

Precise Magnet Alignment for SPring-8-II and Beyond

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1. Alignment Scheme for SPring-8-II using Vibrating Wire Method, VWM

- Introduction
- Demonstration at the New 3GeV Light Source, NanoTerasu
- Magnetic Center vs. Mechanical Bore Center

2. Proposal of a New VWM for Magnet Arrays Containing Permanent Magnets

1. Introduction





Major Parameters	SPring-8-II	SPring-8
Energy (GeV)	6	8
Stored current (mA)	200	100
Circumference (m)	1435.43	1435.95
Effect. emittance (pmrad)	110~50 (with DWs)	2,400



The required alignment tolerance: $\pm 50 \mu m$ for the multipole magnets in the transverse plane.

Even smaller deviation is preferable to make the dynamic aperture as large as possible. Our goal is < $\pm 10\mu$ m or better.

T. Watanabe, SRI2024, Hamburg, Germany.



Fiscal year	2017	2018 -2022	2023	2024	2025 -2028
SPring-8-II Design/Development Restarted and Redesigned Magnet Mass Production 4/2025-6/2028 Shutdown Period 7/2027-9/2028				+ Here	← →
NanoTerasu (3GeV LS in Japan)		◀	>		







- Precise magnet alignment based on a VWM has been developed for SPring-8-II.
- The same alignment procedure was applied to NanoTerasu.
- ➢ Magnets for SPring-8-II will be aligned from 7/2026 to 6/2028.



 (1) "On-girder alignment" was performed using a VWM out of the accelerator tunnel.
 320 multipole magnets (Q and SX) on 96 common girders were aligned for 16 weeks in 4 temperature-controlled vinyl booths.
 (2) Girders were transported into the accelerator tunnel.
 SMRs on the top of the magnets were measured using a laser tracker to confirm the magnet positions.

(3) Girder-to-girder alignment was performed using a laser tracker.



When an AC is applied to a tensioned wire,

the wire vibrates in the presence of a magnetic field.

→ We can determine the magnetic profile of multipole magnets.

3700 2200 Reference line Displacement Wire Sensor Fixed End Loaded End 🗒 Weight ┍┯┝╸ ∎<mark>≓</mark> वि 2kg T ÷ x, y S⊲→X CT Sig x10 LOCK-IN GP-IB PC AMP AWG Ref AMP

• Wire :

NGK Ltd., C1720W-EHM Be-Cu, 0.2[mm]**φ**

- Tension : T = 2.0[kgf]
- Maximum sag : S_{max}=0.23[mm]
- Resonance:
 f₁=36.8[Hz]







- \checkmark Only the alignment target magnet was excited in the magnet array.
- ✓ A spurious wire oscillation due to an external field was canceled using "Sth" and "Stv".

The magnetic center of the target magnet was detected with the resolution < 0.3 μ m.





<u>Reference line</u> was defined as a straight line connecting the magnetic centers

of two end magnets of a straight section.

<u>Displacements</u> of other magnets between the two end magnets from the reference line were compensated by adjusting the magnet position with a conventional adjuster.





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Magnet alignment after the transportation was inspected

by measuring the coordinates of the SMRs on the reference plate of the magnets.



(1) Result of on-girder alignment using a VWM out of the tunnel.
 (2) Confirmation of the magnet positions after the transportation.
 (3) Girder-to-girder alignment was performed using a laser tracker.



(1) <u>Result of on-girder alignment</u>



Displacements of the magnetic centers from the reference line in the transverse plane for the 160 aligned magnets for NanoTerasu.

Displacements of the aligned magnets were successfully suppressed to within $\pm 5 \mu m!$



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(2) <u>Confirmation of the magnet positions after the transportation</u>

We inspected the magnet alignment by using a laser tracker in the tunnel.

The coordinates of SMRs on the magnet reference plate were compared before and after the transportation.

The differences were all within the alignment tolerance.

→ Re-alignment was not performed even once.





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Thanks to the excellent alignment accuracy, the well-suppressed natural COD was obtained. The root mean squares of the COD were

1.2mm in the horizontal and 0.8mm in the vertical directions without orbit correction*. *S.Obara et al., doi:10.48550/arXiv.2407.08925

1. Magnetic Center vs. Mechanical Bore Center

Mechanical Bore Center (measured by using a Coordinate Measuring Machine)

- The center of the two SMRs was defined as the origin of the x-y axes.
- The mechanical bore center was estimated by measuring the pole surfaces at upstream and downstream ends.

Magnetic Center (measured by using the VWM and a Laser Tracker)

- > The wire detected the magnetic center in the VWM.
- The wire position was measured using a laser tracker in the x-y coordinate system*.
 * See reference K. Fukami et al., Review of Scientific Instruments, 90, 054703 (2019)





1. Magnetic Center vs. Mechanical Bore Center

SPring-8

The deviations of the mechanical bore center from the magnetic center in 9 examples exceeded the alignment tolerance due to mechanical errors such as <u>a longitudinal undulation of the magnet poles.</u>



Deviations of <u>the mechanical bore</u> <u>center</u> from <u>the magnetic center</u> of magnets for NanoTerasu.

1. Magnetic Center vs. Mechanical Bore Center



The deviations of the mechanical bore center from the magnetic center in 9 examples exceeded the alignment tolerance due to mechanical errors such as <u>a longitudinal undulation of the magnet poles.</u>

- If we had applied <u>a mechanical bore center-based alignment</u>, the deviation would have contributed to the misalignment of magnets.
- We will again apply the VWM,
 - i.e. <u>a magnetic center-based alignment</u> for SPring-8-II.



Deviations of <u>the mechanical bore</u> <u>center</u> from <u>the magnetic center</u> of magnets for NanoTerasu.

1. Alignment Scheme for SPring-8-II



- <u>The same alignment procedure as we did for NanoTerasu can smoothly be applied</u> <u>to SPring-8-II with the following differences in details;</u>
- > **DQ combined function magnets** are aligned by applying a position offset on a wire.
- Permanent dipole magnets separately placed on independent girders and aligned

NB





Challenge for VWM beyond SPring-8-II

Precise alignment of magnet array involving permanent magnets (PMs).

Disadvantages of conventional VWM

- Since AC is applied to the wire, any magnetic fields from sources other than the alignment target will add spurious oscillation to the wire and result in the alignment error.
- We can subtract the spurious component from the wire oscillation data if the spurious oscillation can be accurately measured with the target turned off. However, when a PM is the target, it is impossible to turn it off.
- Including a PM-based DQ magnet in the alignment will result in a significant spurious oscillation that is difficult to subtract correctly.

We propose <u>a new VWM</u> that enables a precise magnet alignment in the presence of PMs in the same girder.



Field Modulated VWM (FM-VWM)

- <u>A DC</u> is applied to the tensioned wire.
- The target magnet is excited by <u>an AC with a resonance frequency of wire vibration</u>.
 - → An external field does <u>NOT</u> generate a spurious wire oscillation.
- **1.** The FM-VWM can be applied to a group containing permanent magnets.
- 2. A permanent magnet can also be aligned by adding an extra AC field.



Test magnet array for proof-of-principle experiments for FM-VWM using electromagnets.

SPring. 8

Proof-of-principle Experiments

1. Accuracy of magnetic-center measurement

The magnetic center of the target quadrupole magnet was measured with two methods, conventional VWM and FM-VWM.

2. Effect of an external multipole magnetic field

A misaligned extra quadrupole magnet was involved and excited by a DC to simulate a permanent quadrupole magnet.

3. Magnetic center of a simulated permanent magnet.

Alignment target quadrupole magnet was excited by a DC

to simulate a permanent quadrupole magnet.

The magnetic center of the target magnet was measured with FM-VWM by superimposing an AC excitation.



1. Accuracy of magnetic-center measurement

FM-VWM:

Wire DC0.056A, Q1 AC0.03T_{rms} Conventional VWM:

Wire AC0.056A_{rms}, Q1 DC0.03T + Sth, Stv*

* Spurious wire oscillation (1µm)

-> Error of magnetic-center (3.7µm)





Wire vibration amplitude versus wire position in the transverse plane.

The FM-VWM can detect the magnetic center correctly without canceling spurious wire oscillations that disturbed the conventional VWM.

2. Effect of an external multipole magnetic field

A misaligned extra quadrupole magnet was involved and excited by a DC to simulate a permanent quadrupole magnet.



Conventional VWM is useless in the presence of external multipole field, e.g. by permanent quadrupole magnets.

SPring

Horizontal



2. Effect of an external multipole magnetic field

FM-VWM





The FM-VWM can measure the magnetic center correctly even if there is an external multipole field, e.g., by permanent quadrupole magnets.



Vertical

3. Magnetic center of a simulated permanent magnet





Horizontal

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The FM-VWM can measure the magnetic center of a permanent quadrupole magnet!



<u>Notes</u>

 <u>1: The presence of strong dipole fields, e.g., permanent DQ magnets</u>
 The wire moves by Lorentz's force due to an interaction between a direct current and a static magnetic field.
 Correcting the wire movement like a wire sag is necessary when it is not negligible.

<u>2: Frequency dependence of the alignment target magnets</u></u>

No field attenuation and delay were observed up to 100Hz in the test magnets because their iron cores are made of a laminated sheet with a thickness of 0.5mm. We recommend a laminated core for permanent magnets and electromagnets if FM-VWM is applied.



Magnet Alignment for SPring-8-II

- Our alignment scheme for SPring-8-II has been successfully applied to NanoTerasu and the adequately precise alignment was verified from the natural COD.
- > We will apply it to coming SPring-8-II with some improvements in the detailed procedure.

New VWM

- We propose a new alignment scheme that can precisely align magnet arrays in the presence of permanent magnets along the wire.
- > The new VWM we proposed will expand the scope of VWM for future accelerators.