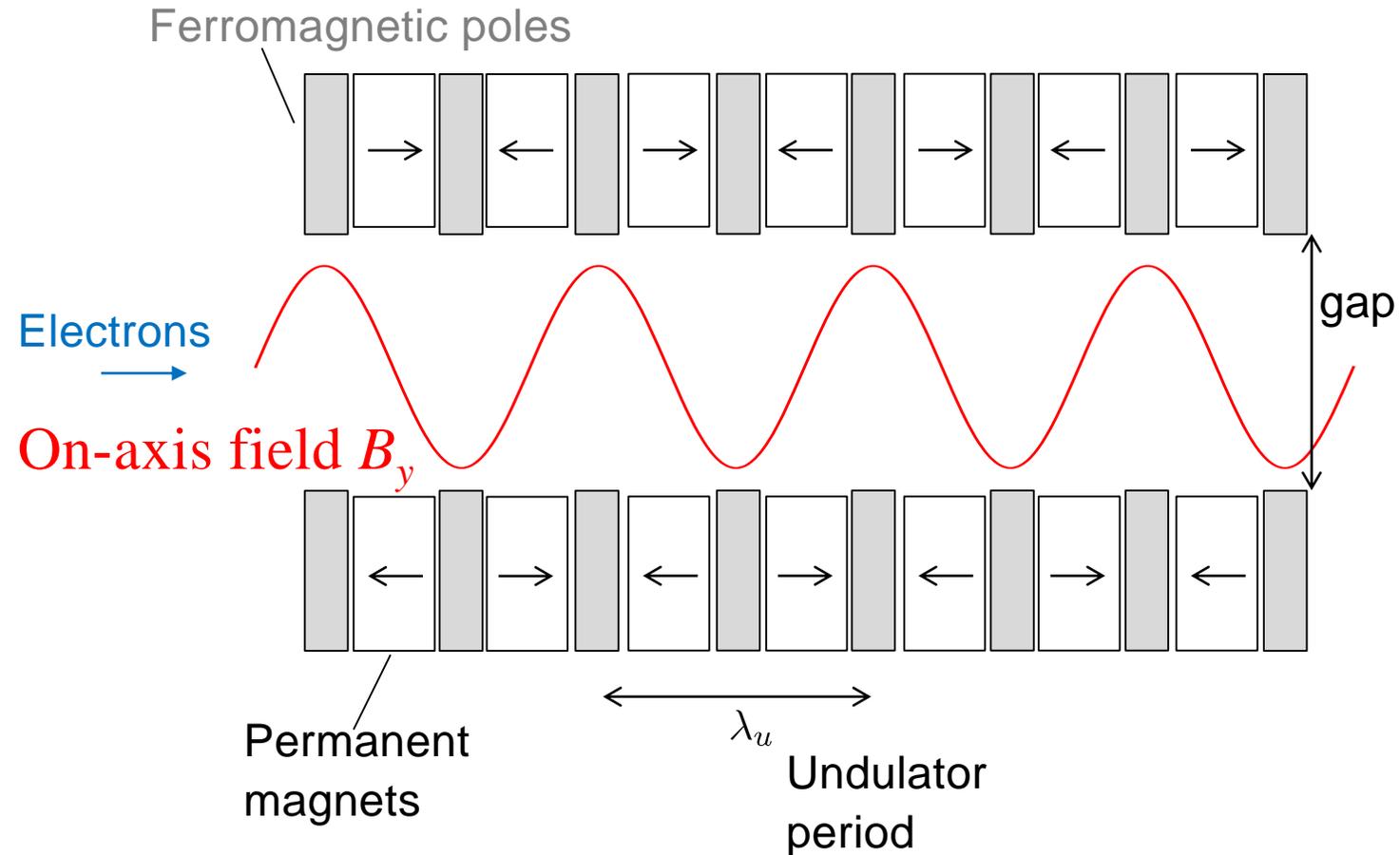
# Introduction

Synchrotron radiation is the light emitted when relativistic charged particles are accelerated (where  $a \perp v$ )

Undulators have been introduced to increase the brightness of the X-ray source by making use of interference effects .

Hybrid undulators make use of ferromagnetic poles to

- Increase the peak on-axis field
- Serve as a tool to locally adjust the field



Traditional hybrid permanent magnet undulator

# Introduction

- To increase the flux and energy of synchrotron radiation, higher magnetic fields and lower undulator period
- A record on-axis field of 2.1 T for a 10 mm period undulator has been demonstrated [K. Zhang, 2023]

$$\lambda = \frac{\lambda_u}{2n\gamma^2} \left( 1 + \frac{1}{2}K^2 \right)$$

Harmonic Number

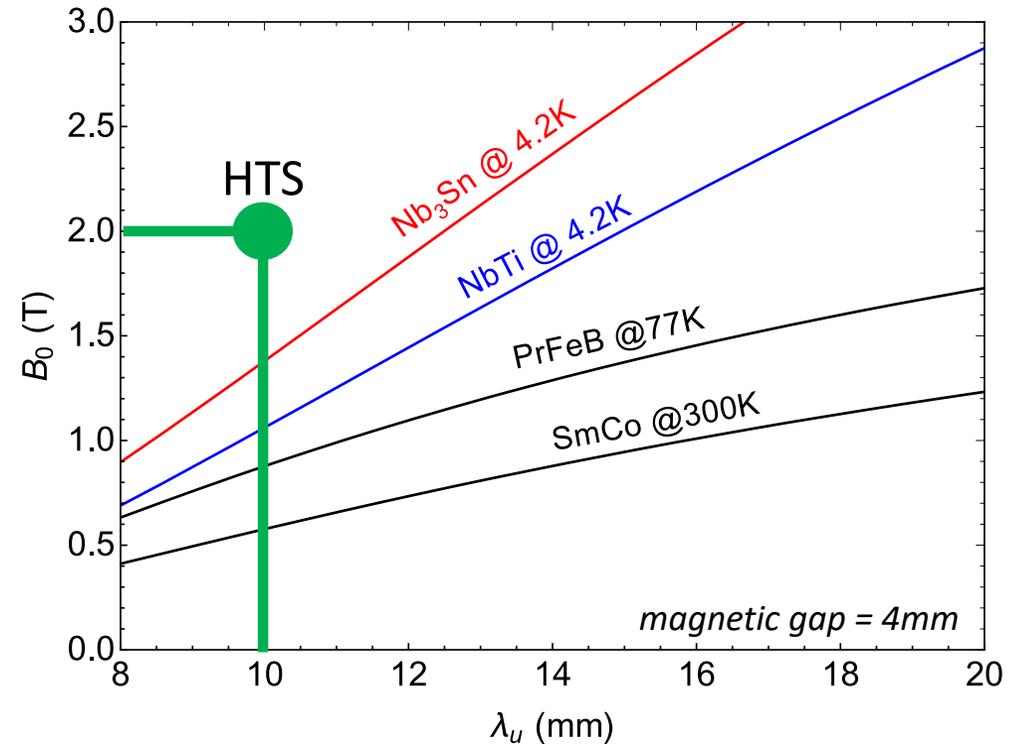
Beam Energy

Deflection Parameter

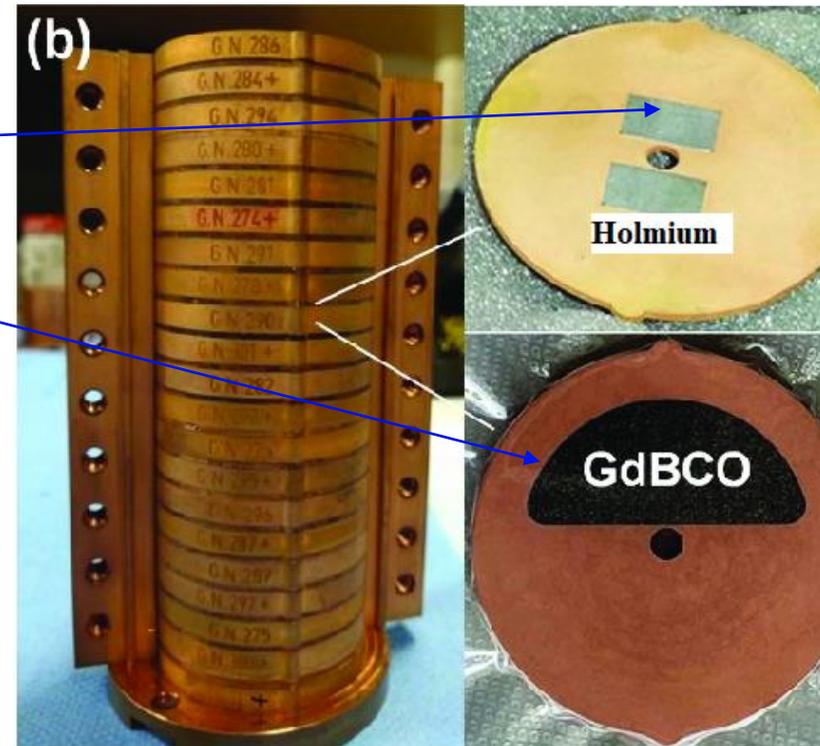
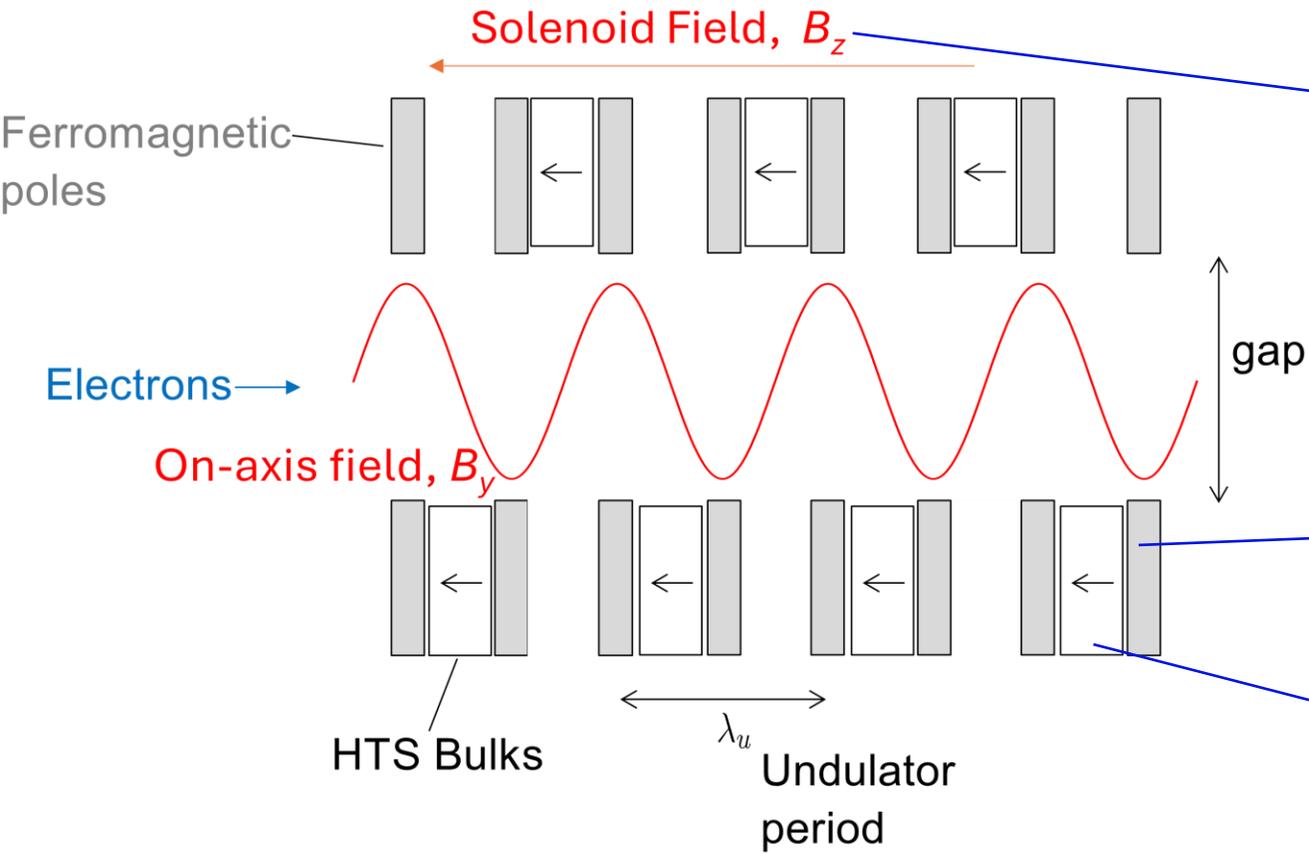
Peak on-axis field

$$K = \frac{B_0 e \lambda_u}{m c 2 \pi}$$

Sinusoidal Field

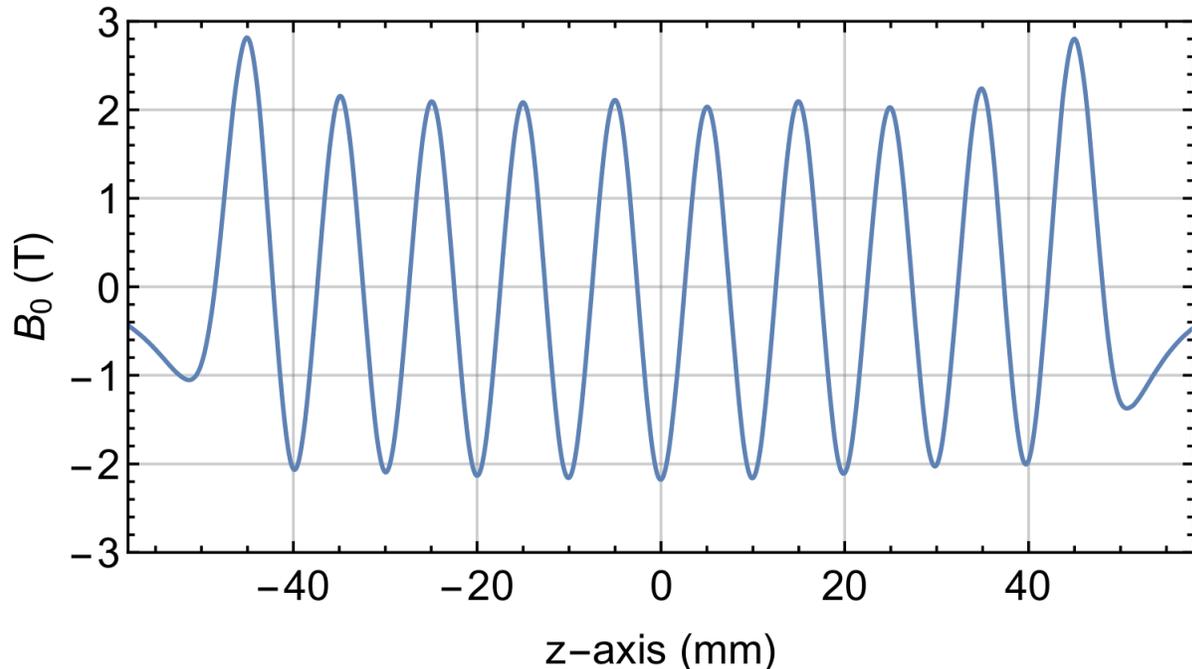


# Introduction

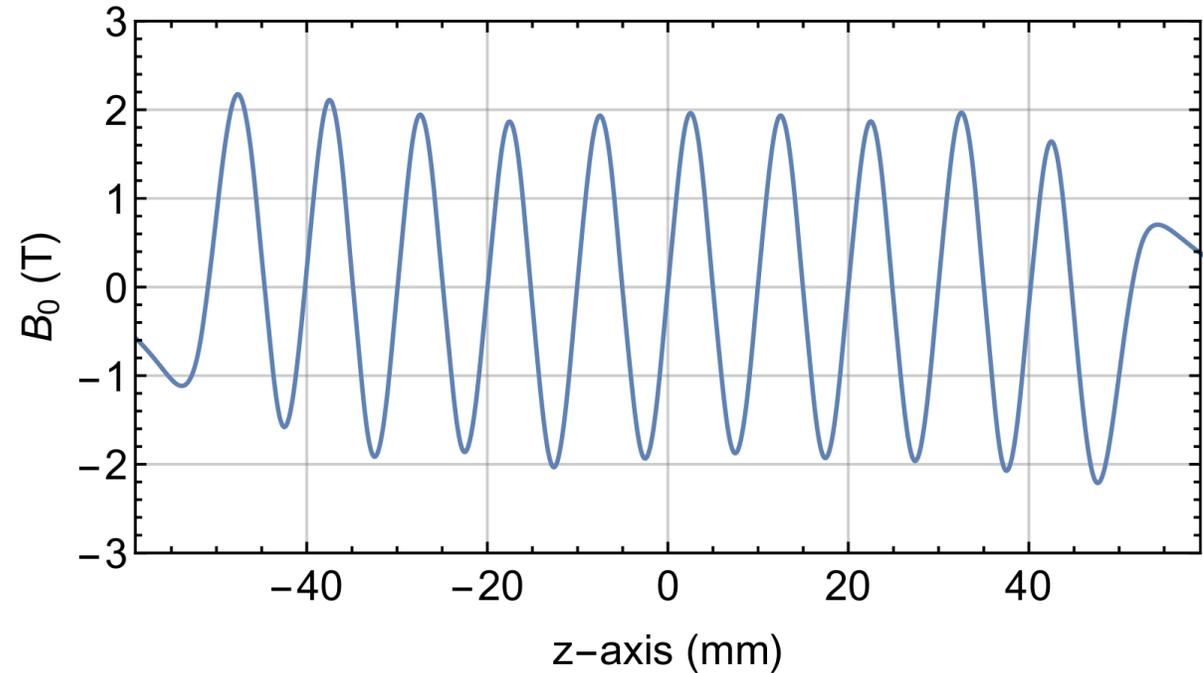


# Introduction

- Due to the growth process, the magnetic properties of HTS bulks can vary, leading to deviations from a periodic on-axis field
- A periodic field is required to use the high harmonics of the emitted light
- Need to find strategies to improve the field quality



High quality Nippon steel bulks; Expensive, less errors



SDMG bulks; Cheaper, require more correction for periodic field

# Agenda



- 1 Introduction
- 2 **Modelling framework**
- 3 Ferromagnetic pole optimization
- 4 Ferromagnetic pole shimming
- 5 Conclusion

# Modelling framework

- The H- $\phi$  formulation was used to simulate the HTSU for efficient computations [A. Arsenault, 2021]
- Involves solving the well-known H-formulation, combining Faraday and Ampere's law:

$$\nabla \times (\rho(J) \nabla \times H) = -\frac{\partial B}{\partial t}$$

Weak Form

$$\int_{\Omega} \rho \nabla \times H \cdot \nabla \times \tilde{H} d\Omega + \frac{\partial}{\partial t} \mu \int_{\Omega} H \cdot \tilde{H} d\Omega - \int_{\Gamma} \hat{n} \times E \cdot \tilde{H} d\Gamma = 0$$

Using the scalar potential  $\phi$  in non-conducting domains, to decrease computation times by a factor of 3

$$H = -\nabla \phi$$

$$\frac{\partial}{\partial t} \mu \int_{\Omega_{nc}} \nabla \phi \cdot \nabla \tilde{\phi} d\Omega - \int_{\Gamma} \hat{n} \times E \cdot \nabla \tilde{\phi} d\Gamma = 0$$

Test Function

The equivalent boundary terms leads to a more natural coupling between the two physics

- The bulk's properties are modelled with  $B = \mu_0 H$  and the superconducting power law resistivity:

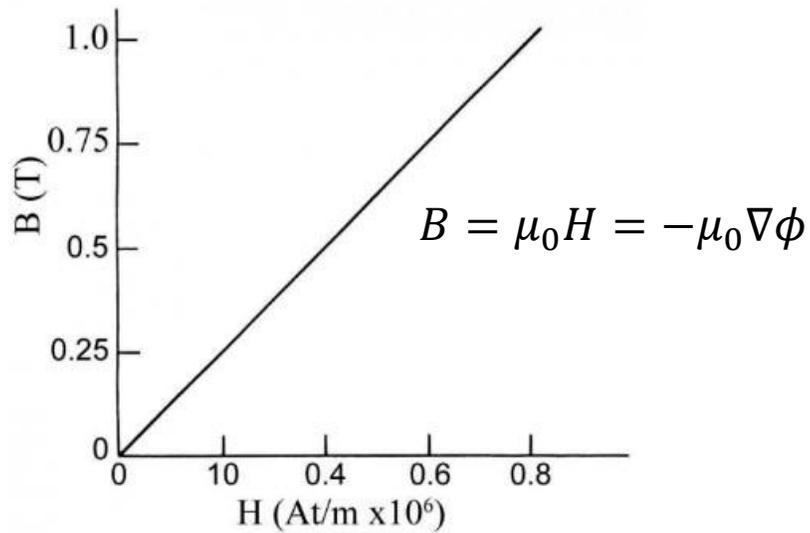
$$\rho = \frac{E_c}{J_c} \left( \frac{|\mathbf{J}|}{J_c} \right)^{n-1}$$

- The air domains are also modelled using  $B = \mu_0 H$
- The conductivity of the holmium poles is smaller than that of copper and may be ignored such that the poles are simulated using the  $\phi$  physics as well

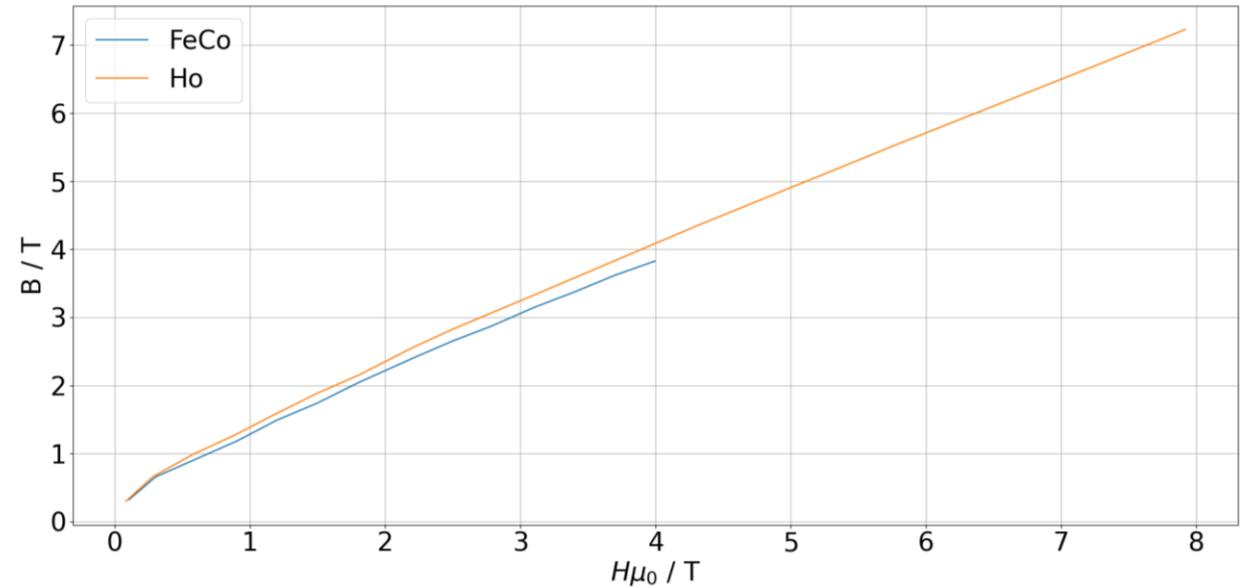
$$\nabla \times (\rho(J) \nabla \times H) = -\frac{\partial B}{\partial t}$$

## Relationship between B and H

### Air and HTS



### Ferromagnet [M. Norsworthy, 2010]



$$B = -f(|\nabla \phi|) \underbrace{\frac{\nabla \phi}{|-\nabla \phi|}}_{\text{Get Sign of Magnetic Field}}$$

BH-Curve

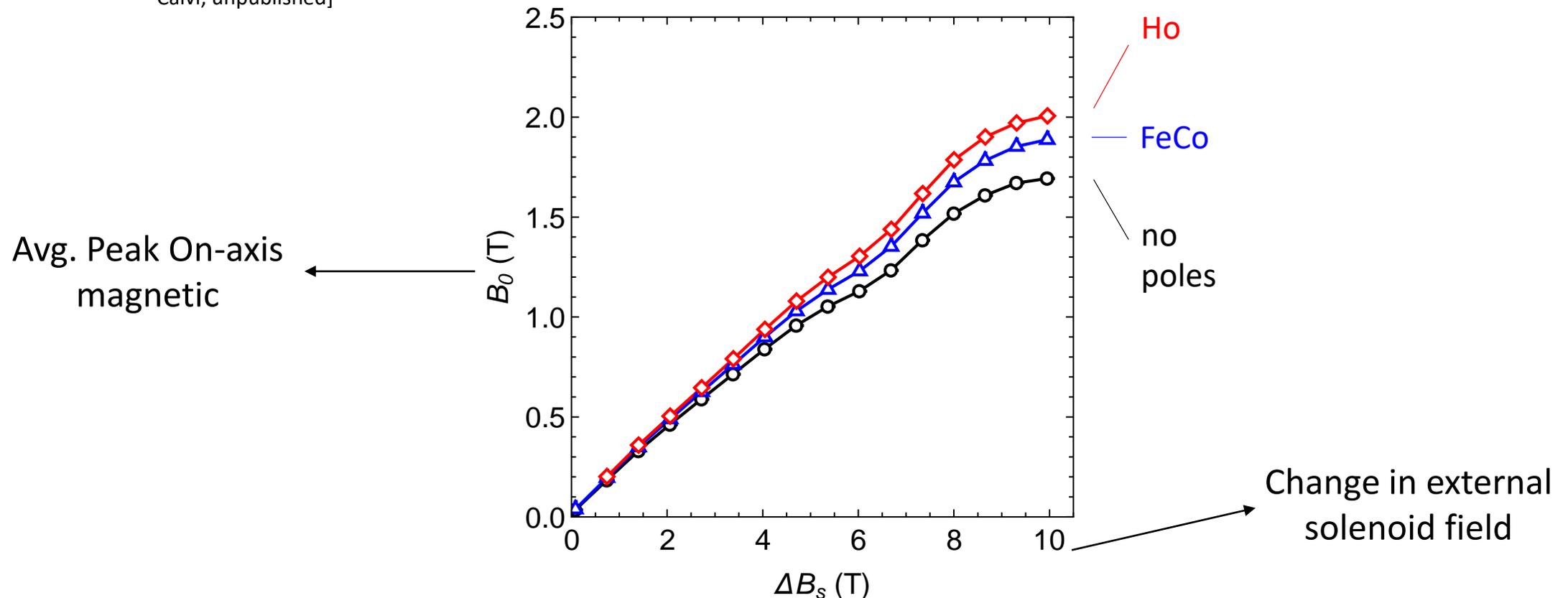
# Agenda



- 1 Introduction
- 2 Modelling framework
- 3 Ferromagnetic pole optimization**
- 4 Ferromagnetic pole shimming
- 5 Conclusion

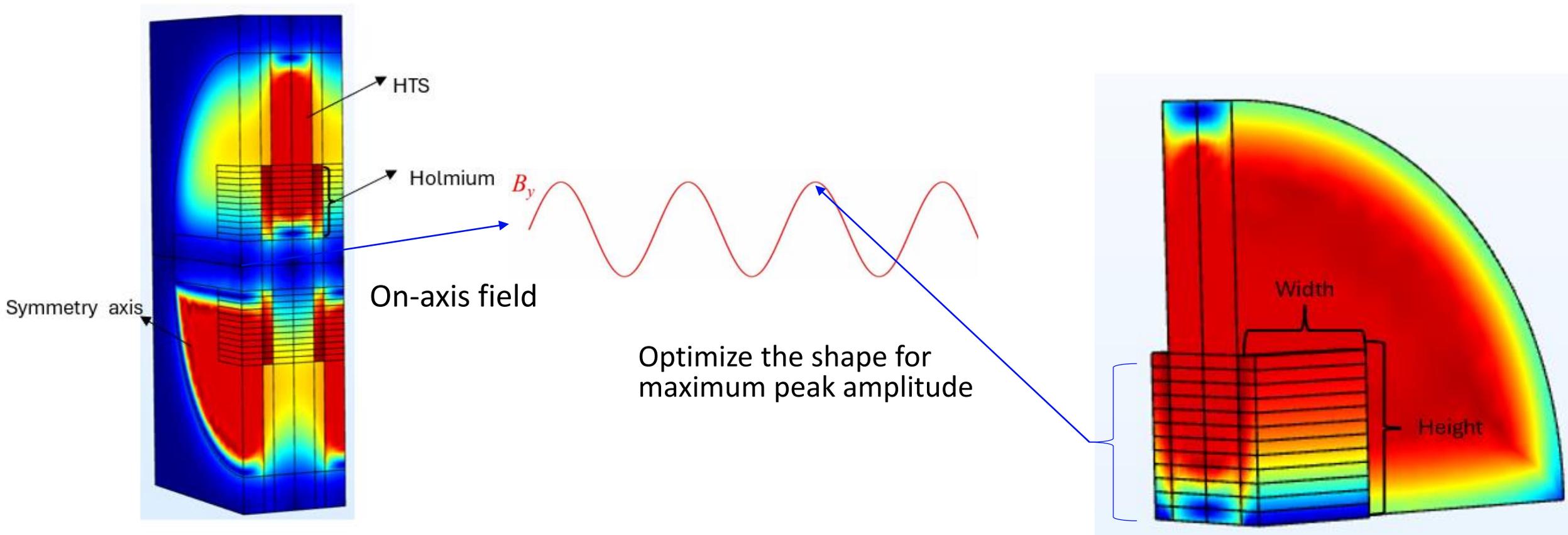
# Ferromagnetic pole optimization

- Traditional undulators use iron cobalt for the poles
- However, at the HTSU operating temperature (<10K) stronger materials become available
- We tested a 20-bulk sample with both materials
- Holmium was found to give a 0.1T peak on-axis field increase compared to iron cobalt [M. Calvi, unpublished]



# Ferromagnetic pole optimization

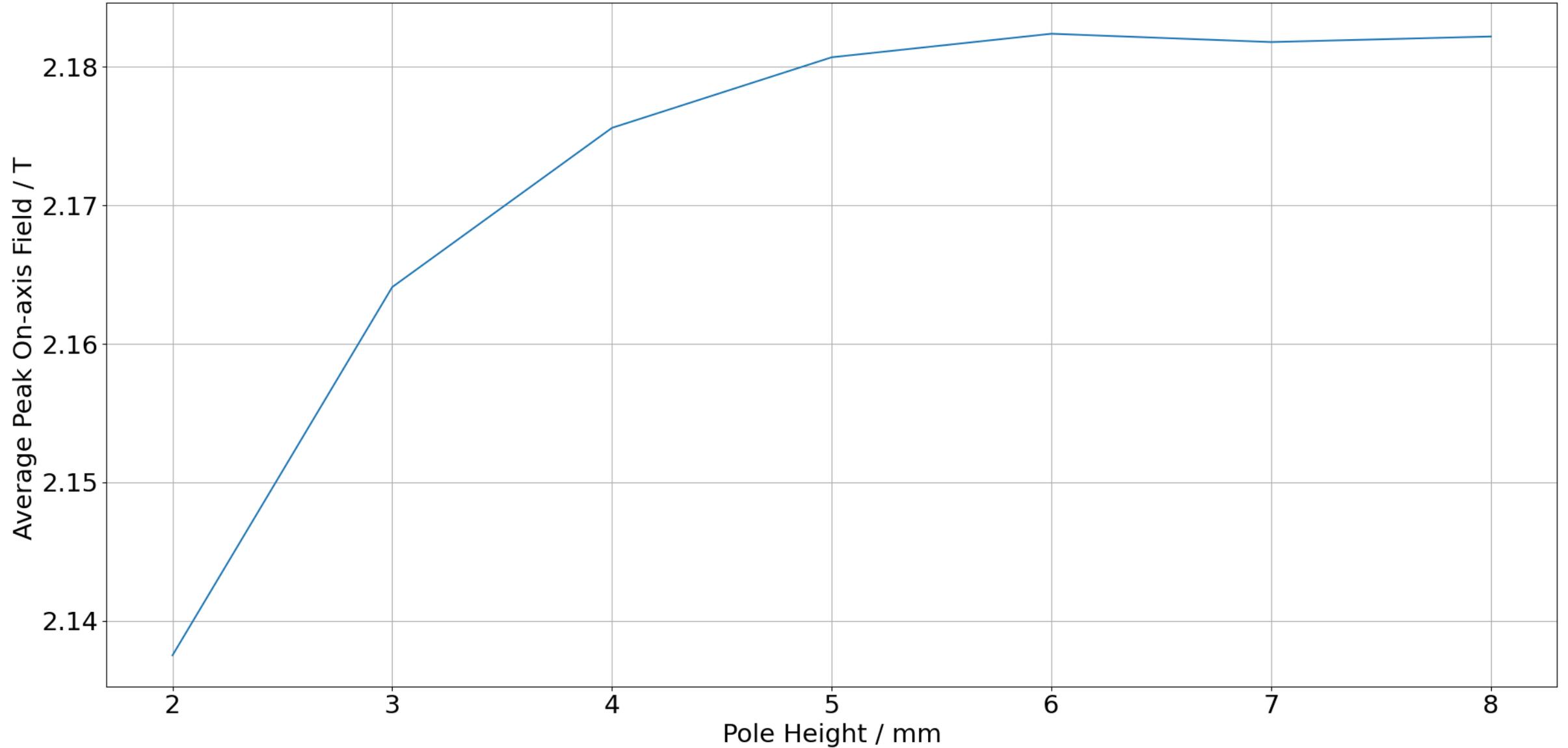
- We implemented a periodic model to optimize the ferromagnetic pole shape in order to get the maximum peak field amplitude



# Ferromagnetic pole optimization



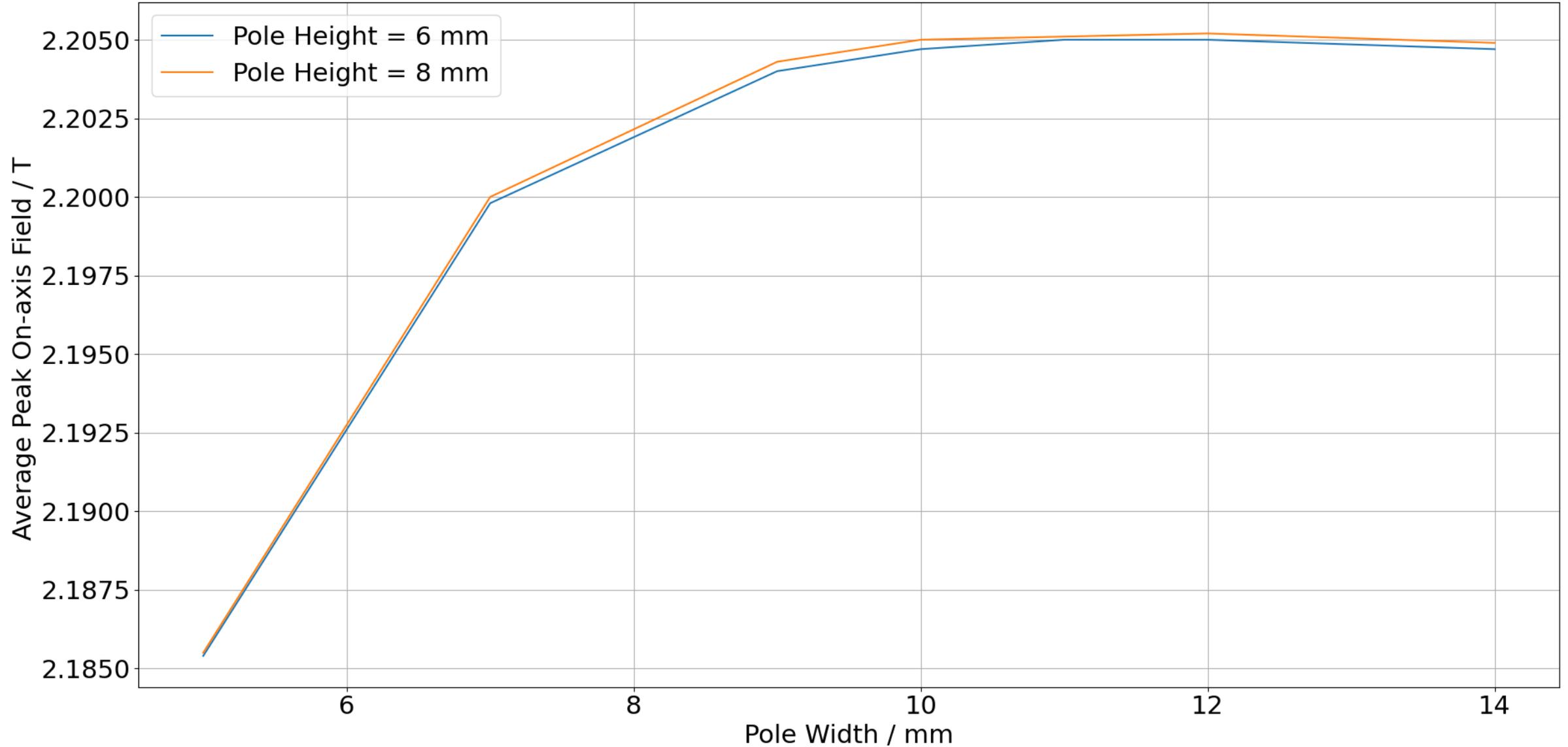
- 2D height sweep: Optimum height of 6 mm



# Ferromagnetic pole optimization

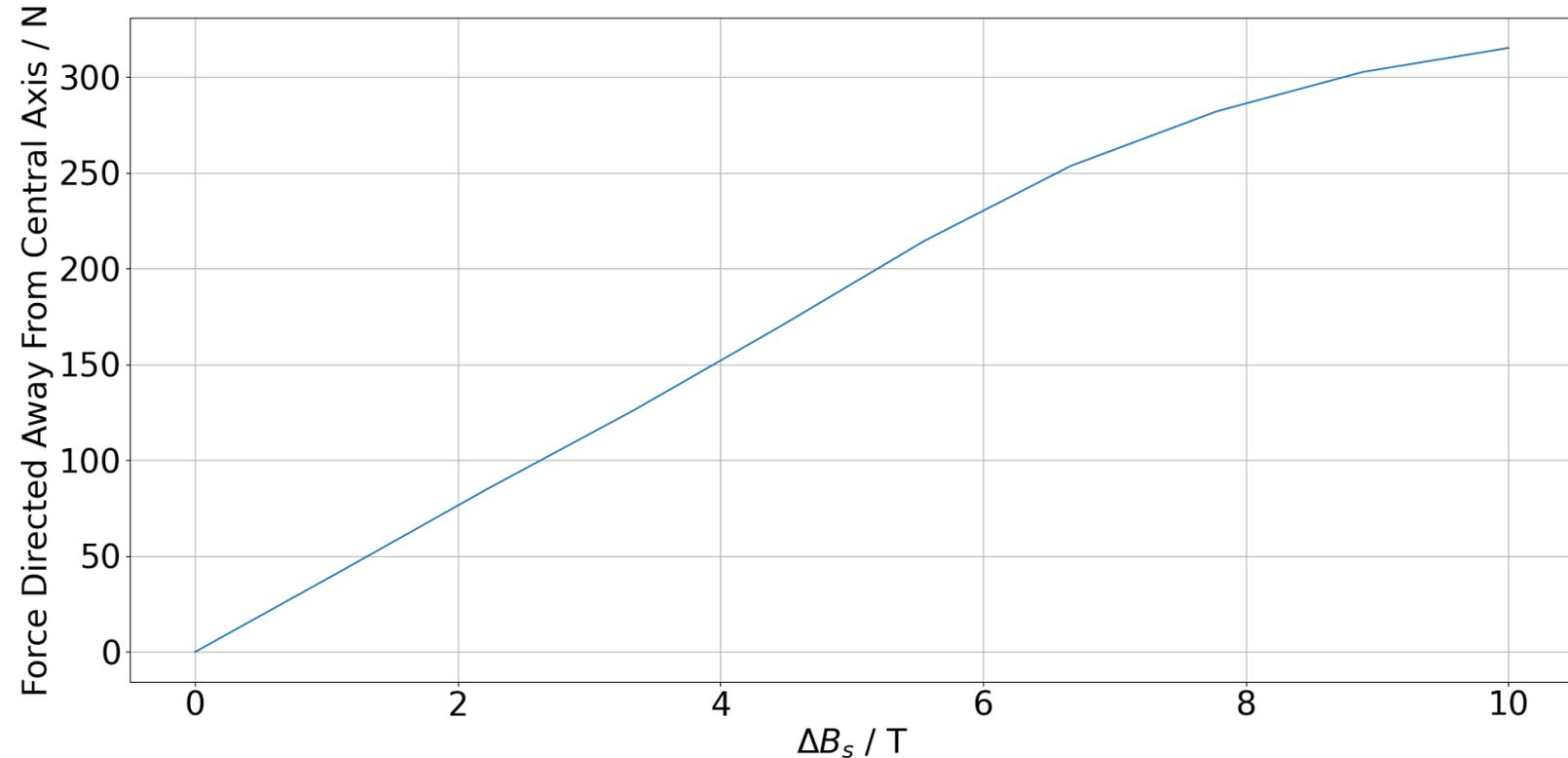
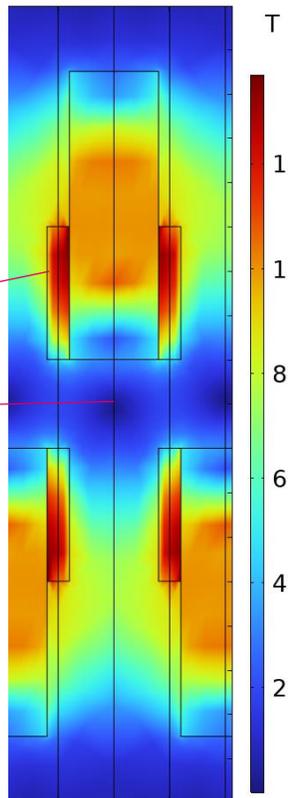
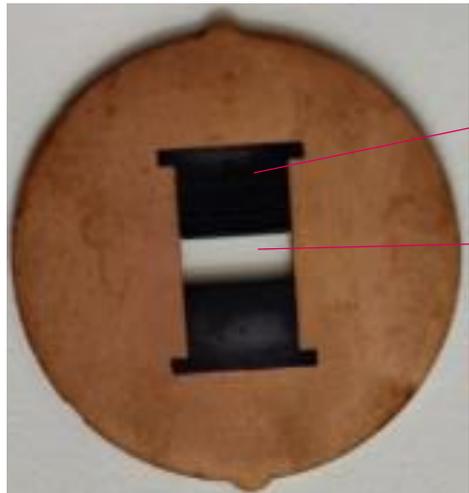


- 3D width sweep: Optimum width of 10 mm



# Ferromagnetic pole optimization

- To shim the HTSU the pole will be trimmed at the gap
- In traditional permanent magnet undulators the magnetic force pulls the poles towards the gap
- For the HTSU the opposite occurs, as the field is stronger in at the center of an HTS

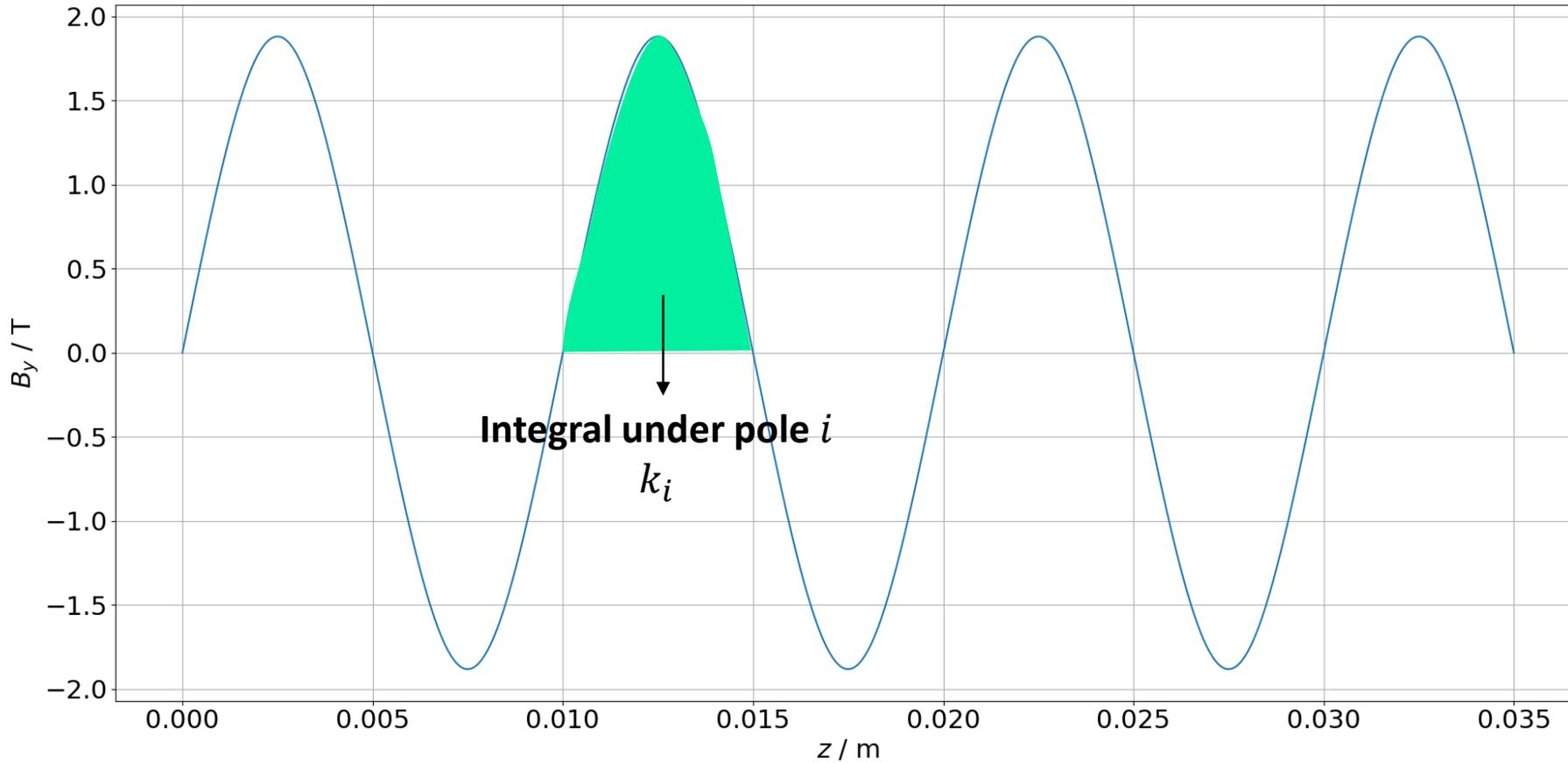


# Agenda

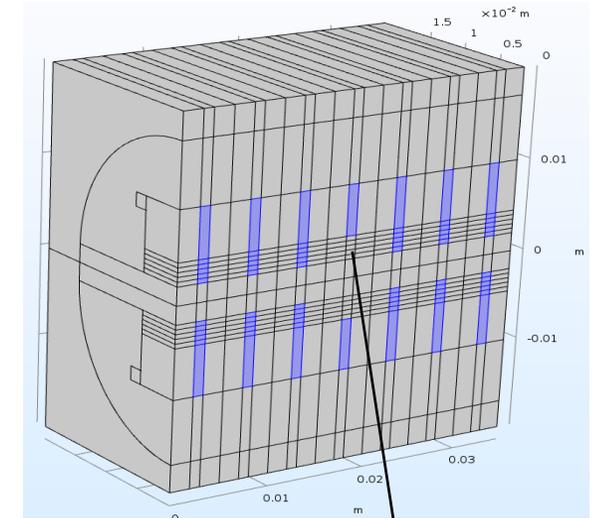


- 1 Introduction
- 2 Modelling framework
- 3 Ferromagnetic pole optimization
- 4 Ferromagnetic pole shimming**
- 5 Conclusion

# Ferromagnetic pole shimming



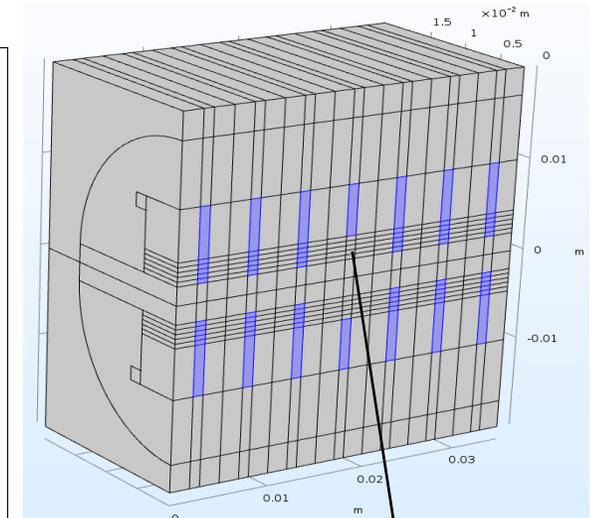
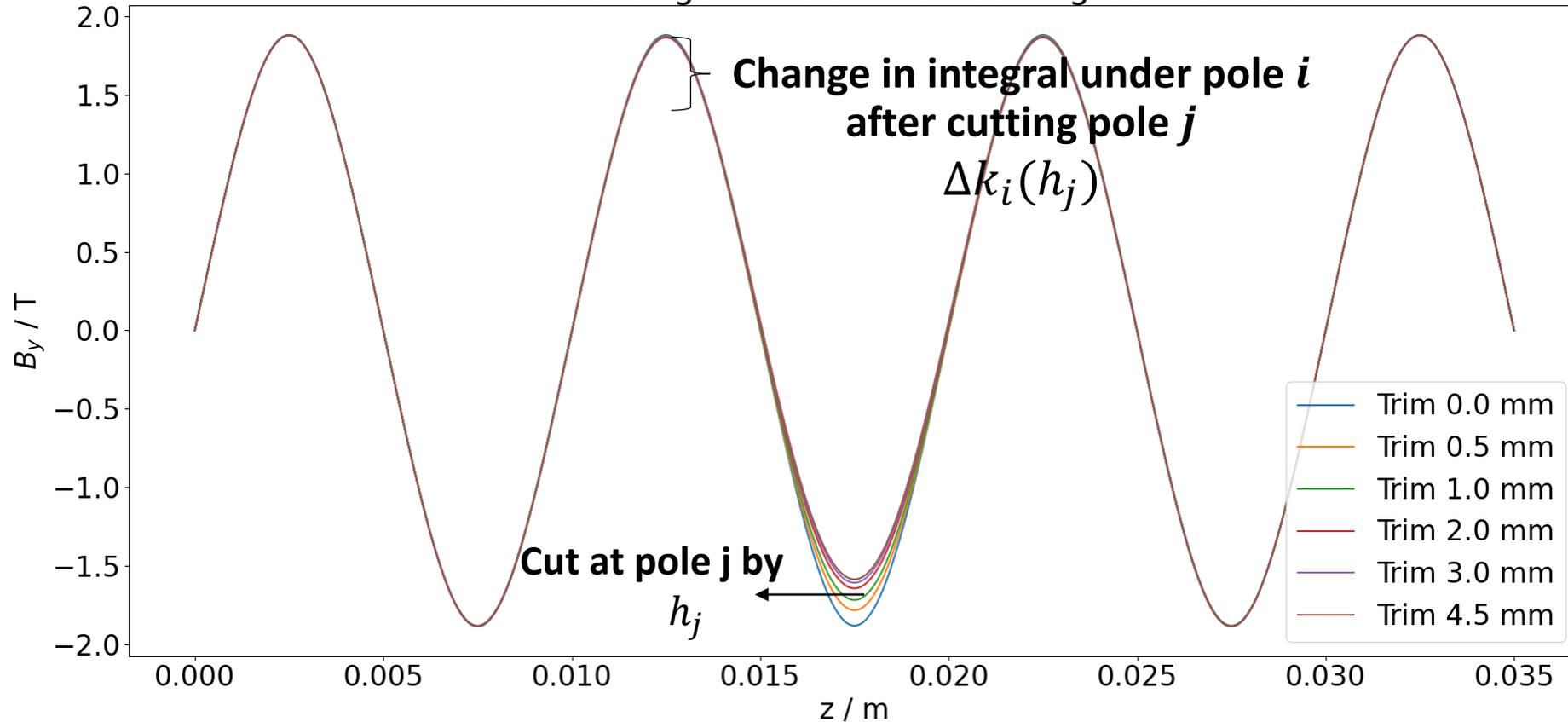
On  $-$ axis field of 3.5 Periods, with no cut;  $h_j = 0$



Simulate cut at pole  $j$   
 $h_j$

# Ferromagnetic pole shimming

Simulated Change in Field When Cutting Central Pole



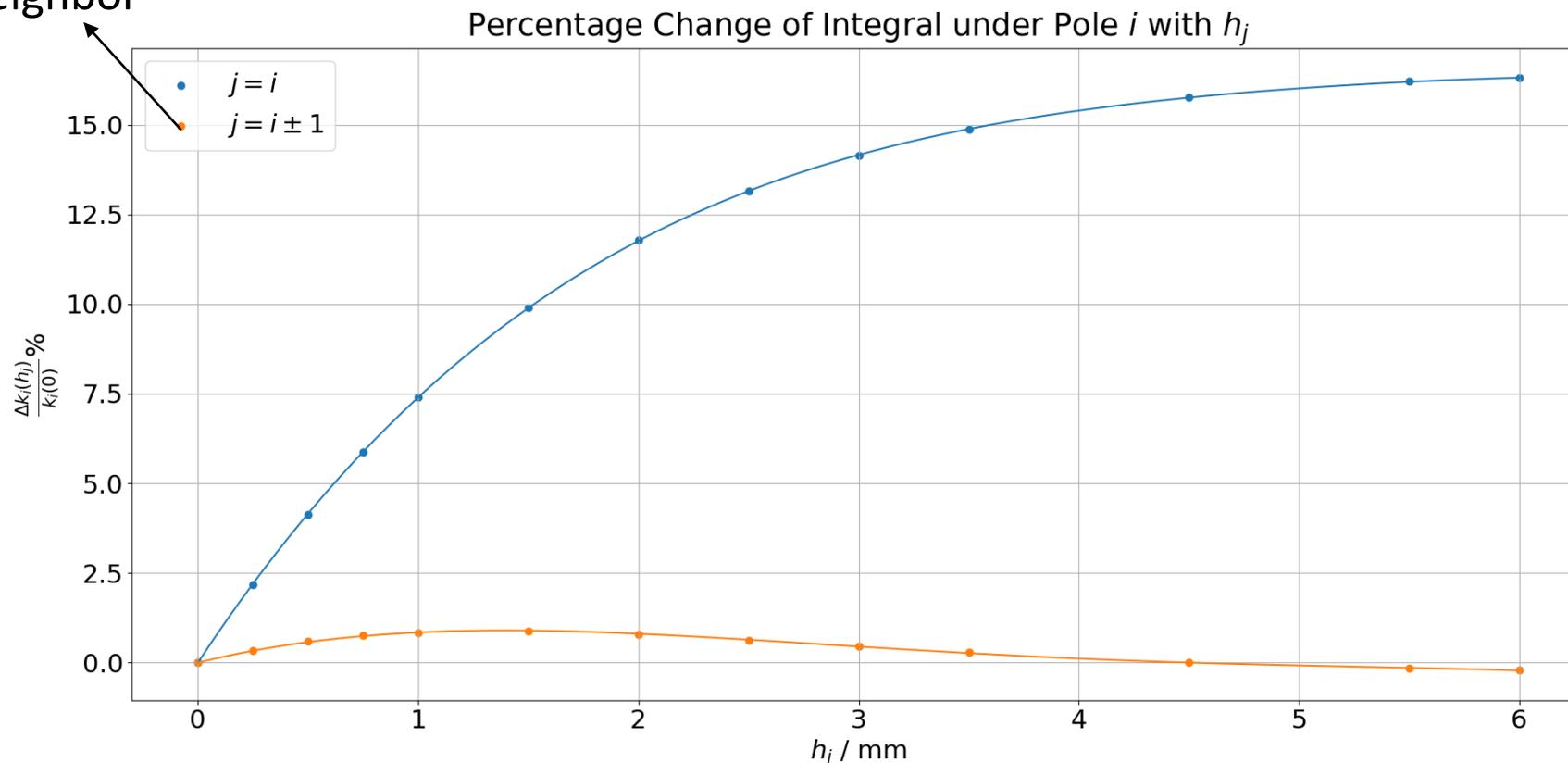
Simulate cut at pole  $j$

Assuming:  $\Delta k_i(\mathbf{h}) = \Delta k_i((0, \dots, h_{i-3}, \dots, 0)) + \dots + \Delta k_i((0, \dots, h_i, \dots, 0)) + \dots + \Delta k_i((0, \dots, h_{i+3}, \dots, 0))$

# Ferromagnetic pole shimming

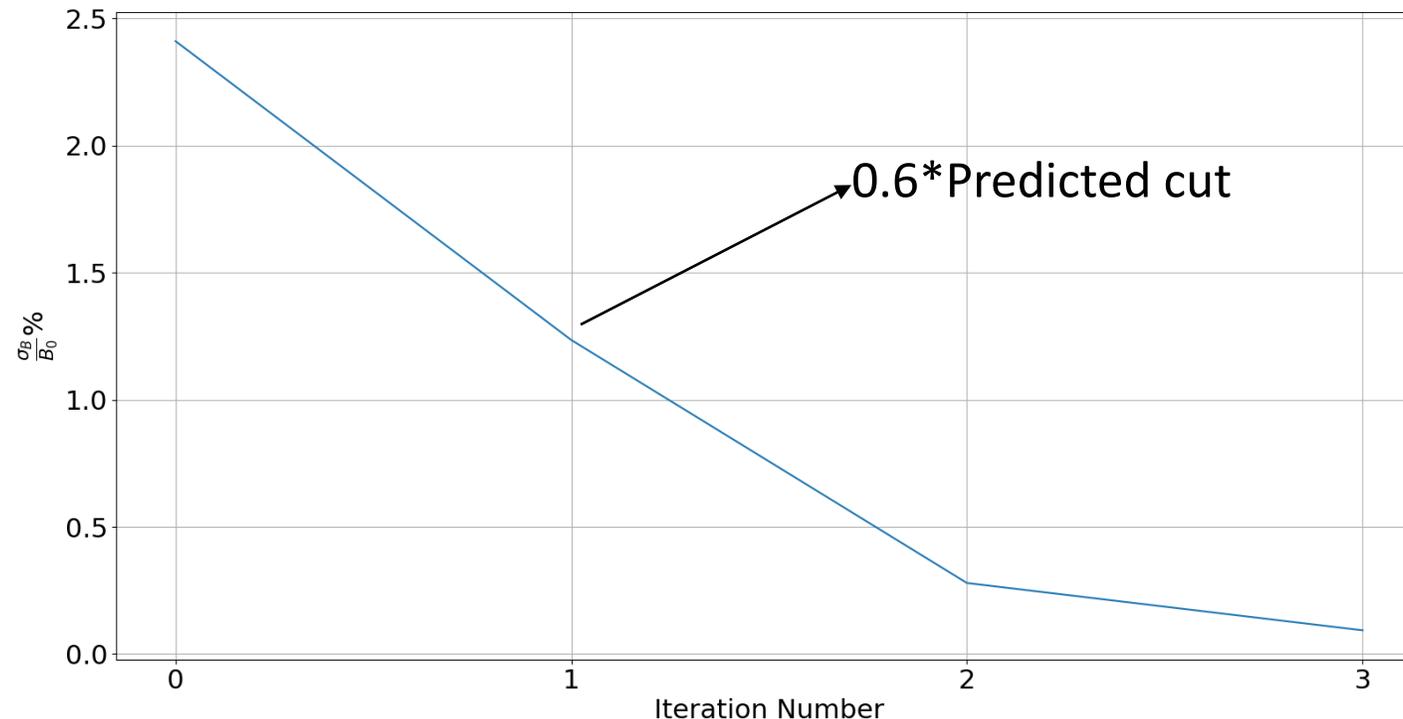
- For each pole  $i$  fit a 4<sup>th</sup> order polynomial  $a_{ij} h_j^4 + b_{ij} h_j^3 + c_{ij} h_j^2 + d_{ij} h_j = \Delta k_i$
- Use coefficients to build circulant matrices  $(\underline{A})_{ij} = a_{ij}, \dots$ , and let  $(\underline{h}) = h_j$
- The change in the integral between each two zeros  $\underline{\Delta k}$  due to a set of cuts  $\underline{h}$  is given by  $\underline{A} \underline{h}^4 + \underline{B} \underline{h}^3 + \underline{C} \underline{h}^2 + \underline{D} \underline{h} = \underline{\Delta k}(\underline{h})$

1<sup>st</sup> Neighbor



# Ferromagnetic pole shimming

- From experimental data we can obtain the first field integral of each peak,  $K_i$
- To get a uniform field we minimize  $R = \underline{K} - \text{avg}(\underline{K}) + \underline{\Delta k}(\underline{h})$  to obtain how much the poles should be cut
- With 3 iterations, we can reduce the error from 2.4% down to 0.2% by simulation
- Target: 0.1% (If all parameters between model and simulated field are the same than we can go to 0% barring mesh errors)



# Agenda



- 1 Introduction
- 2 Modelling framework
- 3 Ferromagnetic pole optimization
- 4 Ferromagnetic pole shimming
- 5 Conclusion

- The HTS undulator field is nonuniform due to the different properties of each bulk -> Need to improve the field quality
- We also optimized the shape of the HTSU poles to maximize the field amplitude
- Finally, a pole cutting algorithm was developed to predict how much each pole should be cut to improve the field quality.
- The pole shimming gives a more fine-tuned field optimization, where we show that the error can go from 2.4% to 0.2% in three iterations by simulations