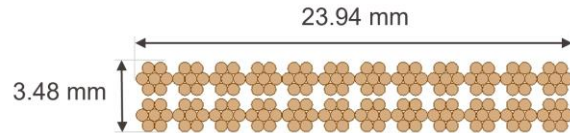


Conductor layout:



Strand diameter	0.7 mm
Copper-noncopper ratio	1
RRR	150
Number of strands	$24 \times 7 = 168$
Total width	24.34 mm
Total height	3.88 mm
Insulation thickness	0.2 mm

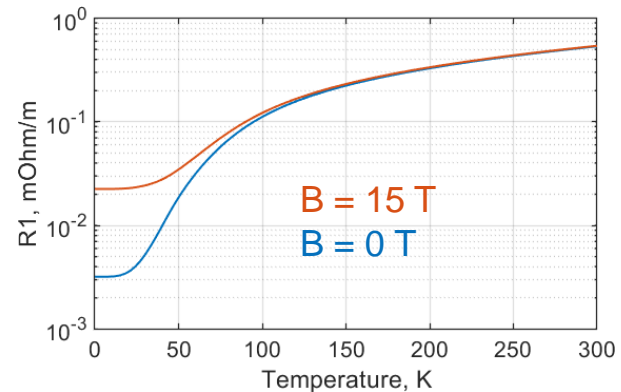
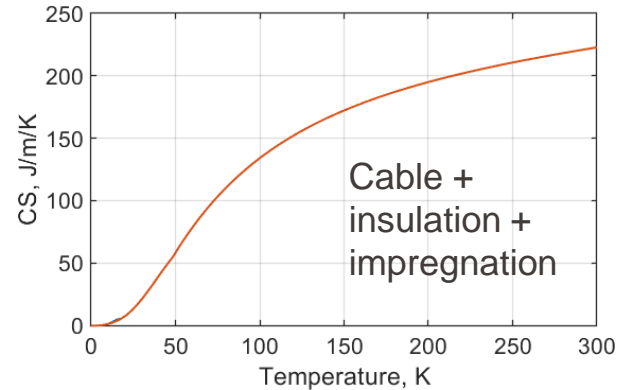
Conductor cross-section	94.4 mm <sup>2</sup>
Cable	64.7 mm <sup>2</sup> (68.5%)
Copper	32.3 mm <sup>2</sup> (34.2%)
Noncopper	32.3 mm <sup>2</sup> (34.2%)
Impregnation	18.7 mm <sup>2</sup> (11.8%)
Insulation	11.1 mm <sup>2</sup> (19.8%)

Operating current	18 kA
J eng	182 A/mm <sup>2</sup>
J cu	533 A/mm <sup>2</sup>
Inductance	0.13 H
Stored energy	21.1 MJ
Discharge voltage (max)	1 kV
Time constant $\tau$	2.34 s
Delay time $t_d$	16 ms

Adiabatic analysis:

$$C(T)S \frac{\partial T}{\partial t} = I^2 R_1(T, B) \text{ [W/m]}$$

- Conductor cross-section isothermal
- Current flow in copper
- Size of normal zone to reach 100 mV at 18 kA:  
1.7 m (0 T), 0.2 m (15 T)
- $T(t = 0) = 8 \text{ K}$ :  
 $T_{max} = 397 \text{ K}$  at  $B = 0 \text{ T}$  constant  
 $T_{max} = 1090 \text{ K}$  at  $B = 15 \text{ T}$  constant  
 $T_{max} = 1060 \text{ K}$  for  $B = k \times I$
- $I = 17 \text{ kA}$ ,  $V = 1.5 \text{ kV}$ ,  $\tau = 1.47 \text{ s}$ :  
 $T_{max} = 100 \text{ K}$  at  $B = 0 \text{ T}$  constant  
 $T_{max} = 262 \text{ K}$  at  $B = 15 \text{ T}$  constant  
 $T_{max} = 243 \text{ K}$  for  $B = k \times I$



Constant B:

- $Z(T) = \int_{T_0}^T \frac{c(x)S}{R_1(x,B)} dx$

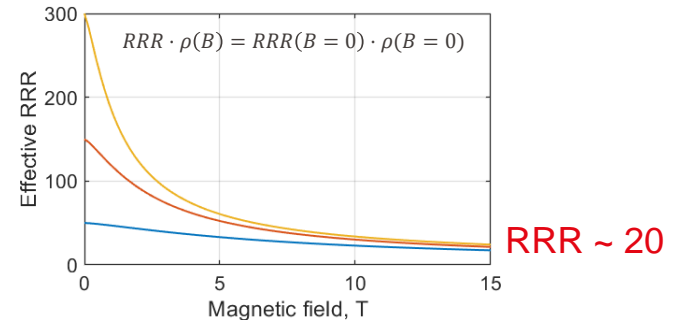
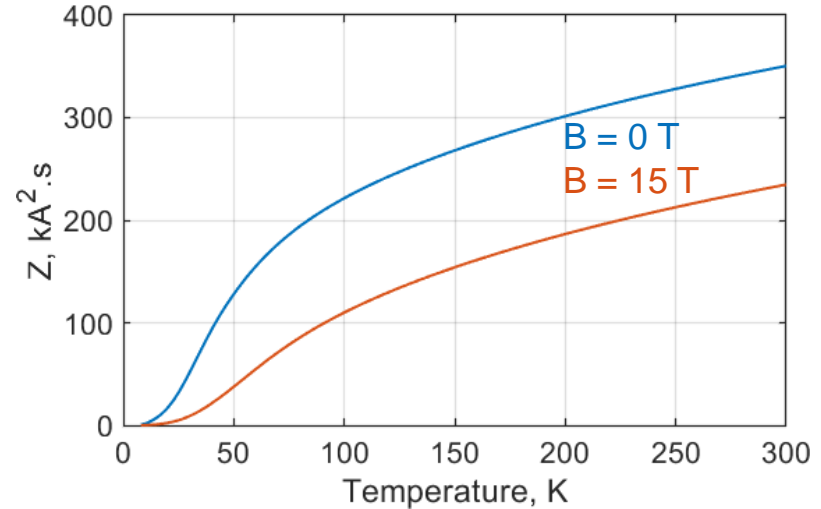
- Quench integral:

$$\int I^2 dt = I^2(t_d + \tau/2) \approx EI/V = LI^3/2V$$

$$= 384 \text{ kA}^2 \cdot \text{s at } 18 \text{ kA, } 1.0 \text{ kV}$$

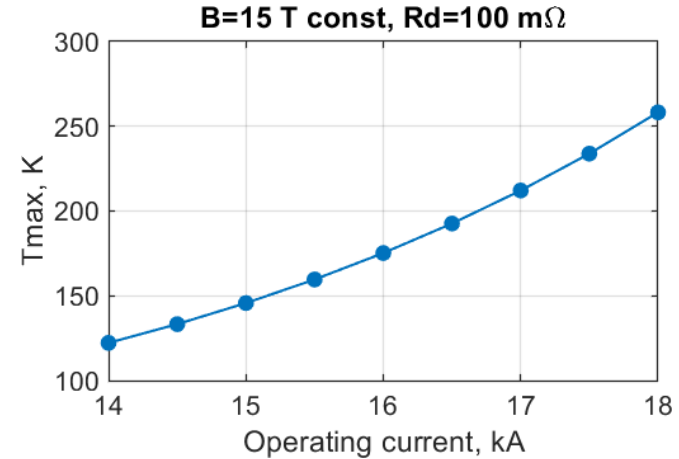
$$= 218 \text{ kA}^2 \cdot \text{s at } 17 \text{ kA, } 1.5 \text{ kV}$$

- Cross-check the actual effect of magnetoresistance?
- 3-D model to be prepared to quantify impact of thermal conductivity in transverse and longitudinal directions, though strong impact on T<sub>max</sub> is not expected

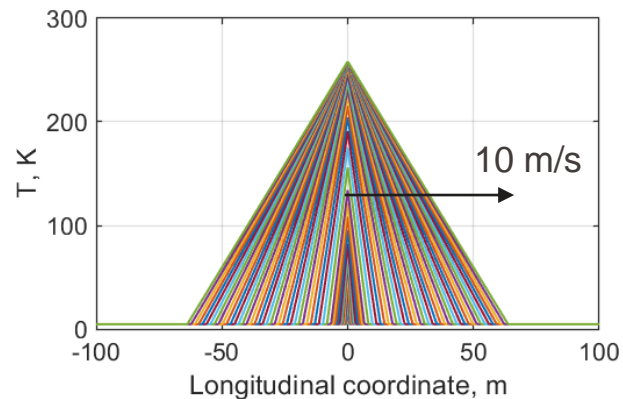
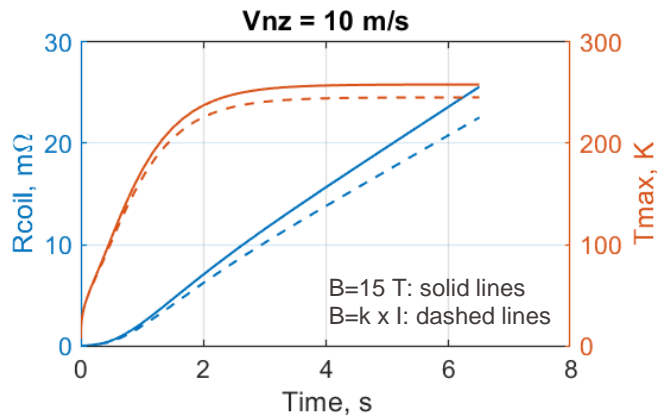
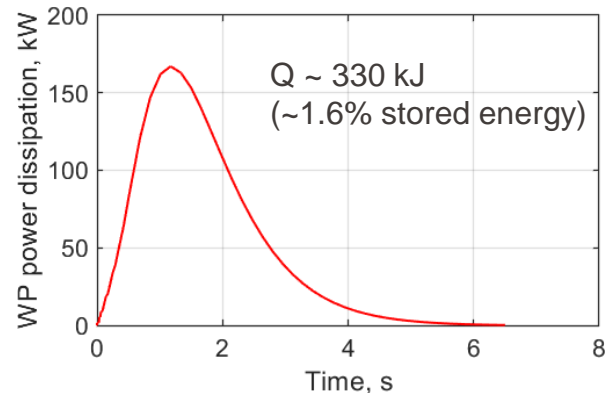
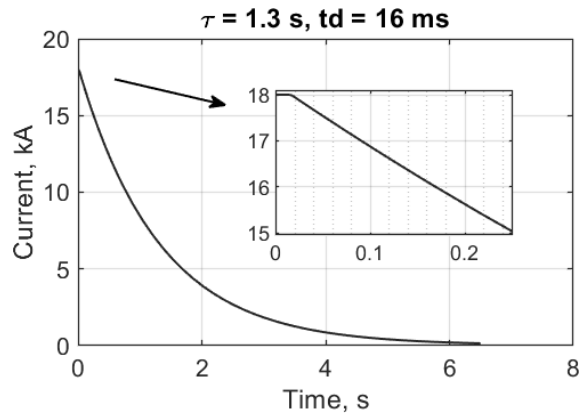


Rd, mΩ	<b>100</b>	
$\tau$ , s	1.3	
I, kA	18.0	17.0
E, MJ	21.1	18.8
V, kV	1.8	1.7
Tmax*, K	258	212

\* @ B = 15 T constant



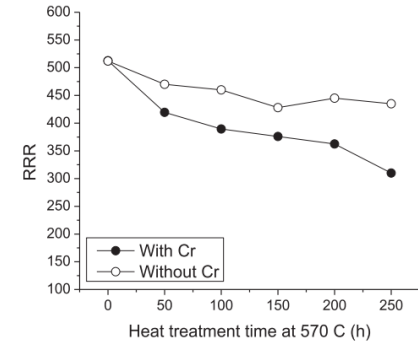
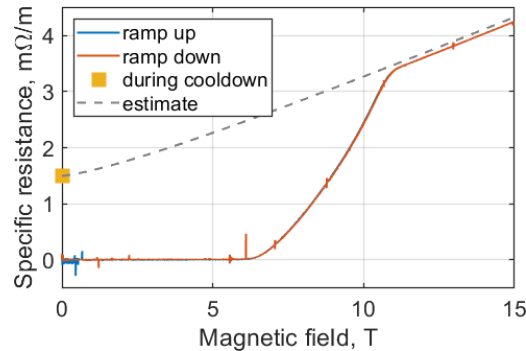
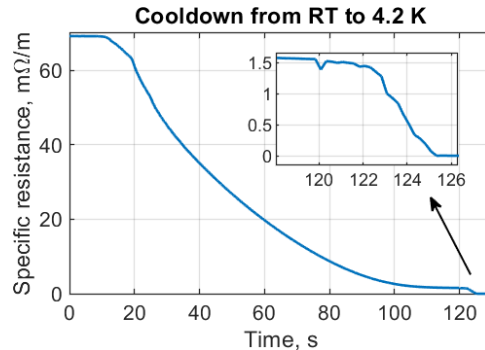
# Quench analysis: OD estimate



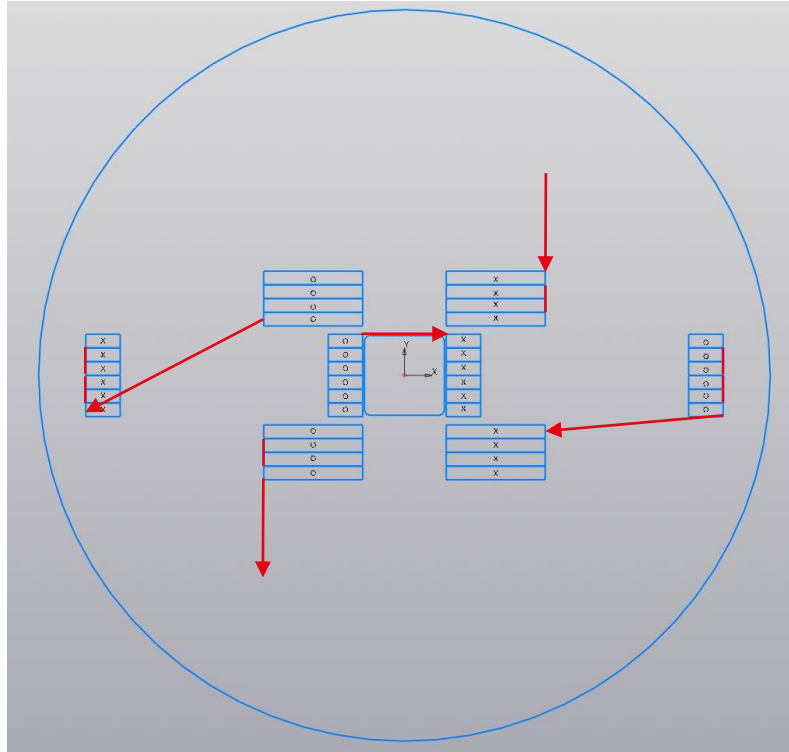
Neglected terms so far:

- Thermal conductivity in longitudinal and transverse direction → lower  $T_{\max}$
- AC loss heating due to  $B\dot{d}$ , thus faster current decay → lower  $T_{\max}$
- Higher resistance due to  $R_{\text{coil}}$ , thus faster current decay → lower  $T_{\max}$
- Impact of iron on coil inductance during quench? ~20% higher  $L$  at low  $B$ ?

- OD 0.7 mm, cnc  $\sim 1.2$ , Scu 0.21 mm<sup>2</sup>, RRR Likely 50-100, but best effort
- Resistance estimate for RRR = 50:  
 $\sim 80 \text{ m}\Omega/\text{m}$  at 293 K  $\rightarrow \sim 1.5 \text{ m}\Omega/\text{m}$  at 4 – 20 K  $\rightarrow \sim 4.3 \text{ m}\Omega/\text{m}$  at 4 K, 15 T
- Measurements on **non-reacted** 0.5 m-long sample
- Impact of heat-treatment...



**Figure 6.** RRR of the JASTEC strand as function of heat treatment time at 570 °C (first step) for samples with and without plated Cr.



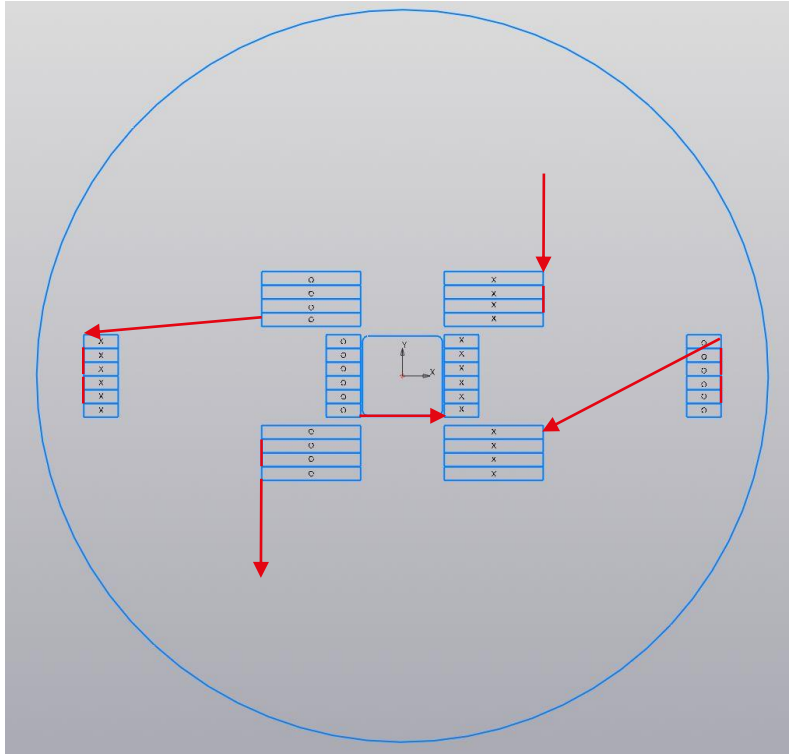
Coil splicing layout?

Cooling interface?



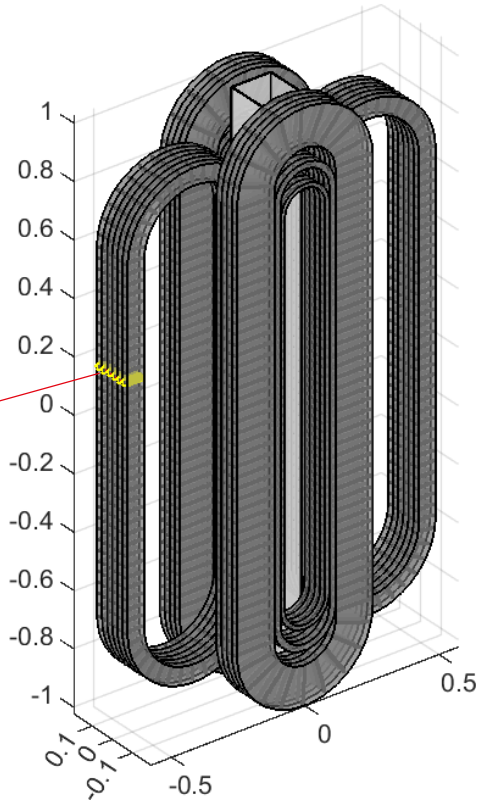
0.099609	{V threshold LF Cable}	[Volt]
0.099609	{V threshold HF Cable}	[Volt]
0.120117	V threshold Current leads Warm Side [Volt]	[Volt]
0.009766	V threshold Current leads Cold Side	[Volt]
0.049805	V threshold Bus Bar Jumper	[Volt]
10	UTV Threshold	[Volt]
800	Req Sampling Freq	(Hz)
800	Applied Sampling Freq	(Hz)
40	Req Total Validation Time	(ms)
39.75	Applied Total Validation Time	(ms)
11	ASOT thr (1 - 100)	#
14	Raw Validation Time	(ms)
1	Fir 16 On ?	0 Off; 1 On.
1	LPF Filter On ?	0 Off; 1 On.
35	Ft LPF	(Hz)
16	FIR delay	(ms)
10	LPF Delay	(ms)
0.21582	a0	0 <= a0 <= 1
60	Pre Trigger	(sec)
10	Post Trigger	(sec)
1000000	Init Time	(uSec)
1000000	Pulse duration	(uSec)
2	Current State	0 Init; 1 Autocal; 2 Reading; 3 Quench; 4 Post Trigger; 5 End
1250	Requested T Sampling	(uSec)
1250	Real T Sampling	(uSec)

+ few ms to open circuit breakers



### Setting up 3-D quench model:

- Geometry import
- Matrix of mutual inductances
- Magnetic field incl. iron (by Xabier)
- Current sharing, Tcs distribution
- Heat equation



### Geometry:

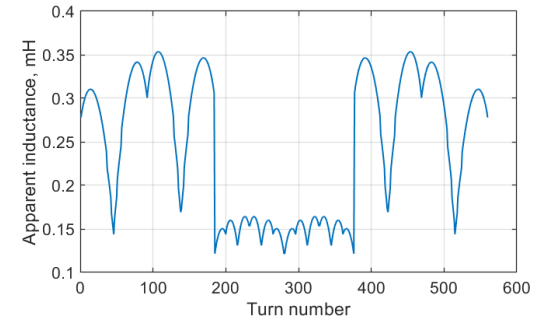
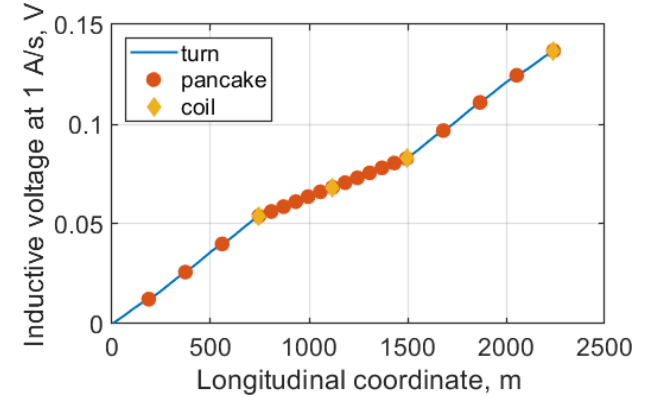
- 20 pancakes (4 per vertical, 6 per side coils)
  - 560 turns (46 per vert. pancake, 16 per side pancake)
  - 100 nodes per turn
- 56'000 nodes to evaluate heat equation

Inductance:

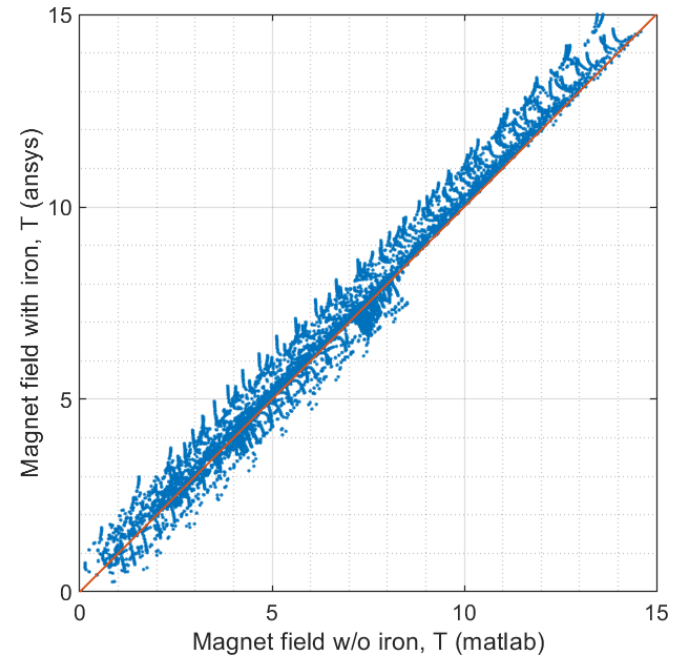
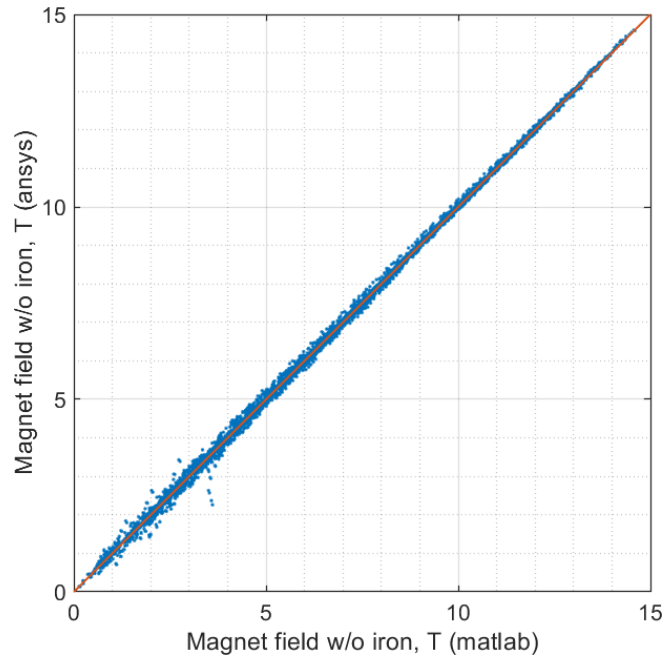
- Magnet: 137 mH
- Coil: 4 x 4 matrix
- Pancake: 20 x 20 matrix
- Turn: 560 x 560 matrix  
(Average value = 0.44  $\mu$ H, max value = 9.93  $\mu$ H, min value = -0.21  $\mu$ H)

	1	2	3	4
1	43.7290	0.0297	0.0297	10.1622
2	0.0297	15.5806	-1.2102	0.0297
3	0.0297	-1.2102	15.5806	0.0297
4	10.1622	0.0297	0.0297	43.7290

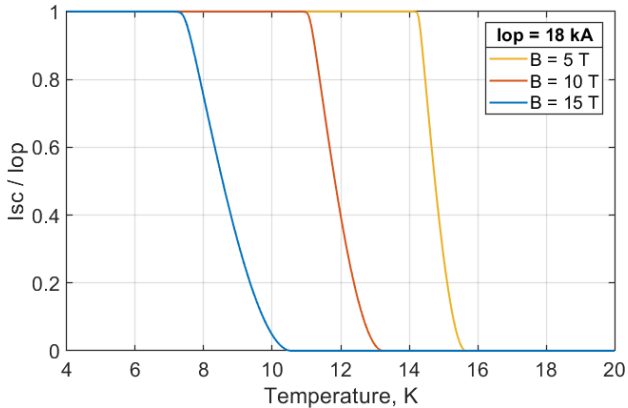
	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20
1	3.5317	2.7587	2.2960	1.9329	0.0110	-0.0109	-0.0273	-0.0393	-0.0479	-0.0540	-0.0540	-0.0479	-0.0393	-0.0273	-0.0109	0.0110	0.6208	0.5538	0.4962	0.4464
2	2.7587	3.5317	2.7587	2.2960	0.0400	0.0110	-0.0109	-0.0273	-0.0393	-0.0479	-0.0479	-0.0393	-0.0273	-0.0109	0.0110	0.0400	0.6990	0.6208	0.5538	0.4962
3	2.2960	2.7587	3.5317	2.7587	0.0784	0.0400	0.0110	-0.0109	-0.0273	-0.0393	-0.0393	-0.0273	-0.0109	0.0110	0.0400	0.0784	0.7910	0.6990	0.6208	0.5538
4	1.9329	2.2960	2.7587	3.5317	0.1293	0.0784	0.0400	0.0110	-0.0109	-0.0273	-0.0273	-0.0109	0.0110	0.0400	0.0784	0.1293	0.8997	0.7910	0.6990	0.6208
5	0.0110	0.0400	0.0784	0.1293	0.7086	0.4841	0.3838	0.3160	0.2664	0.2282	-0.0275	-0.0301	-0.0324	-0.0342	-0.0353	-0.0357	-0.0273	-0.0393	-0.0479	-0.0540
6	-0.0109	0.0110	0.0400	0.0784	0.4841	0.7086	0.4841	0.3838	0.3160	0.2664	-0.0301	-0.0324	-0.0342	-0.0353	-0.0357	-0.0342	0.0110	-0.0109	-0.0273	-0.0393
7	-0.0273	-0.0109	0.0110	0.0400	0.3838	0.4841	0.7086	0.4841	0.3838	0.3160	-0.0324	-0.0342	-0.0353	-0.0357	-0.0353	-0.0342	0.0110	-0.0109	-0.0273	-0.0393
8	-0.0393	-0.0273	-0.0109	0.0110	0.3160	0.3838	0.4841	0.7086	0.4841	0.3838	-0.0342	-0.0353	-0.0357	-0.0353	-0.0342	-0.0324	0.0400	0.0110	-0.0109	-0.0273
9	-0.0479	-0.0393	-0.0273	-0.0109	0.2664	0.3160	0.3838	0.4841	0.7086	0.4841	-0.0353	-0.0357	-0.0353	-0.0342	-0.0301	0.0784	0.0400	0.0110	-0.0109	-0.0273
10	-0.0540	-0.0479	-0.0393	-0.0273	0.2282	0.2664	0.3160	0.3838	0.4841	0.7086	-0.0357	-0.0353	-0.0342	-0.0324	-0.0301	0.1293	0.0784	0.0400	0.0110	-0.0109
11	-0.0540	-0.0479	-0.0393	-0.0273	-0.0275	-0.0301	-0.0324	-0.0342	-0.0353	-0.0357	0.7086	0.4841	0.3838	0.3160	0.2664	0.2282	0.1293	0.0784	0.0400	0.0110
12	-0.0479	-0.0393	-0.0273	-0.0109	-0.0301	-0.0324	-0.0342	-0.0353	-0.0357	-0.0353	0.4841	0.7086	0.4841	0.3838	0.3160	0.2664	0.0784	0.0400	0.0110	-0.0109
13	-0.0393	-0.0273	-0.0109	0.0110	-0.0324	-0.0342	-0.0353	-0.0357	-0.0353	-0.0342	0.3838	0.4841	0.7086	0.4841	0.3838	0.3160	0.0400	0.0110	-0.0109	-0.0273
14	-0.0273	-0.0109	0.0110	0.0400	-0.0342	-0.0353	-0.0357	-0.0353	-0.0342	0.3160	0.3838	0.4841	0.7086	0.4841	0.3838	0.2664	0.0110	-0.0109	-0.0273	-0.0393
15	-0.0109	0.0110	0.0400	0.0784	-0.0353	-0.0357	-0.0353	-0.0342	-0.0324	0.2664	0.3160	0.3838	0.4841	0.7086	0.4841	0.1293	0.0784	-0.0109	-0.0273	-0.0393
16	0.0110	0.0400	0.0784	0.1293	-0.0357	-0.0353	-0.0342	-0.0324	-0.0301	-0.0275	0.2282	0.2664	0.3160	0.3838	0.4841	0.0784	-0.0273	-0.0393	-0.0479	-0.0540
17	0.6208	0.6990	0.7910	0.8997	-0.0273	-0.0109	0.0110	0.0400	0.0784	0.1293	0.1939	0.2664	0.3160	0.3838	0.4464	0.4962	0.5538	0.6208	0.6990	0.7910
18	0.5538	0.6208	0.6990	0.7910	-0.0393	-0.0273	-0.0109	0.0110	0.0400	0.0784	0.0784	0.0784	0.0400	0.0110	-0.0109	-0.0273	-0.0393	2.7587	3.5317	2.7587
19	0.4962	0.5538	0.6208	0.6990	-0.0479	-0.0393	-0.0273	-0.0109	0.0110	0.0400	0.0400	0.0110	-0.0109	-0.0273	-0.0393	-0.0479	2.2960	2.7587	3.5317	2.7587
20	0.4464	0.4962	0.5538	0.6208	-0.0540	-0.0479	-0.0393	-0.0273	-0.0109	0.0110	0.0110	-0.0109	-0.0273	-0.0393	-0.0479	-0.0540	1.9329	2.2960	2.7587	3.5317



## Magnetic field within the coil winding (over 56'000 nodes)



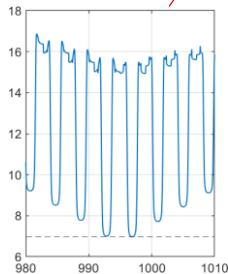
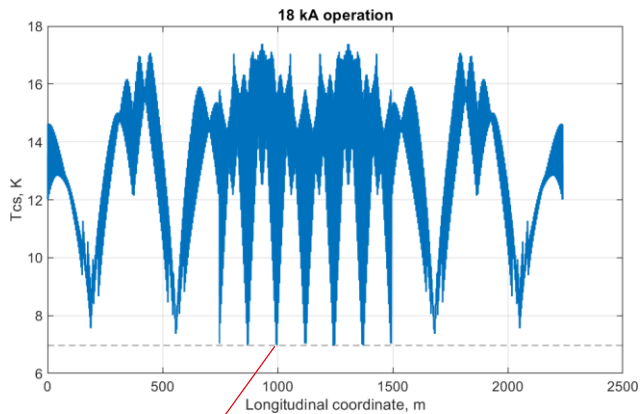
### Current sharing at 18 kA operation



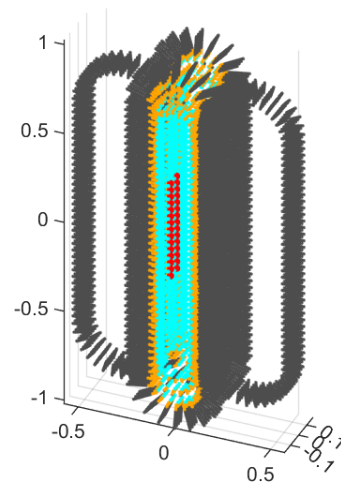
$$\eta_{st} \frac{I_i - I_{sc}}{A_{st}} = E_0 \left( \frac{I_{sc}}{I_c} \right)^n \quad I_{st} = I_i - I_{sc}$$

Intra-strand resistance neglected

### Tcs distribution along conductor length



min Tcs = 6.97 K



Tcs < 11 K

Tcs < 9 K

Tcs < 7 K

Heat equation:

$$C \frac{\partial T}{\partial t} = q_{joule} + \frac{\partial}{\partial x} \left( k \frac{\partial T}{\partial x} \right) + q_{trans} - q_{cooling} + q_{external} \text{ [W/m}^3\text{]}$$

```

for i=1:N1
    Ti=T(i,:);
    h1=h_face(Ti);
    h2=h_side(Ti);
    q_trans(i,:)=sum((C_face.*(h1+h1')/2+C_side.*(h2+h2')/2).*(Ti'-Ti),1);
end

qface(coolingface)=h_face(T(coolingface)).*(T(coolingface)-4.2);
qside(coolingside)=h_side(T(coolingside)).*(T(coolingside)-4.2);
q_cooling=qface+qside;

if t>=heater_t(1) && t<=heater_t(2) && ~quench
    q_heater(heater_pos)=P; %W/m
end

```

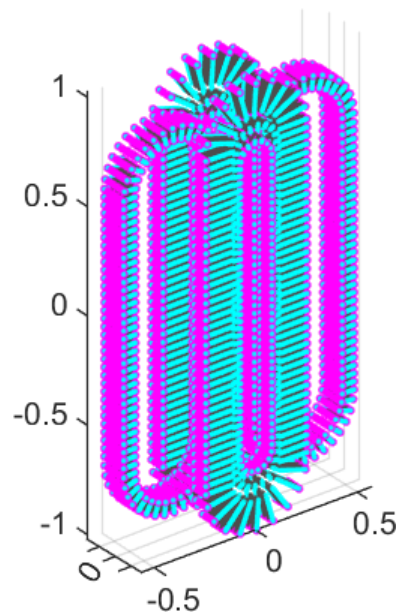
Connectivity matrices for nodes  
in the same cross-section

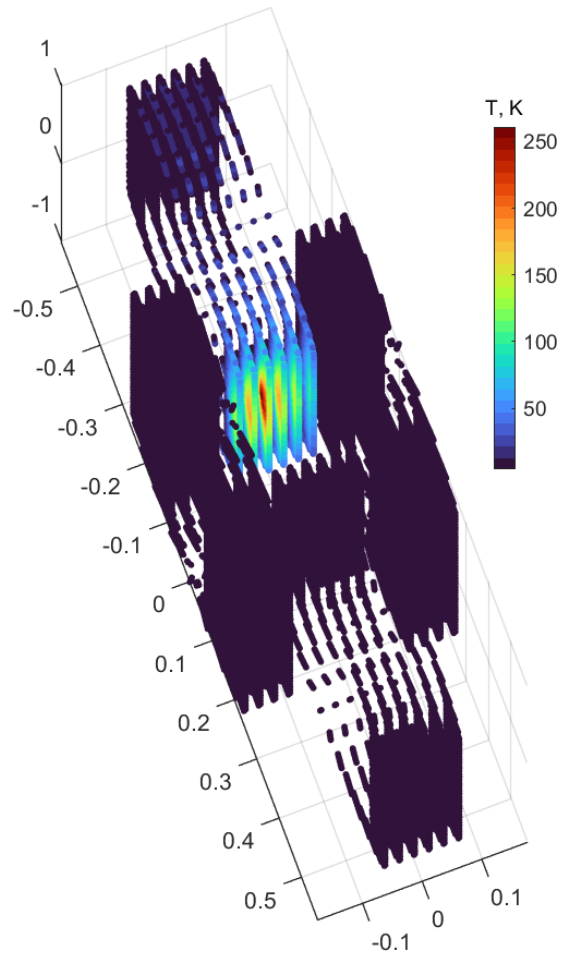
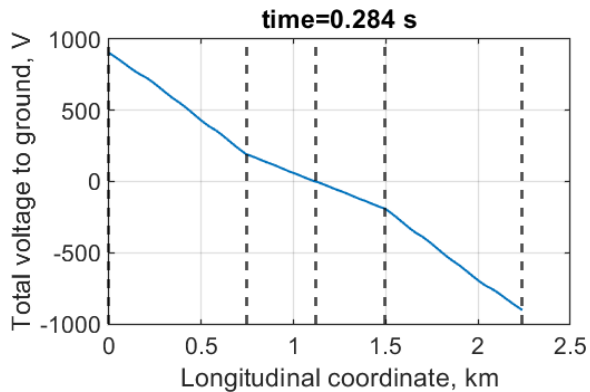
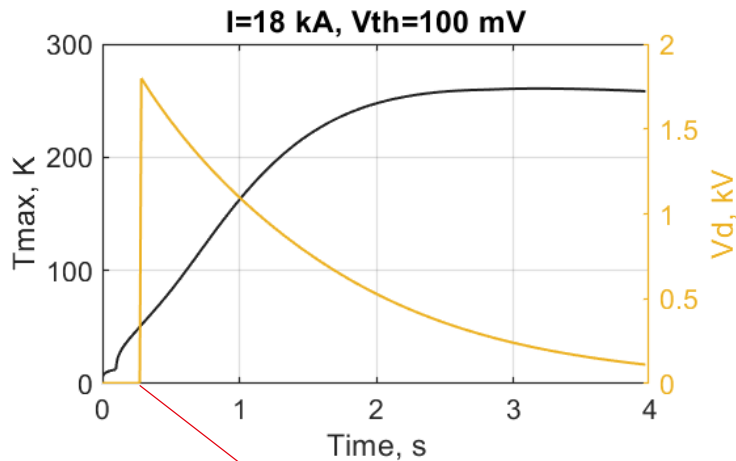
Current discharge once 'quench is detected' ( $t_d = 0.1$  s):

$$L \frac{\partial I}{\partial t} = -V_{coil} - IR_d$$

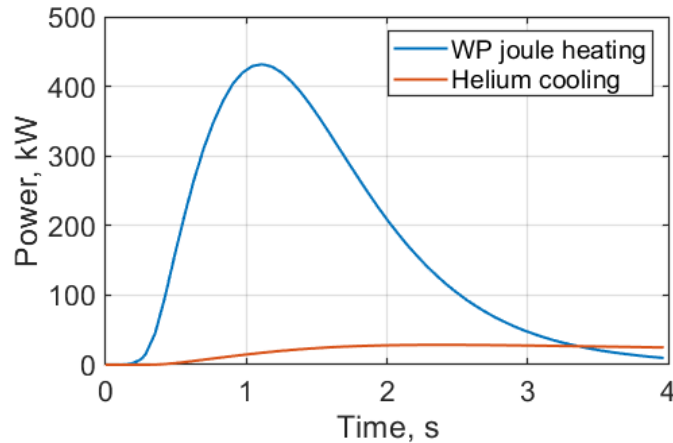
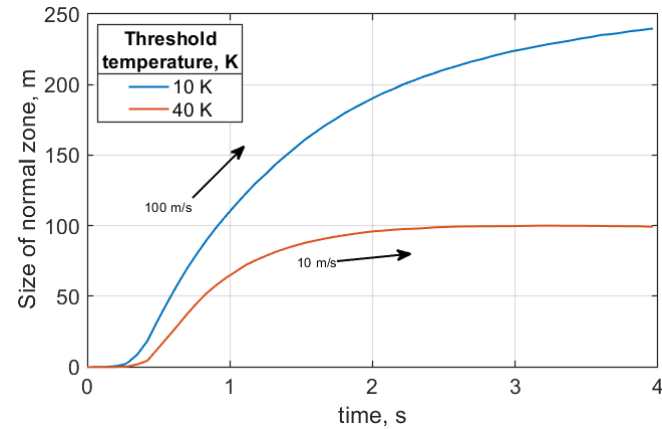
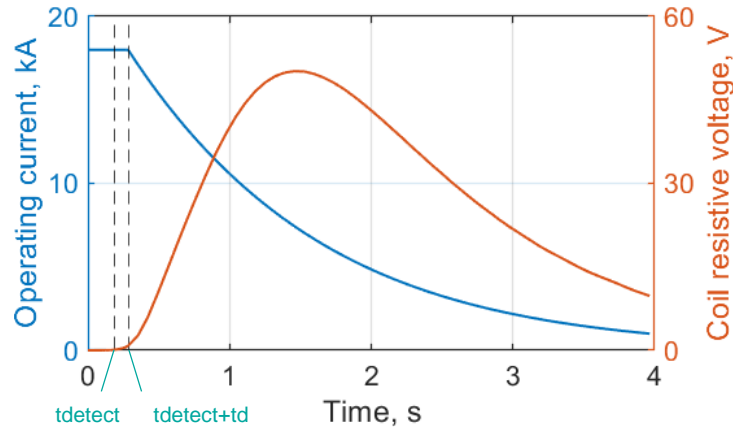
(mutual inductance used to calculate distribution of voltage to ground)

Conductor face and  
conductor side  
cooled by helium  
(through 0.2 mm G10)









- ~98% stored energy released in Rdump, ~660 kJ in the coil winding, i.e. losing ~250 liters of helium (latent heat 2.6 kJ/liter)
- Heat removal rate by helium up to ~30 kW
- NZPV strongly depends on temperature threshold, up to ~100 m/s for the 10 K front

