

# Magnet Alignment Challenges for an MBA Storage Ring\*

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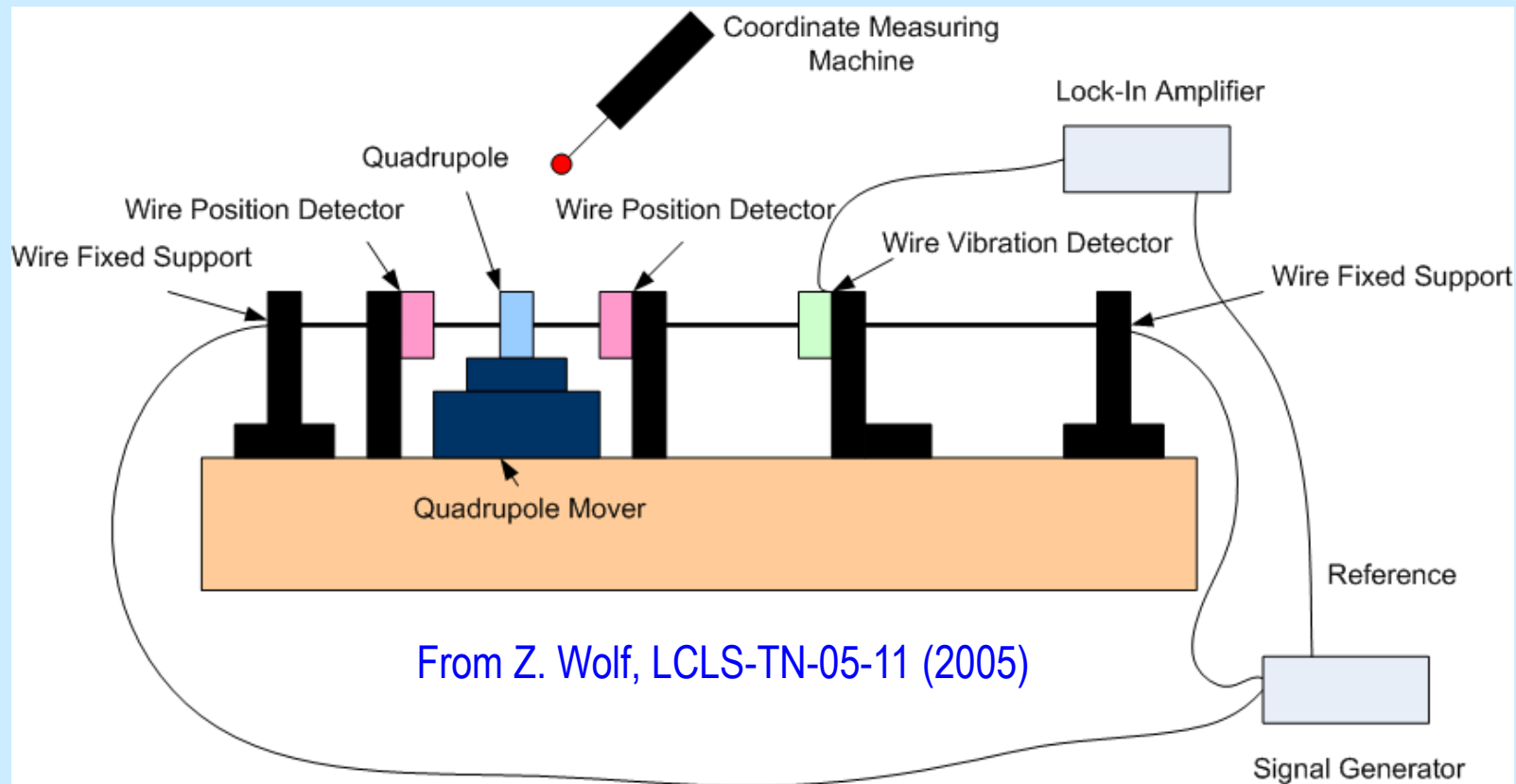
# Outline

- Definition of “alignment” in the context of this talk:
  - The process of positioning multiple ( $>2$ ) *physically disjointed* objects such that their magnetic centers lie on a desired curve.
- Alignment methods involving survey and/or mechanical precision, with or without the use of magnetic measurements:
  - Magnetic measurements to *fiducialize*, then survey to install
  - Magnetic measurements to *characterize*, then shim (?) to install
  - Alignment using manufacturing tolerances alone
- Direct alignment using magnetic measurements
- Special requirements for multi-bend acromat (MBA) storage rings.

# Fiducialization of Magnetic Axis

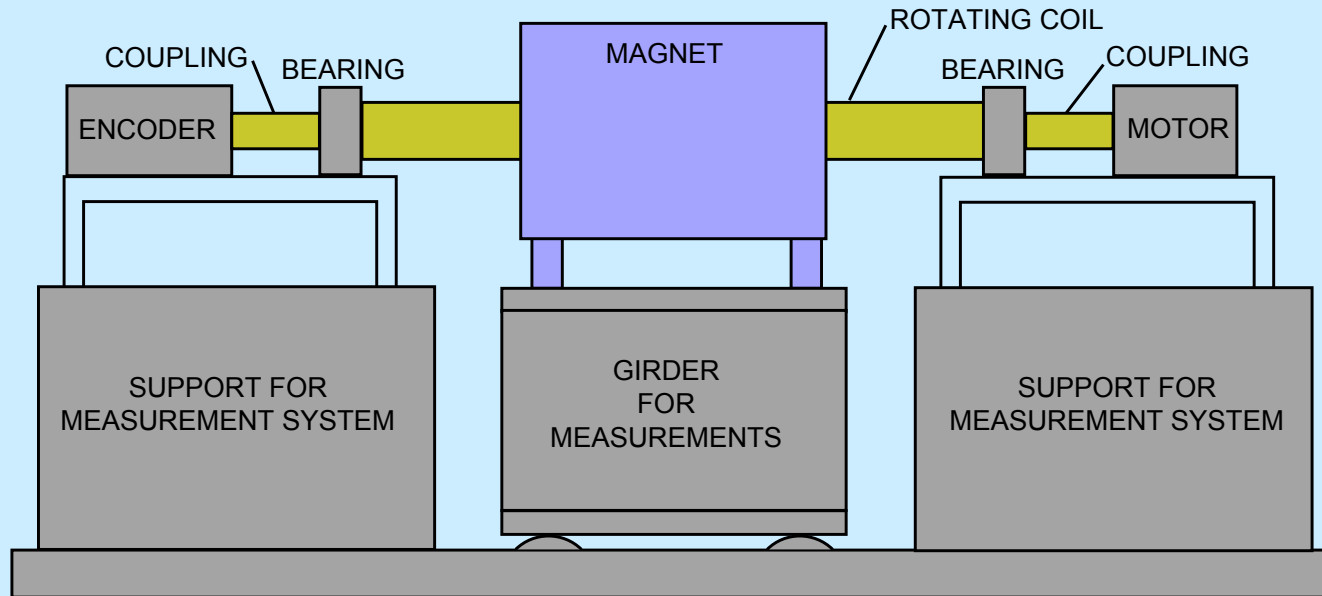
- Techniques such as rotating coils or wire based magnetic measurements (vibrating wire, stretched wire, ...) of a single magnet element can measure the magnetic axis to within  $\pm 1-5 \mu\text{m}$  *in a coordinate system tied to the measurement probe.*
- But the probe itself must be located in relation to fiducials or reference surfaces of the magnet. This is typically carried out by survey. Errors may be  $\sim 10-25 \mu\text{m}$ , or more, depending on setup.
- Final installation may incur additional errors (e.g. by survey).
- Using magnetic measurements reduces uncertainty due to possible mismatch between the mechanical and magnetic axes.
- Stack up of errors may preclude alignment  $< \pm 25-30 \mu\text{m}$ . Still, the benefit is that no precise reference surfaces are needed.

# Fiducialization: Vibrating Wire for LCLS



- Quadrupole is moved to align it with the wire (~ few microns)
- Wire is located to tooling balls on wire position detectors (~10 microns)
- Magnet fiducials are located to the wire (~15 microns)

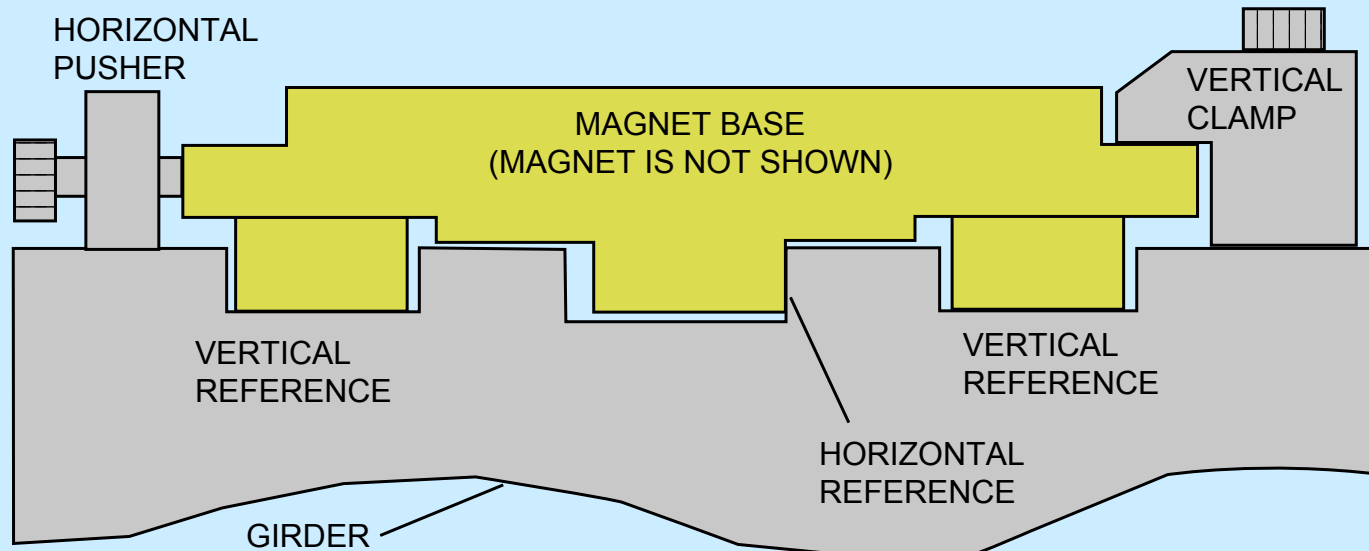
# Characterization: Rotating Coil for SLS



Based on Antokhin et al., Nucl. Instrum. Meth. A 470 (2001) 11–17.

- Rotating coil axis precisely adjusted relative to reference surfaces on the girder.
- Magnet located to the girder using reference surfaces.
- Measurements verify that the magnetic axis is within specification.
- Mean offset of all magnets  $< 5 \mu\text{m}$  horizontal,  $< 10 \mu\text{m}$  vertical, Std. dev.  $< 20 \mu\text{m}$ .
- Several magnets installed on a girder using reference surfaces.

# Alignment of SLS Multipoles on Girders



Based on Antokhin et al., Nucl. Instrum. Meth. A 470 (2001) 11–17.

- Magnet axis is verified to be within specification in relation to the reference surfaces by magnetic measurements.
- Installation of several magnets on a girder is done entirely based on reference surfaces. This allows easy alignment of several magnets.
- It is possible to use shims if the axis is found to be too far off from nominal.

# Purely Mechanical Alignment

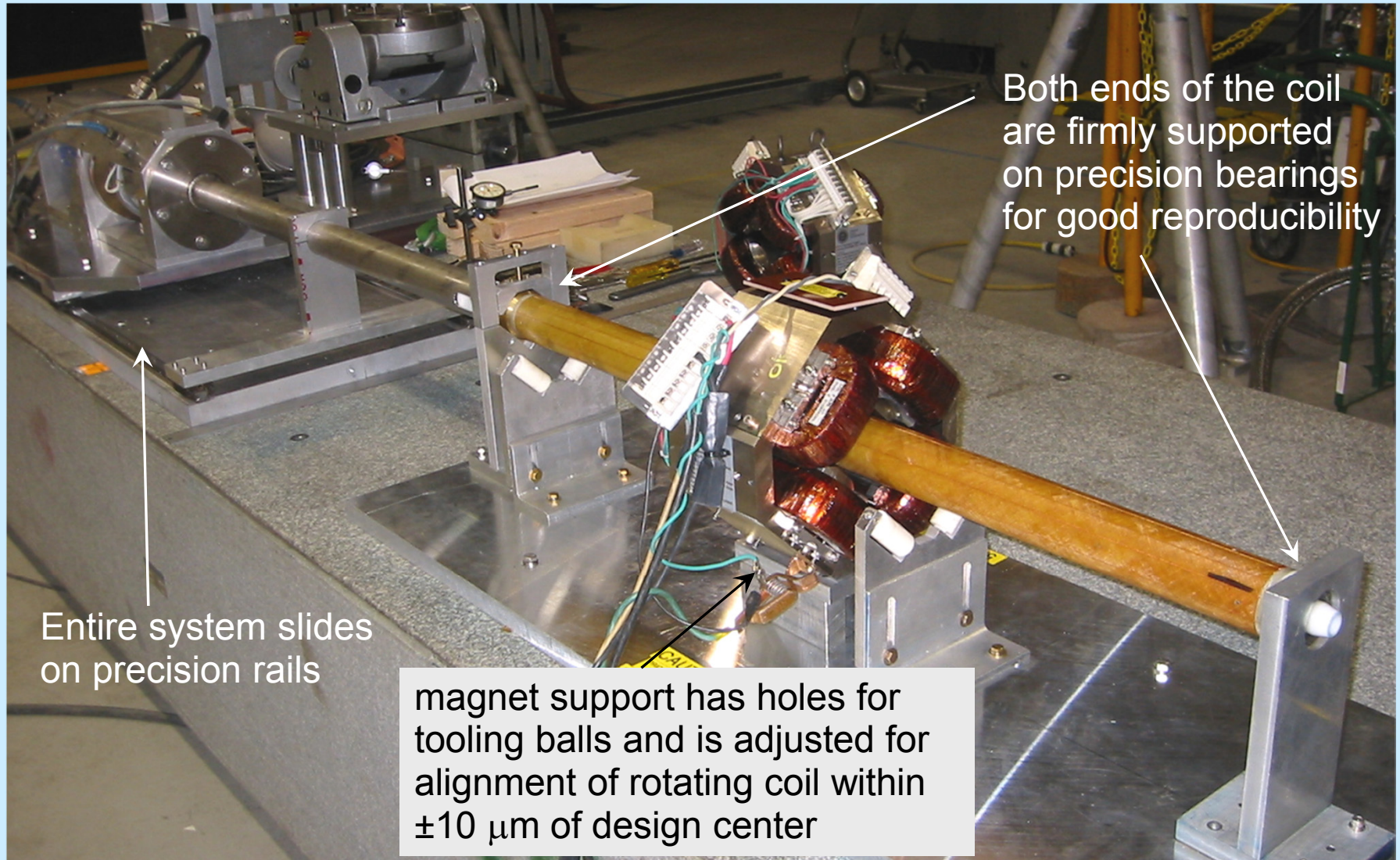
- It may be argued that in a well built magnet (good field quality), the magnetic and mechanical axes must coincide.
- It should, therefore, be possible to skip fiducialization, or a verification using magnetic measurements.
- A purely mechanical alignment does require precision machined surfaces on all magnets, as well as on long and massive support structures, similar to those used for SLS.
- Since magnets are to be machined to high precision anyway, it may not be too expensive to add precision reference surfaces.
- Surfaces with  $\sim 10 \mu\text{m}$  accuracy over long lengths, however, may add significant cost and limit the pool of possible vendors.

# Mechanical Vs. Magnetic Axes

- While the definition of magnetic axis is less ambiguous, there is no unique definition of the mechanical axis of an as-built magnet
  - Option 1: Define as a fixed offset from reference surfaces
    - Easy to use; no ambiguity; but really only pole positions matter
  - Option 2: Define somehow based on survey of individual poles
    - Tedious; complex pole profiles not very suitable to work with; subject to data analysis procedures; not too useful for aligning.
- While good agreement between mechanical and magnetic axes is reported in some cases (e.g. SLS), counter examples exist.
- It may be prudent to confirm the validity of this agreement in a specific production before deciding on a purely mechanical alignment, specially if tight alignment tolerances are needed.



# Example: Quadrupoles for BNL ERL



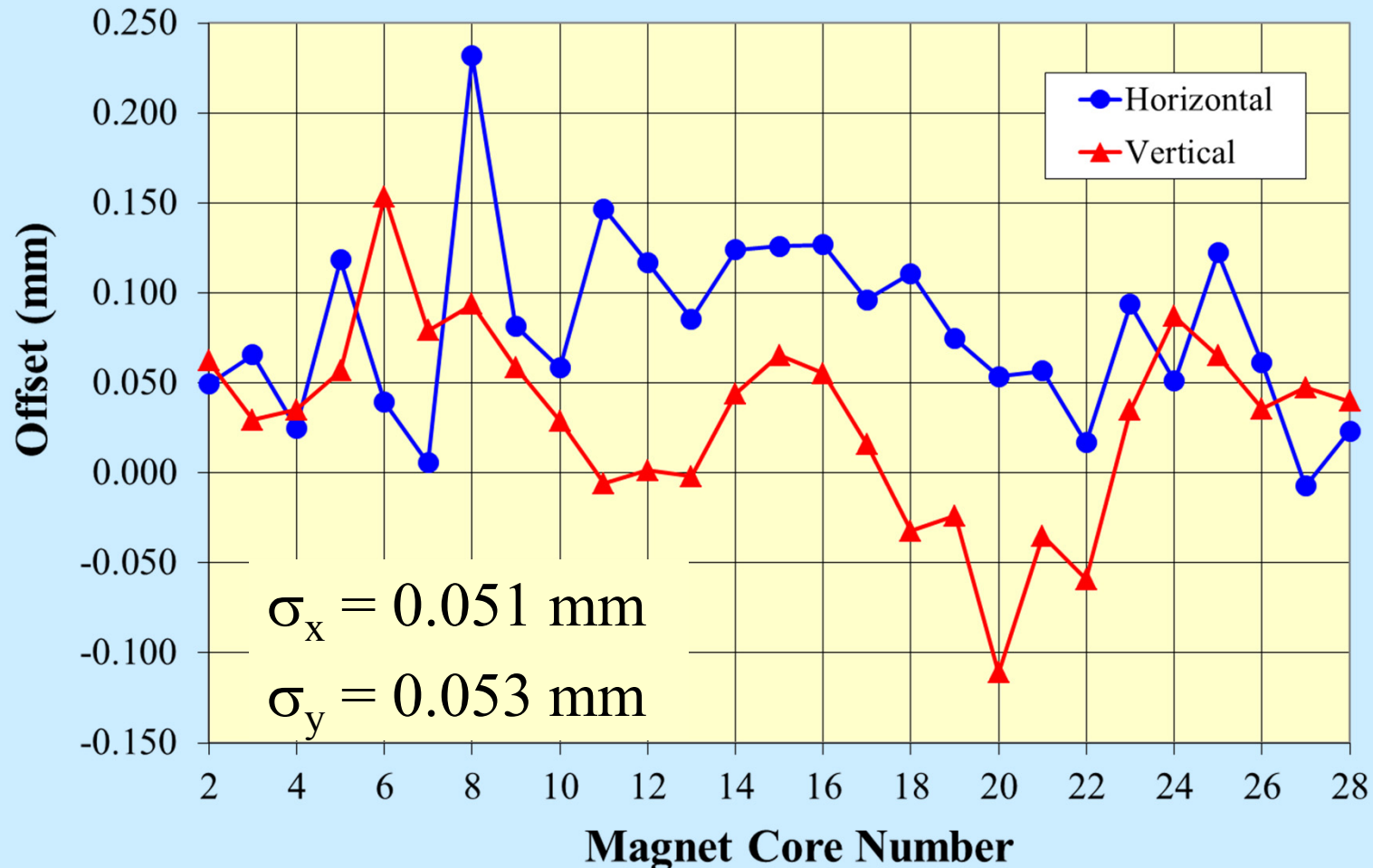
Both ends of the coil are firmly supported on precision bearings for good reproducibility

Entire system slides on precision rails

magnet support has holes for tooling balls and is adjusted for alignment of rotating coil within  $\pm 10 \mu\text{m}$  of design center

# Measured Offsets in ERL Quadrupoles

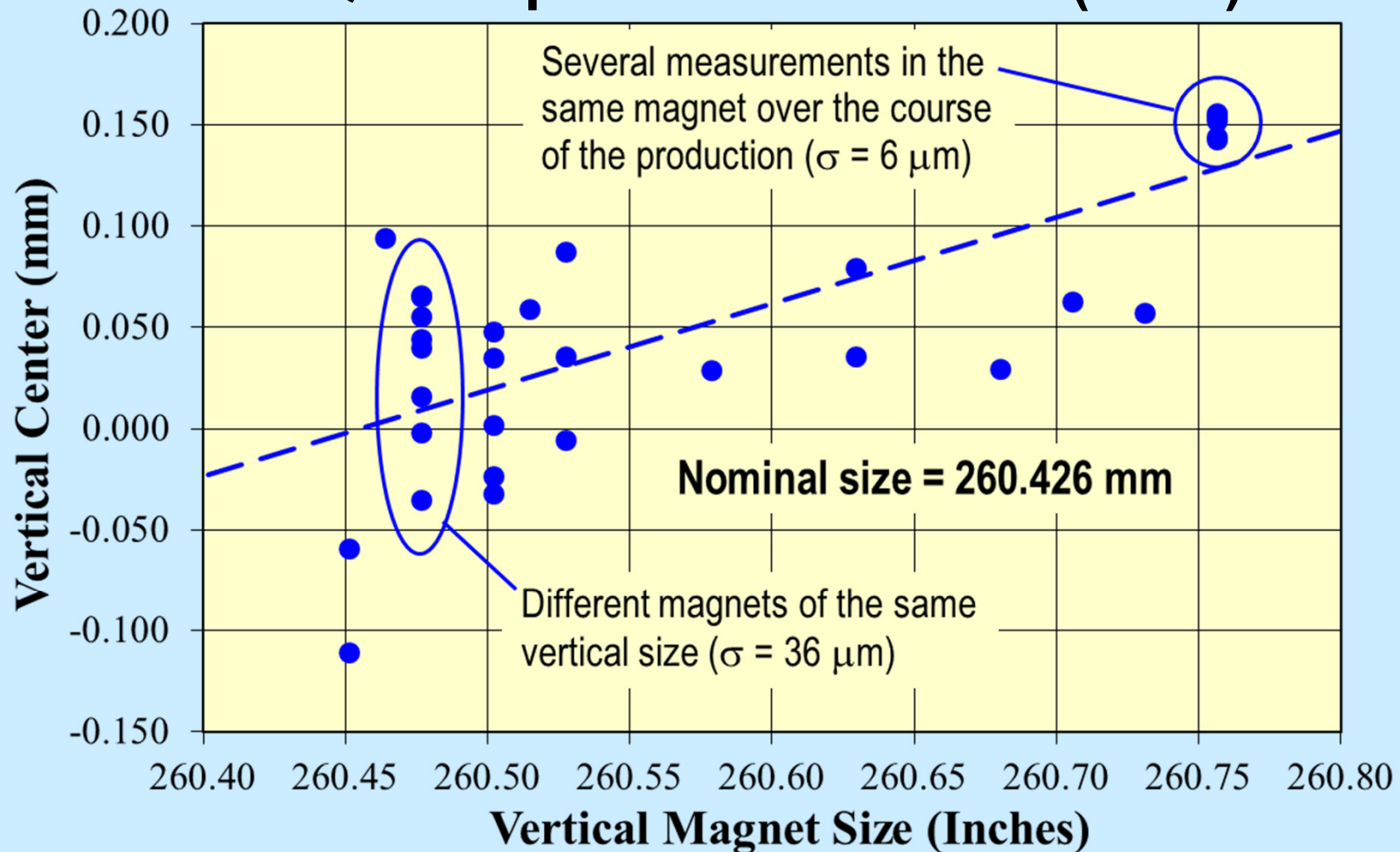
## Offsets from Reference Surfaces in ERL Quads



The vertical offset shows some correlation with magnet vertical size

# Y-Offset Vs. Magnet Vertical Size

## Quadrupoles for BNL ERL (2007)





# Summary: Mechanical/Survey based Alignment

- Alignment using survey:
  - Does not require special precision machined reference surfaces.
  - Requires the magnet fiducials to be related to the magnet center (either magnetic or mechanical).
  - Alignment at  $\sim 30 \mu\text{m}$  level of several elements on a common support spanning several meters may be possible, but not easy.
- Alignment using precision reference surfaces:
  - Aligning several elements on a common support is straightforward.
  - Requires precision machining of each magnet element as well as of long, massive support structures that should not deform easily.
  - Magnetic and mechanical axes must show good agreement.

# Direct Magnetic Alignment

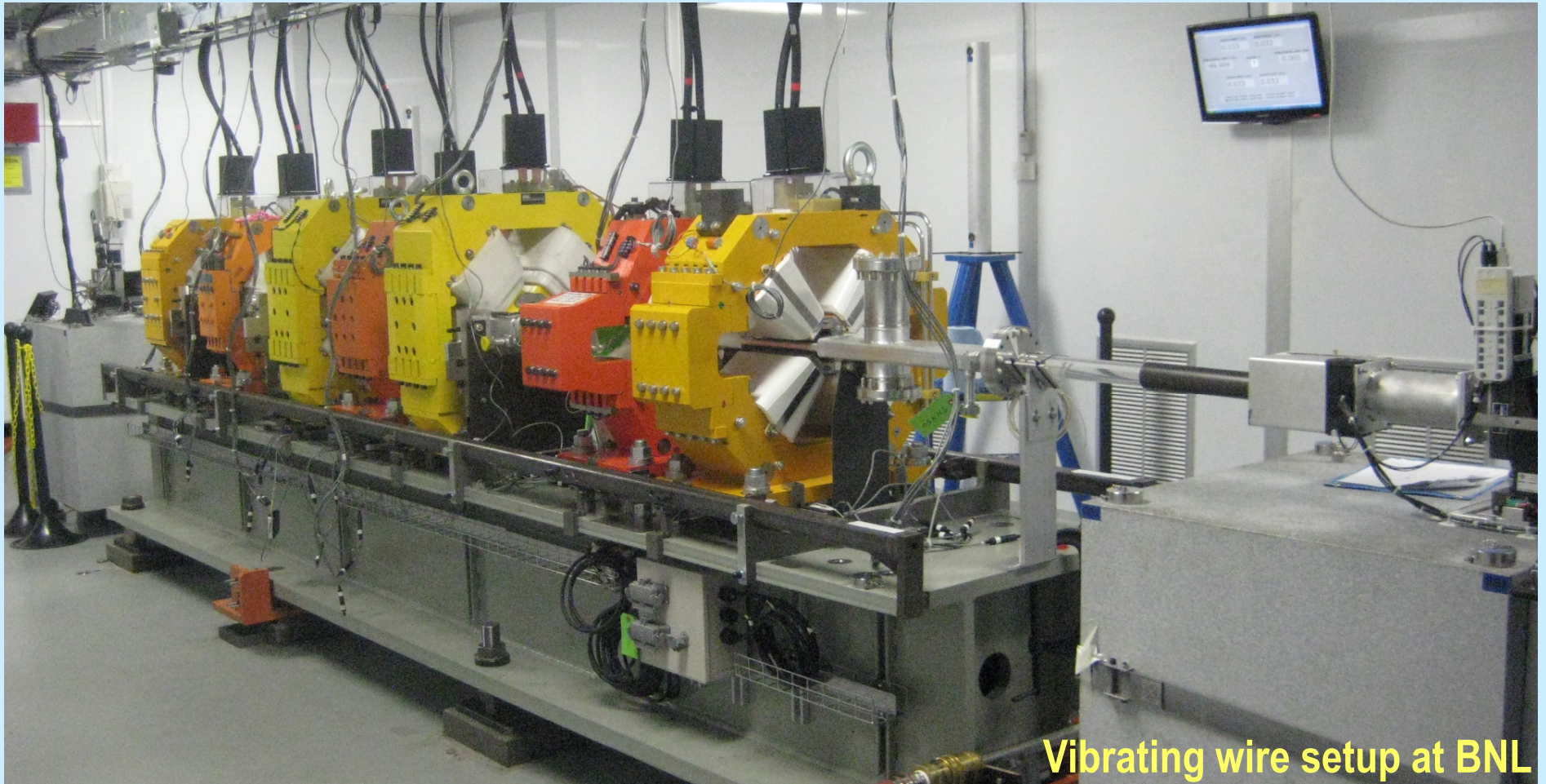
- Magnets may be aligned directly to each other using magnetic measurements. This offers some advantages:
  - No need to fiducialize magnets, no stack up of errors
  - No need for precision reference surfaces
  - Support structure requires no precision manufacturing (cheap)
  - Mechanical vs. magnetic axes is irrelevant (less R&D & monitoring)
- Requires a wire based measurement technique, and is thus most suitable for straight assemblies up to ~5 m long.
- Requires temporary fixtures to move and secure magnets.
- Most frequently voiced concern is that it is too expensive, or too time consuming (not necessarily well founded!)

# Wire Based Measurement Techniques

- Stretched Wire
  - The wire is moved across the aperture and the change in flux is measured. The axis is derived from a set of measurements with different wire motion paths. (Accuracy  $\sim 2\text{-}5\ \mu\text{m}$ ; time  $\sim \frac{1}{2}$  hr)
- Vibrating wire
  - An AC current of a frequency matching a resonant mode of the wire is passed through the wire. This causes the wire to vibrate with an amplitude proportional to the field strength.
  - Vibration amplitudes are analyzed as a function of wire position to derive the magnetic axis. (Accuracy  $\sim 2\text{-}5\ \mu\text{m}$ ; time  $\sim \frac{1}{2}$  to  $\frac{3}{4}$  hr)
- Rotating wire (not yet well established, but promising)
  - A single wire is used as a rotating coil. (Accuracy ?; time  $\sim \frac{1}{4}$  hr)



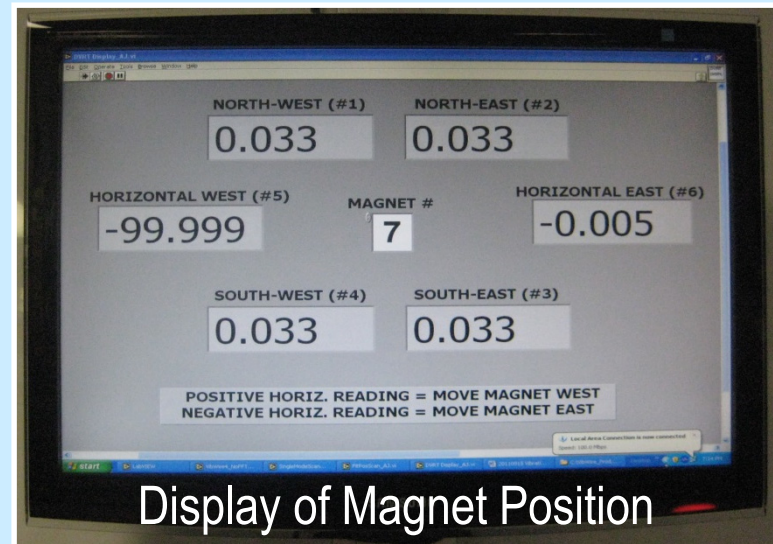
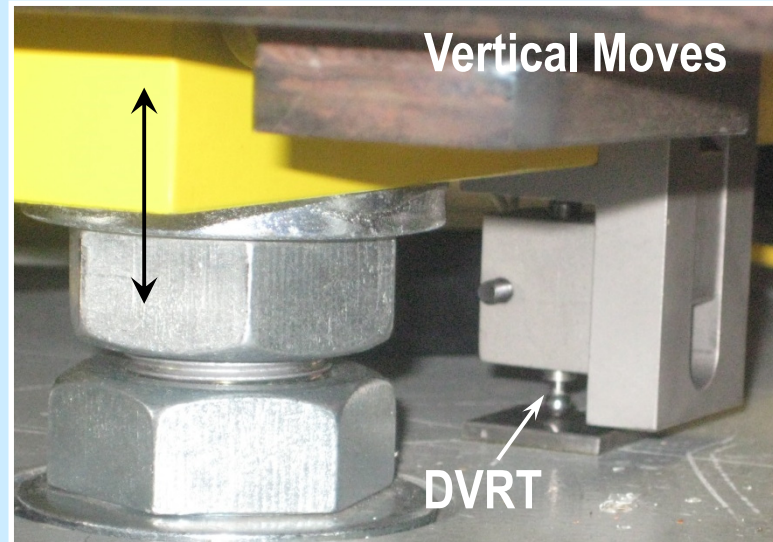
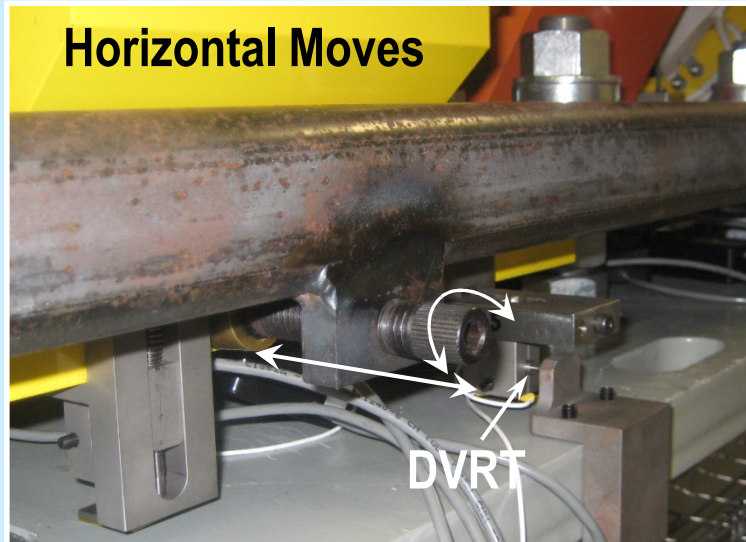
# A NSLS-II Girder Undergoing Alignment



Vibrating wire setup at BNL



# Adjusting Magnet Position





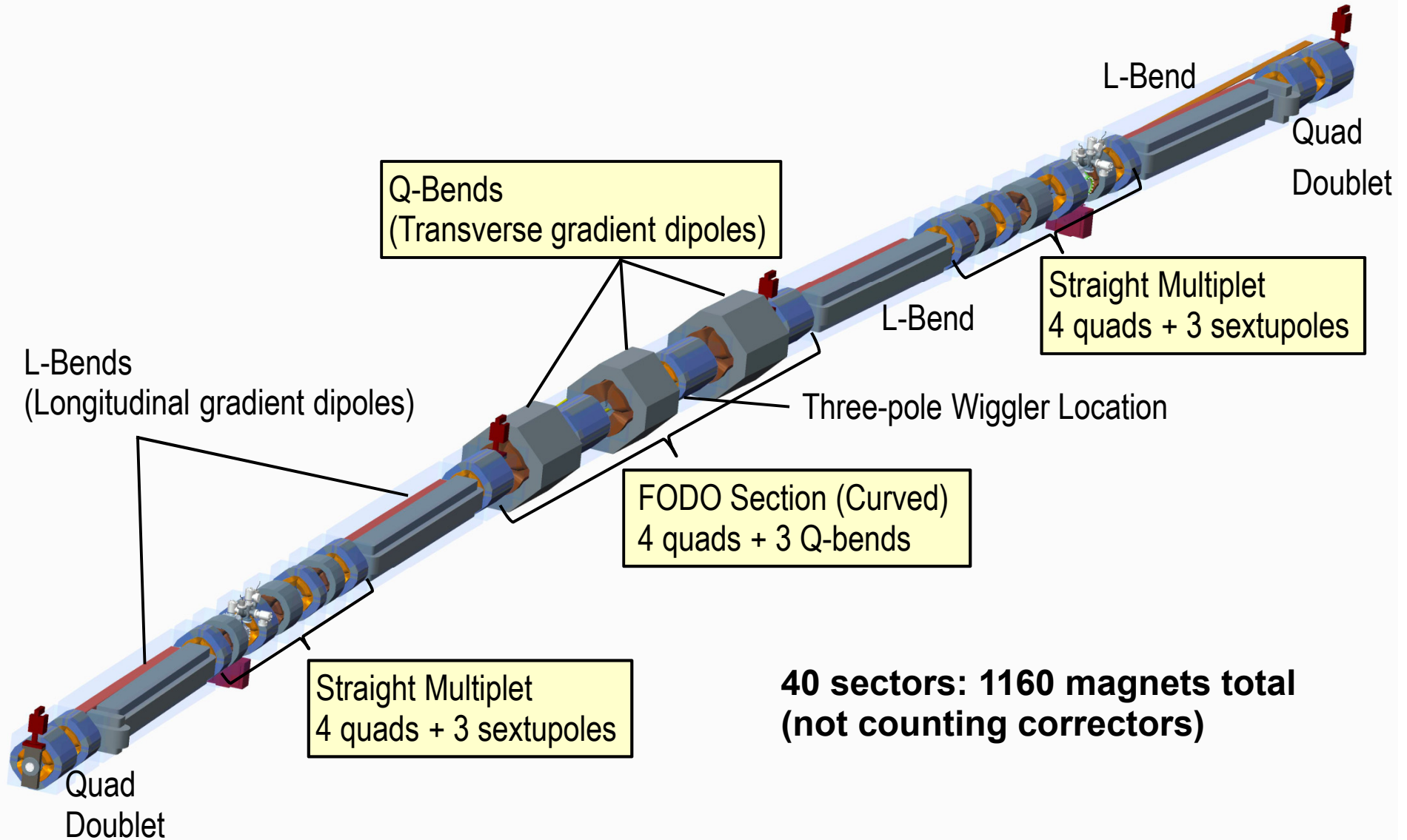
# Summary of Magnetic Alignment

- Magnetic alignment provides the best assurance that magnets are aligned to the required tolerance, or better.
- Direct alignment using a wire based technique saves the effort to fiducialize individual magnets, or the cost of precision reference surfaces. It also avoids error stack up.
- But there are a few drawbacks:
  - Measurements can be time consuming (can be reduced significantly by developing techniques such as a rotating wire).
  - Moving magnets precisely and securing them to the girder requires small moves, and could be time consuming for large moves.
  - Girder must be very rigid, or the profile must be reproduced.
  - Readily applicable to straight assemblies only.

# Multi-bend Acromat Storage Rings

- Multi-bend acromat (MBA) designs for the low emittance rings contain several bending elements per cell, and a large number of magnets packed closer together.
- One obvious challenge is that there are many magnet elements to align, and any technique used must be cost effective.
- The presence of many bending elements may mean that not all magnets within a “logical group” are arranged in a straight line.
- The MBA designs also feature combined function magnets where both the field and the field gradient are very high. These magnets pose a unique alignment challenge, not encountered in the traditional Double Bend Achromats (DBA).

# Example: APS Upgrade Sector Layout



# Straight Sections in MBA Lattice

- If only multipoles are to be aligned on a straight line, these assemblies are similar to existing machines and any of the alignment techniques described earlier may be used.
- The choice of which method to use depends on several factors:
  - Prior experience and resources available for magnetic alignment.
  - Level of agreement between mechanical and magnetic axes.
  - Availability and cost of high precision ( $\sim 10 \mu\text{m}$ ) machining.
- Perhaps a good compromise could be (?):
  - Align based on precision reference surfaces, but verify magnetically (also gives “assembly axis”); shim only larger than acceptable offsets ( $> 30 \mu\text{m}$ , say; hopefully in rare cases).

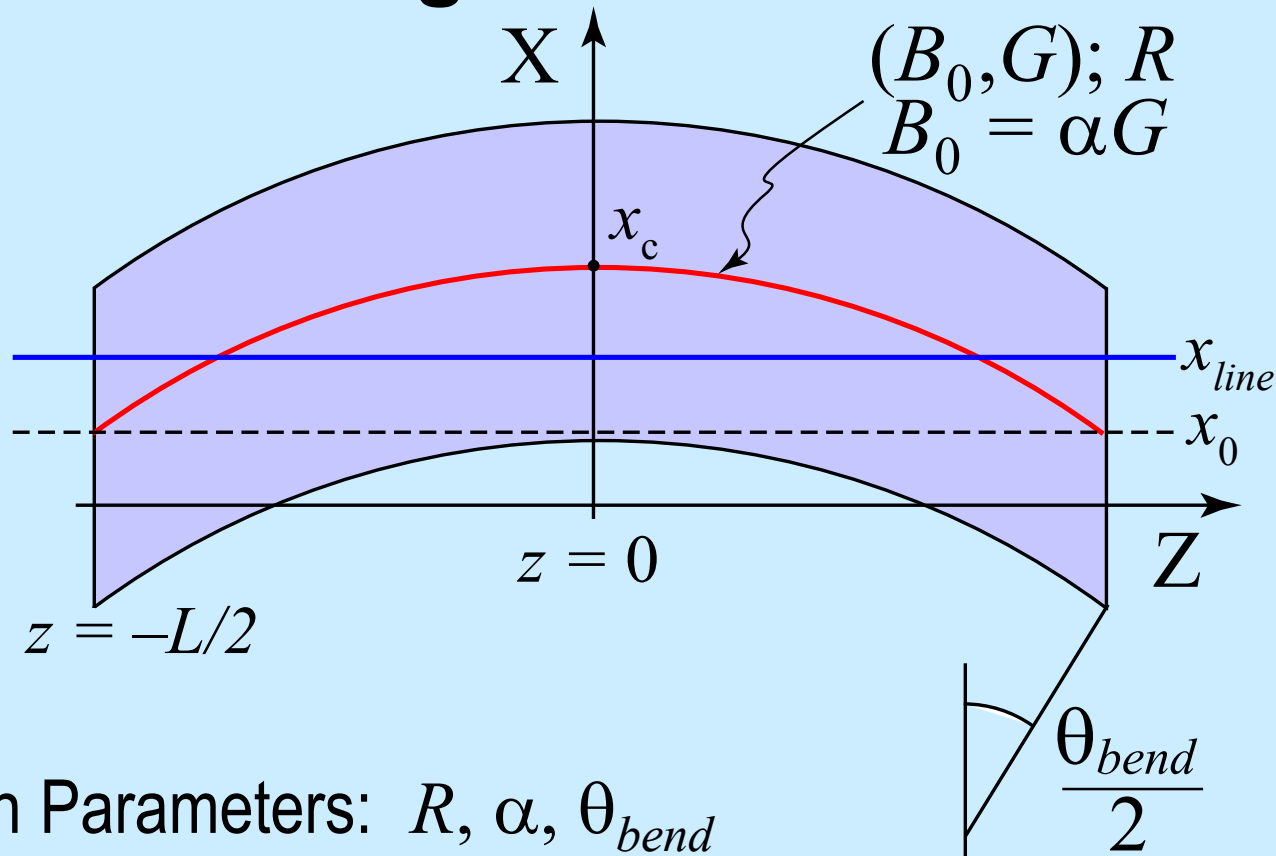
# Curved Sections in MBA Lattice

- Several bending and focusing elements are closely interleaved in some sections, e.g., the central FODO section for the APS upgrade. The bending elements may have strong gradients too.
- An assembly of reasonable length may consist of at least one bending element.
- The alignment of the bending element may also be critical due to strong transverse gradients:
  - Example (APS-U): 100  $\mu\text{m}$  misalignment  $\sim$  0.8% bending error
- There is no well established technique to find the axis of a curved magnet at the level of precision needed ( $\sim$ 10-15  $\mu\text{m}$ ).
- R&D is needed to develop procedures for curved magnets.

# Options for Curved Sections

- Standard technique applicable to measurement of curved sections is to use a Hall probe system with precision stages.
- Hall probe element can be located in the stage coordinate system using a magnetic pin, for example. But this involves accurate knowledge (survey) of the pin location.
- The magnet can be mapped using Hall probe, and the axis derived, provided there is easy access for the Hall probe holder.
  - Easier to do with an open side design (e.g. ESRF design)
  - Achievable accuracy may not be sufficient; also time consuming.
- Another option is to measure along straight lines using a wire, and apply appropriate offset (to be developed, ESRF inspired).

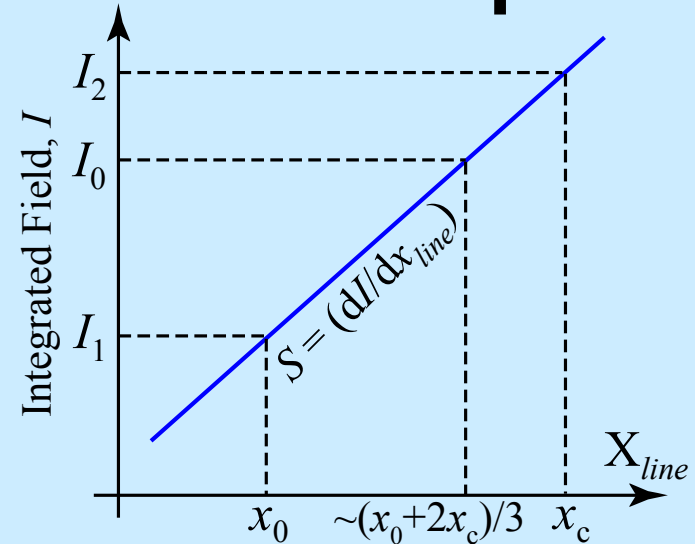
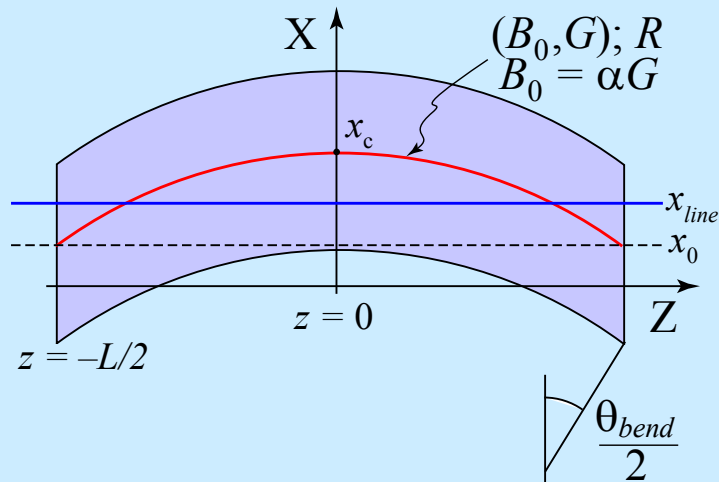
# Straight Line Integration in Gradient Dipoles



- Known Parameters:  $R, \alpha, \theta_{bend}$
- Integration path assumed parallel to tangent at  $x_c$  (General case is to be investigated)
- Goal is to locate the point  $x_c$  for a given magnet setting.



# Straight Line Integration in Gradient Dipoles



$$I(x_{line}) = \int_{-\infty}^{\infty} B_y(x_{line}, z) \cdot dz$$

$$I = S \left[ x_{line} - x_0 + \alpha + R \left\{ \cos\left(\frac{\theta_{bend}}{2}\right) - \frac{\theta_{bend} + \sin \theta_{bend}}{4 \sin(\theta_{bend}/2)} \right\} \right]$$

$$I_1 = S \left[ \alpha + R \left\{ \cos\left(\frac{\theta_{bend}}{2}\right) - \frac{\theta_{bend} + \sin \theta_{bend}}{4 \sin(\theta_{bend}/2)} \right\} \right] \approx S \left[ \alpha - \frac{R\theta_{bend}^2}{12} \right]$$

$$I_2 = S \left[ \alpha + R \left\{ 1 - \frac{\theta_{bend} + \sin \theta_{bend}}{4 \sin(\theta_{bend}/2)} \right\} \right] \approx S \left[ \alpha + \frac{R\theta_{bend}^2}{24} \right]$$

Integral along curved trajectory:

$$I_0 = S \frac{\alpha \theta_{bend}}{2 \sin(\theta_{bend}/2)} \\ \approx (S\alpha) \left[ 1 + \frac{\theta_{bend}^2}{24} \right]$$



# Fiducializing Curved Gradient Dipoles

- Install magnet on a wire based measurement bench such that the wire is parallel to the tangent to the nominal trajectory at the axial midpoint of the magnet.
  - Based on mechanical measurements or reference surfaces
- Measure integrated field (e.g. using rotating wire) as a function of transverse position. The slope of a straight line fit gives roughly the integrated gradient (may correct for finite bending).
- Compute the integrated field expected when the wire is tangent to the nominal trajectory, and interpolate the tangent point ( $x_c$ ).
- Use this information to install the magnet by survey, or to align to adjacent multipoles using the same wire setup.

# Summary

- Alignment methods used in the past range from purely mechanical to purely magnetic alignment.
- Mechanical alignment offers ease of installation, but requires precision machined surfaces on all magnets, as well as on long support structures. Magnetic alignment is not guaranteed.
- Direct magnetic alignment offers the best assurance of good alignment without requiring precision machined surfaces.
- Multi-bend achromats contain many more magnets. Method used should be the fastest, while ensuring alignment tolerance is met.
- Curved gradient dipoles pose the maximum alignment challenge, requiring new alignment procedures to be developed.