

Multiscale modelling of cracking in CeO_2 and UO_2 pellets

Janne Heikinheimo, Tom Andersson, Anssi
Laukkanen, Wade Karlsen, and Jason L.
Schulthess
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Outline

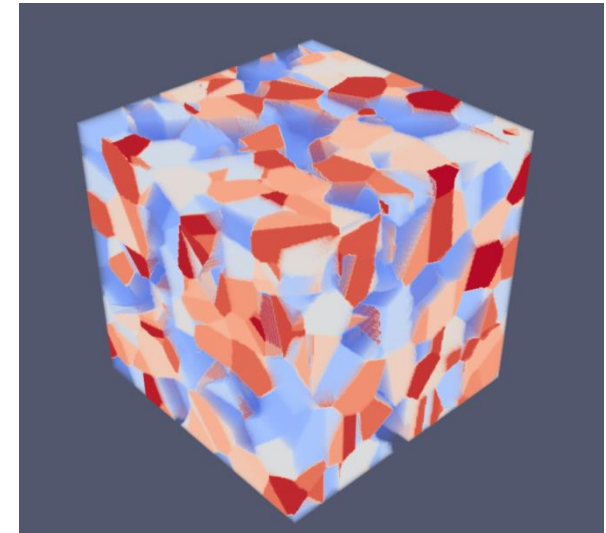
- Motivation for fuel cracking multiscale modelling
- What is properTune?
- Crystal plasticity modelling
- Case example with modelling: Martensite steel cracking
- Model development for UO_2 and CeO_2 cracking
- Experimental comparison
- Future plans

Motivation for fuel cracking multiscale modelling

- Nuclear fuel complex thermomechanical processes are not yet understood well enough
- The more physics based modelling requires multiple length and time scales to cover e.g. fuel heterogeneous development
- Fuel deformation phenomena (including cracking) affects significantly fuel performance and safety features
 - Recently understanding of microcracking has been named as an important future need in explaining fission gas burst release (Tonks et al., 2018)

What is properTune?

- Collection of tools used in solving thermomechanical properties of different materials
- Applies the MOOSE framework
- Covers length and time scales from MD to component scale
- Applied so far successfully in steel cracking modelling under stress: ductile to brittle transition (DBT)
- Development for ceramic cracking modelling ongoing

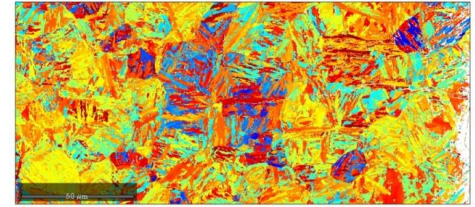


Lindroos, M., et al. *Comput. Mater. Sci.* 170, 109185, 2019

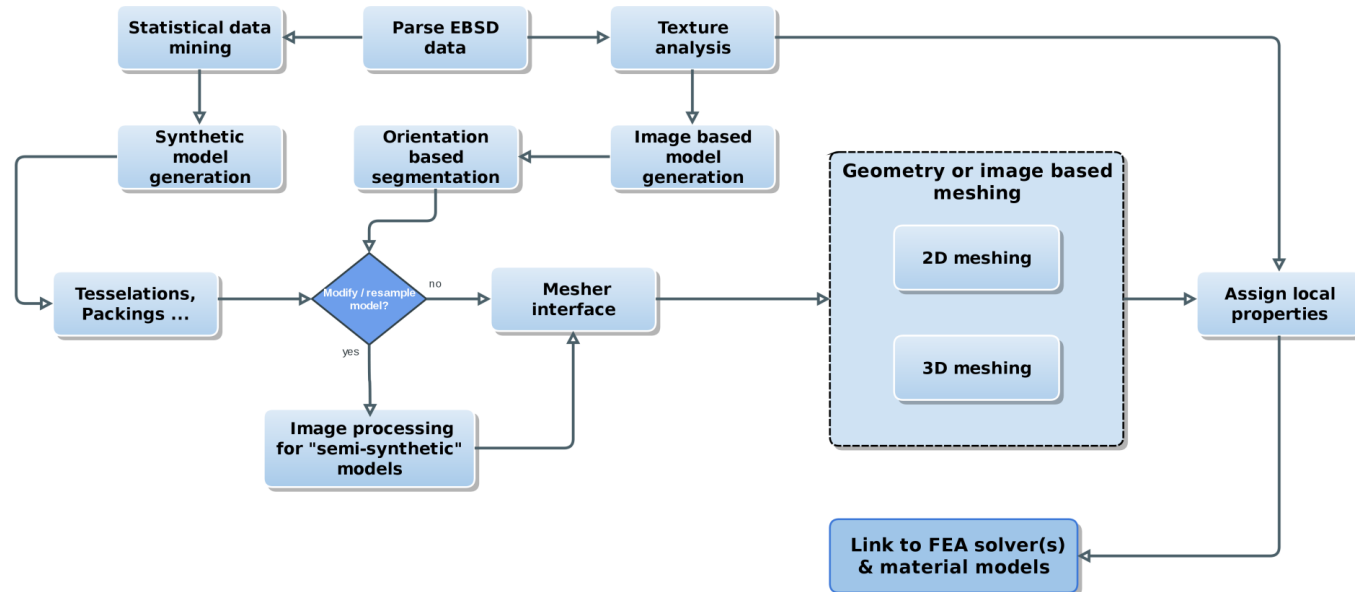
Crystal plasticity modelling

1) Preferably SEM EBSD characterization as input. Information about the grain morphology and possible texture is needed

2) 3D microstructural model geometry from a stack of 2D EBSD images as input (utilizing FIB for serial sectioning) if available.

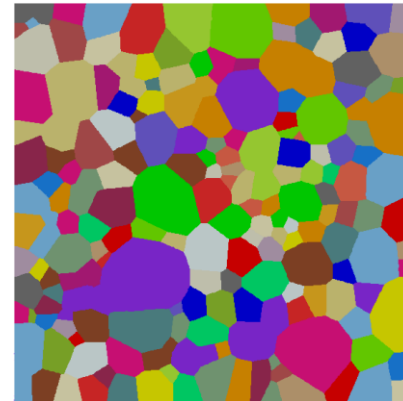
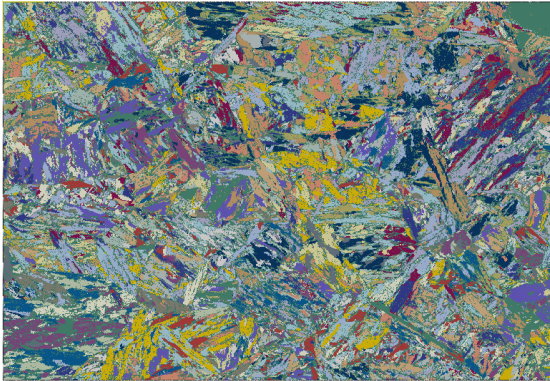


- Finite element type approach
- Thermomechanical properties depend on the crystal orientation



Electron backscatter diffraction (EBSD) based mesh model

- EBSD inverse pole figure (IPF) map
- Realistic microstructure
- Synthetic models



Crystal plasticity model with "cleavage damage"

$$\dot{\gamma}^s = \dot{\nu} \text{sign}(\tau^s) = \left\langle \frac{|\tau^s - x^s| - r^s - \tau_0}{K} \right\rangle^n \text{sign}(\tau^s - x^s)$$

Phenomenological slip rate formulation

$$x^s = c\alpha_s ; \dot{\alpha}_s = (\text{sign}(\tau^s - x^s) - d\alpha^s)\dot{\nu}^s$$

Kinematic hardening parameter

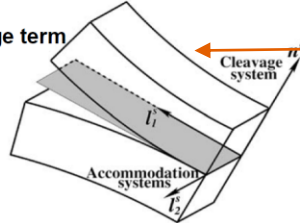


$$r^s = Q \sum_r H_{rs} \{1 - \exp(-b\dot{\nu}^r)\} + H\beta^2 \dot{\nu}^s + H\beta d$$

Isotropic hardening and softening arising from the contribution of damage

Beta is coupling factor

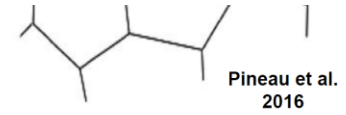
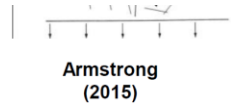
Plasticity term



$$\dot{\epsilon}^{in} = \dot{\epsilon}^p + \dot{\epsilon}^d$$

$$\dot{\epsilon}^d = \sum_{s=1}^{N_{damage}} \dot{\delta}_c^s n_d^s \otimes n_d^s + \dot{\delta}_1^s n_d^s \otimes l_{d1}^s + \dot{\delta}_2^s n_d^s \otimes l_{d2}^s$$

Crack growth



where $\dot{\delta}_c^s, \dot{\delta}_1^s, \dot{\delta}_2^s$ are the strain rates for mode I, mode II, and mode III crack growth, respectively.

$$\tau_{dc} = n_d^s \cdot M \cdot n_d^s$$

Background in Aslan(2011) and Sabnis(2016) for FCC and soft BCC materials

$$\dot{\delta}_c^s = \left\langle \frac{\tau_{dc} - Y_c^s}{K_d} \right\rangle^{n_d} \text{sign}(\tau_{dc})$$

while the mode II and mode III shearing is computed similarly.

$$\tau_{di} = n_d^s \cdot M \cdot l_{di}^s$$

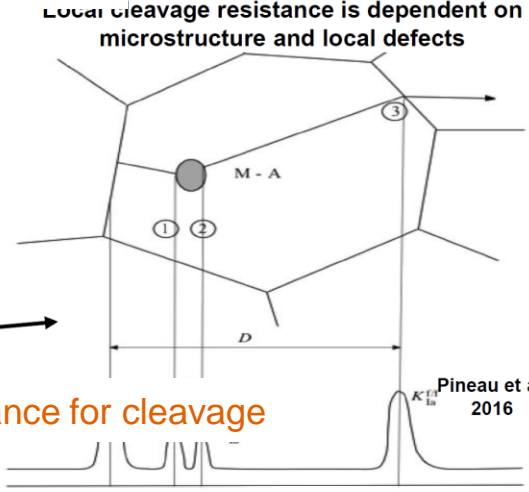
Cleavage systems in BCC operate on [100] planes

$$\dot{\delta}_i^s = \left\langle \frac{\tau_{di} - Y_i^s}{K_d} \right\rangle^{n_d} \text{sign}(\tau_{di}), \text{ with } (i = 1, 2)$$



Damage variable (d) is strain based instead of scalar [0,1]
Therefore, crack opening strain is tracked and it can go back to zero (crack is closed)

Resistance for cleavage



Pineau et al. 2016

Damage model parameters

■ Plasticity

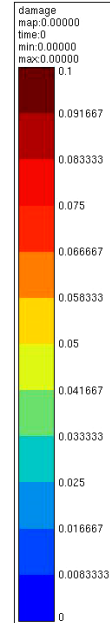
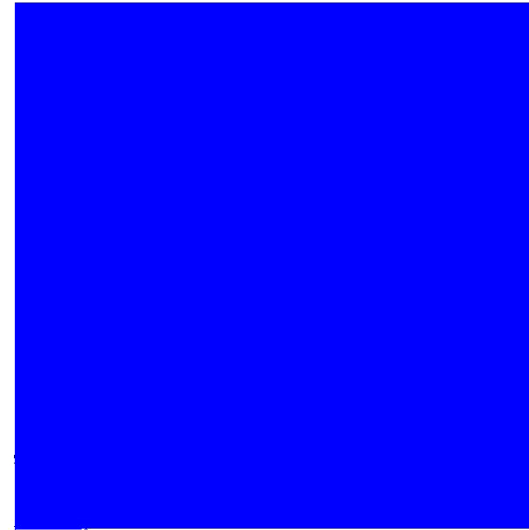
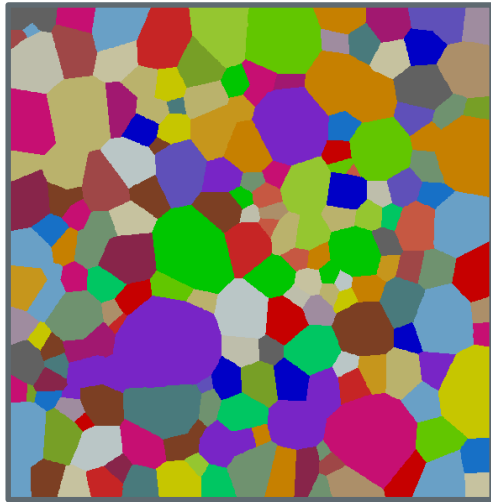
- Initial critical resolved shear stress, τ_0 (slip families 110, 112)
- Hardening coefficient, Q
- Interaction matrix (slip-slip), H_1-H_8
- Strain rate parameters, K, n
- Kinematic hardening parameters, C, D

■ Damage

- Softening parameters, H_i (for each damage mode)
- Plasticity-damage coupling parameter, β
- Cleavage opening threshold, τ_{cl}
- Cleavage shear mode II threshold, τ_{sl}
- Cleavage shear mode III threshold, τ_{sh}
- Viscous parameters (growth rate)
- Limiting compression strength, α
- Hardening limit (damaged zones)

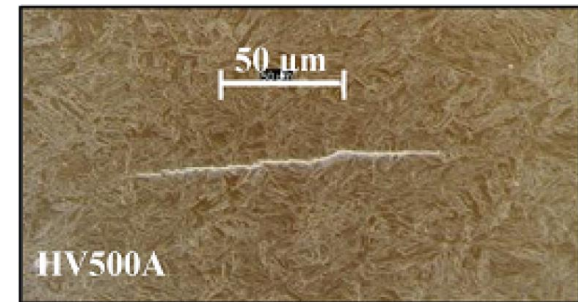
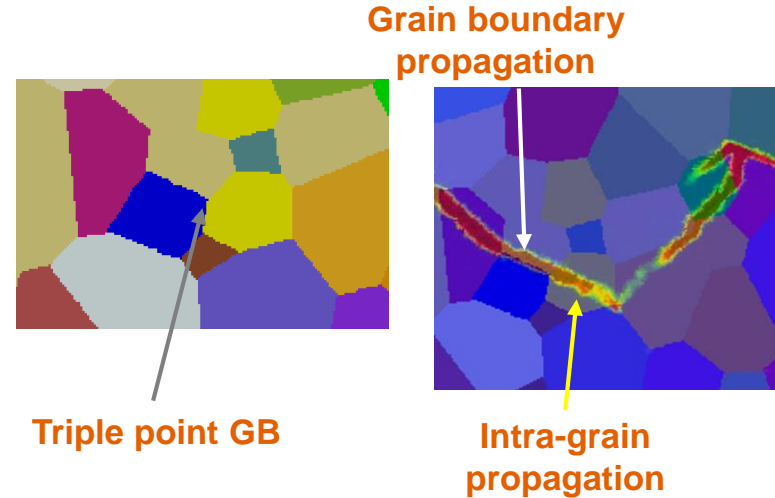
Case example with modelling: Martensite steel cracking

- Tensile test
- Damage evolution



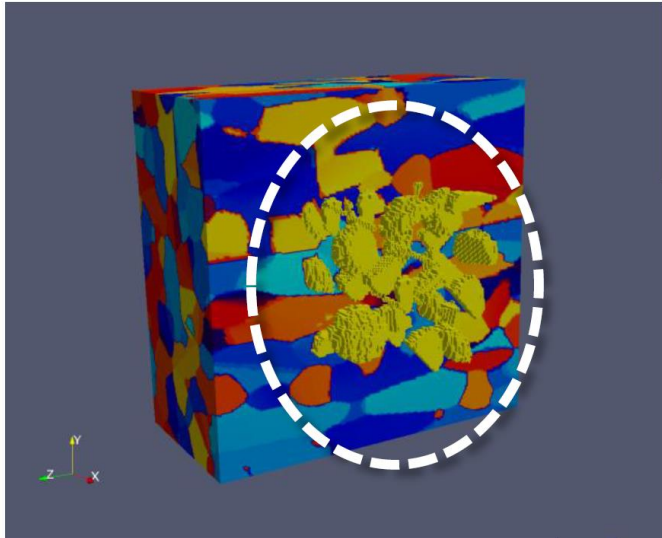
Case example with modelling: Martensite steel cracking

- Damage initiates near grain boundaries, usually at triple points
- Damage propagates intra grain and inter grain, e.g., at grain boundaries and within grains
- Shear localization affects damage path

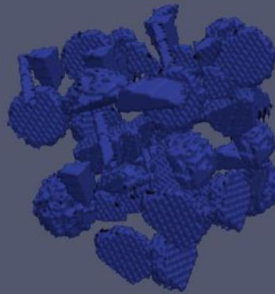


Model development for UO_2 and CeO_2 cracking

- Inclusions: gas bubbles at grain boundaries, porous phases
- Crystal plasticity: Discontinuities can be taken into account as geometrical objects with different or absent material properties or as field variable in FE analysis.
- Coupled phase field modelling: size evolution of porous phases



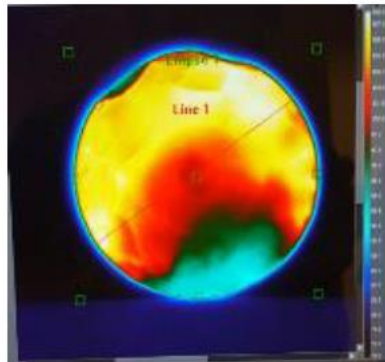
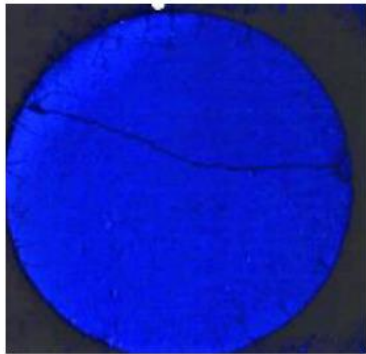
Inclusion cluster in an anisotropic oriented microstructure



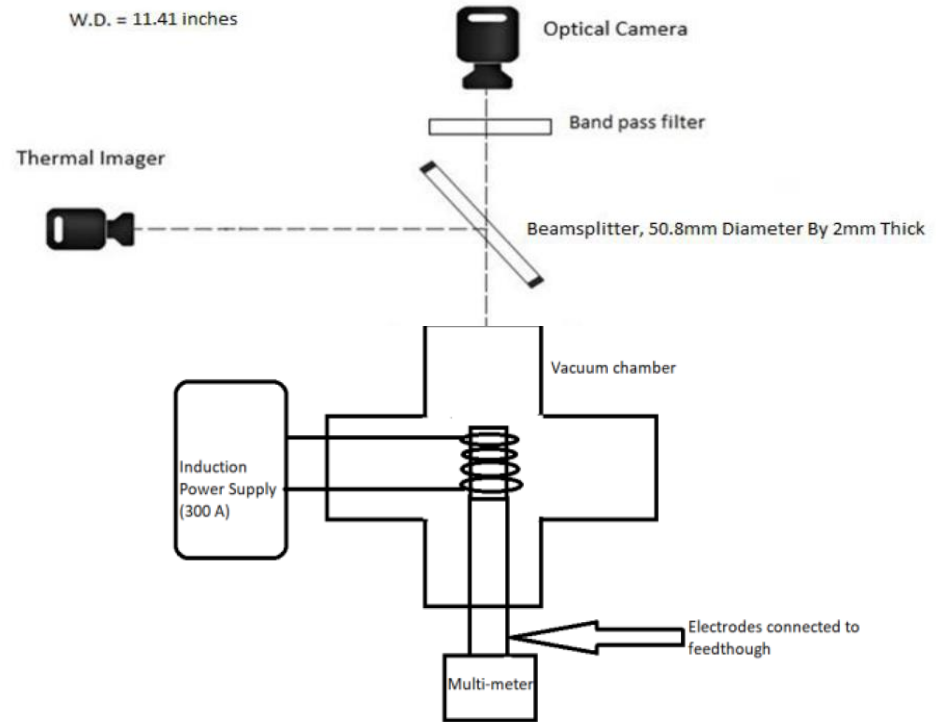
Closer view of cluster inclusion phase

Experimental comparison

- Induction heating applying Ar as cooling gas
- Simultaneous optical and infrared imaging
- Different temperatures and temperature gradients



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Future plans

- CeO₂ and UO₂ EBSD imaging and crystal model construction
- Test crystal plasticity modelling to reference fuel materials
- Add porosity and/or fission gas bubbles to the grain boundaries and apply phase field modelling together with the crystal plasticity approach
- Comparison of the obtained results to similar modelling at INL preferably with the MARMOT/BISON codes
- Comparison of the results with the upcoming experiments at INL

Thank you!



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the obvious

Janne Heikinheimo
Janne.heikinheimo@vtt.fi
+358 40 152 0296

@VTTFinland

www.vtt.fi