

Design, construction, commissioning, and early operation of the third-generation n_TOF neutron spallation target at CERN

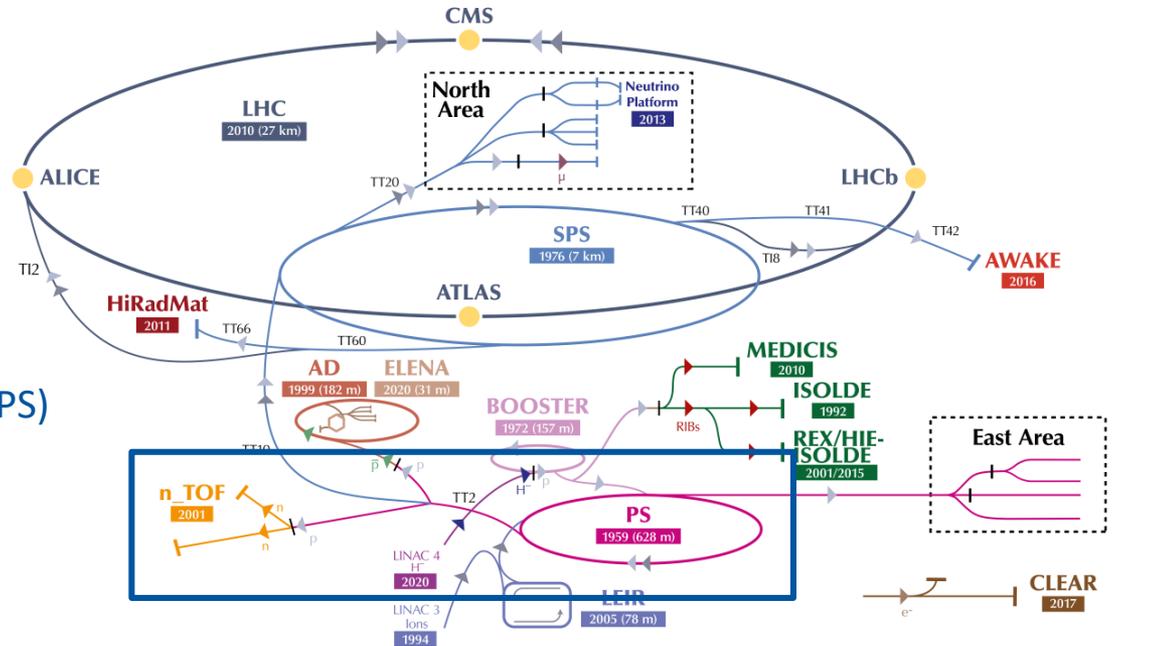
R. Esposito and M. Calviani

CERN – European Laboratory for Particle Physics

for the n_TOF third-generation spallation target project team

The n_TOF facility at CERN

The CERN accelerator complex
Complexe des accélérateurs du CERN



The Proton Synchrotron (PS) can send to n_TOF:

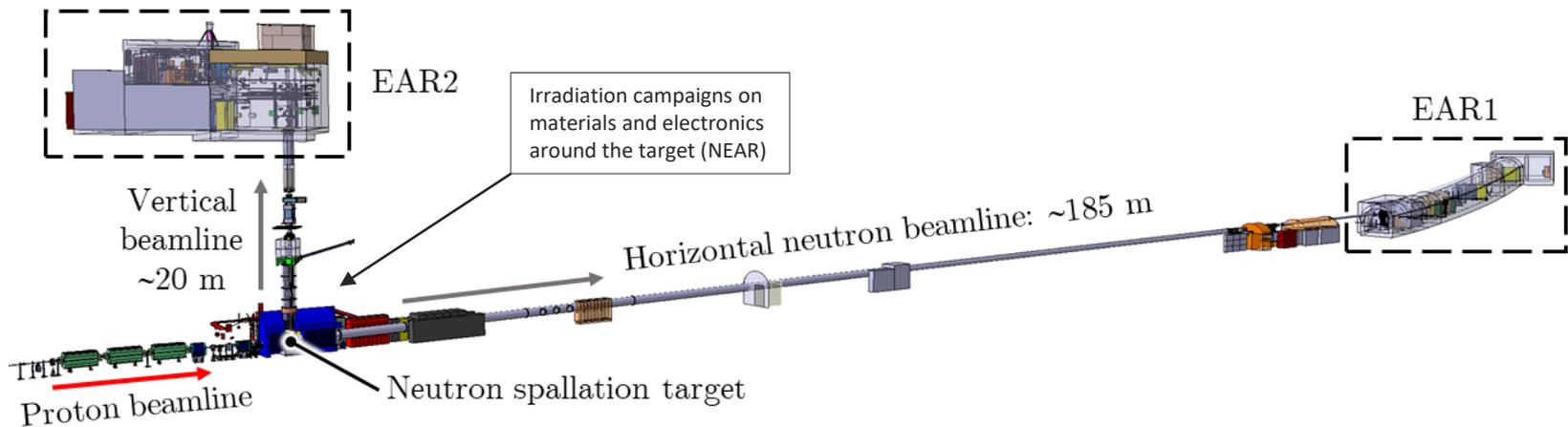
- 1 pulse every 1.2 s
- 20 GeV/c
- 8.5×10^{12} p⁺/pulse

▶ H⁻ (hydrogen anions) ▶ p (protons) ▶ ions ▶ RIBs (Radioactive Ion Beams) ▶ n (neutrons) ▶ \bar{p} (antiprotons) ▶ e⁻ (electrons) ▶ μ (muons)

LHC - Large Hadron Collider // SPS - Super Proton Synchrotron // PS - Proton Synchrotron // AD - Antiproton Decelerator // CLEAR - CERN Linear Electron Accelerator for Research // AWAKE - Advanced WAKEfield Experiment // ISOLDE - Isotope Separator OnLine // REX/HIE-ISOLDE - Radioactive Experiment/High Intensity and Energy ISOLDE // MEDICIS // LEIR - Low Energy Ion Ring // LINAC - LINear ACcelerator // n_TOF - Neutrons Time Of Flight // HiRadMat - High-Radiation to Materials // Neutrino Platform

The n_TOF facility at CERN

n_TOF: neutron Time Of Flight



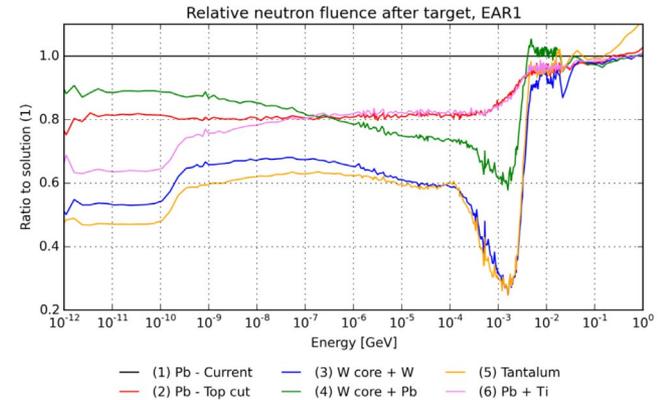
- High instantaneous neutron fluence (10^8 n/cm² in a single pulse)
- Wide energy spectrum (sub-thermal to 1 GeV)
- High energy resolution ($\Delta E/E = 10^{-4}$)

Ideal for high signal-to-background ratio neutron cross-section measurements on radioactive isotopes available only in small amounts

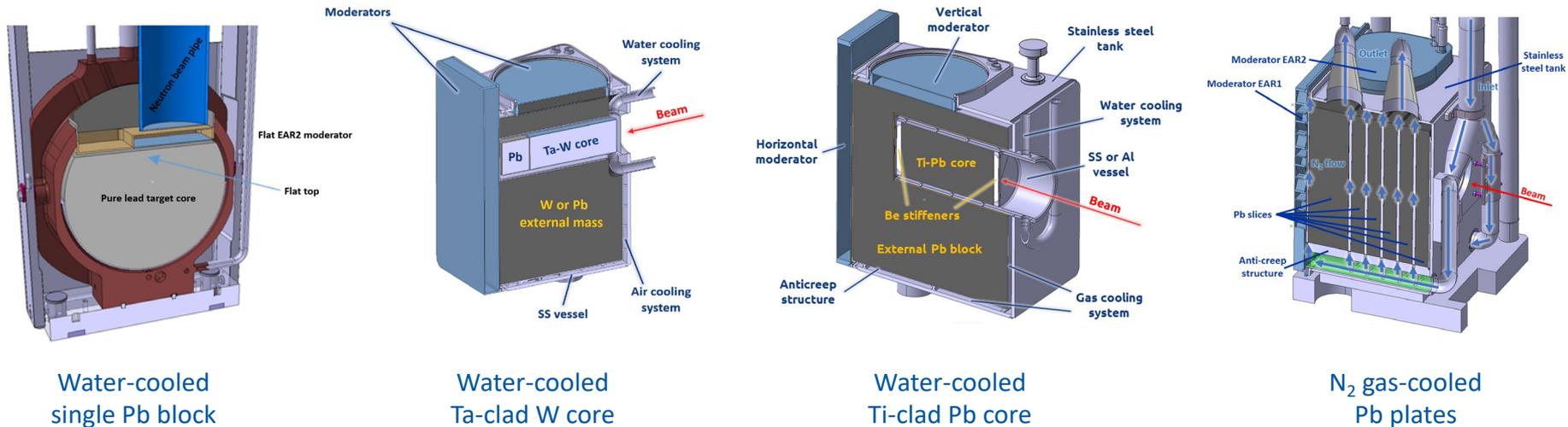
Design studies for the 3rd-gen target

Many different design solutions investigated:

- Core materials (Pb, Ta, W, ...)
- Cladding materials (Ta, Ti64, Inconel, ...)
- Cooling fluids (water, N₂, Ar, ...)

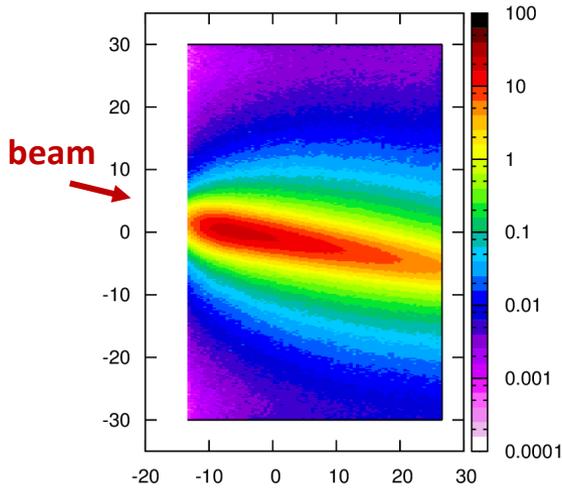


Examples:

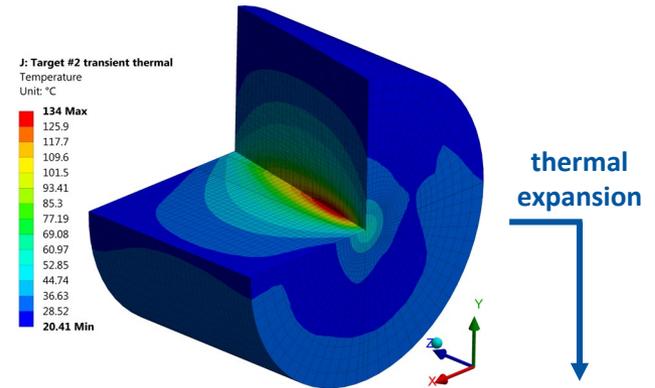


Design studies for the 3rd-gen target

Energy deposition (Monte Carlo)

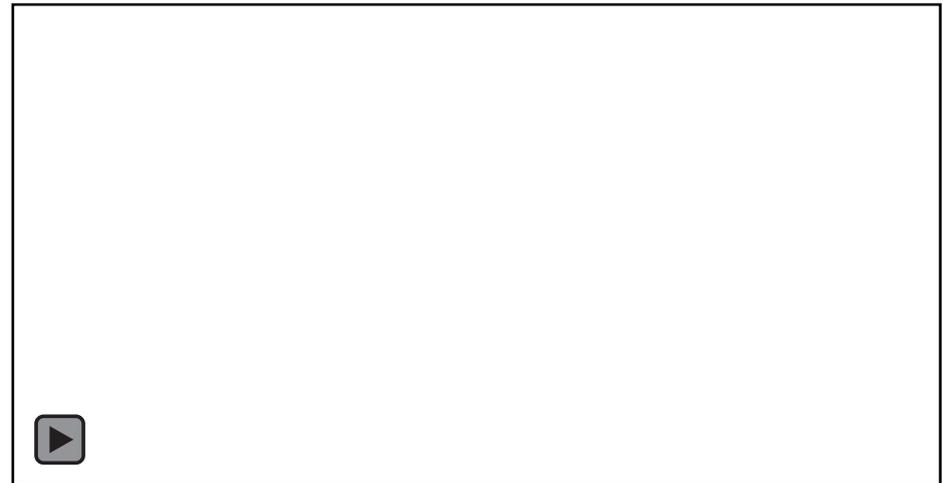
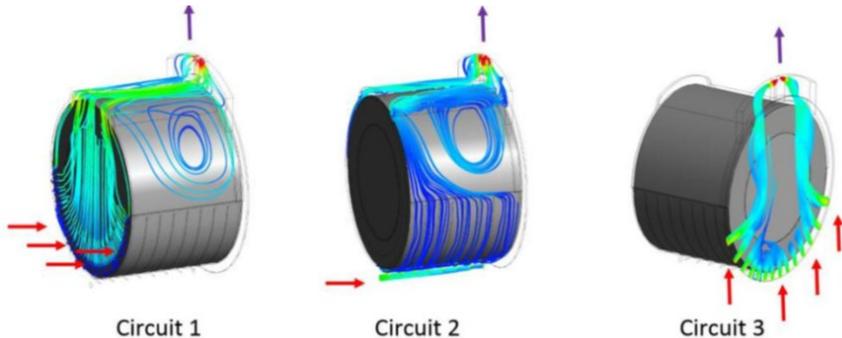


Temperature (thermal FEM)



32 kJ in 6-ns (RMS) → Stress wave propagation

Heat transfer coefficient (CFD)



The 3rd-gen n_TOF target

➡ Nitrogen circuit

➡ Demineralized water circuit

➡ Borated water circuit

➡ Beam

Cover
(St Steel 316L Low cobalt <0.1%)

Lead wedge
(Pur lead 99.99%)

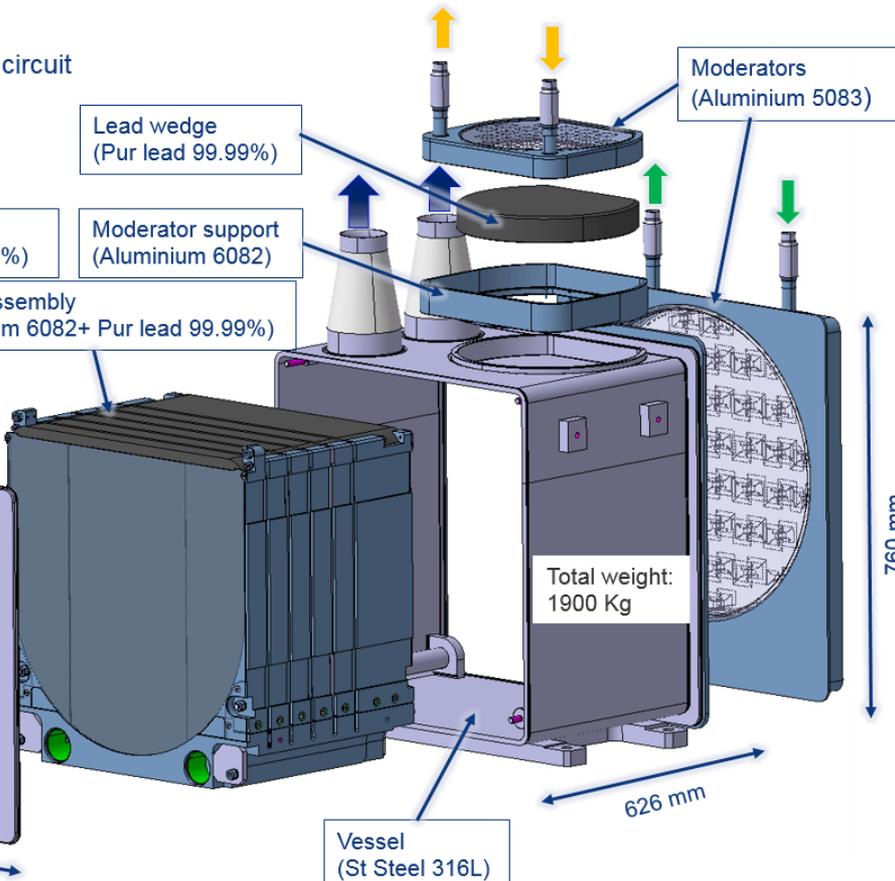
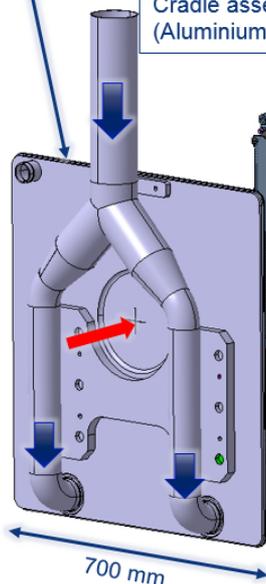
Moderator support
(Aluminium 6082)

Cradle assembly
(Aluminium 6082+ Pur lead 99.99%)

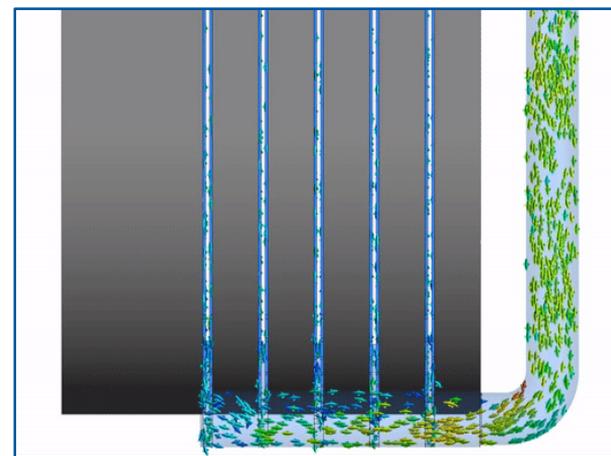
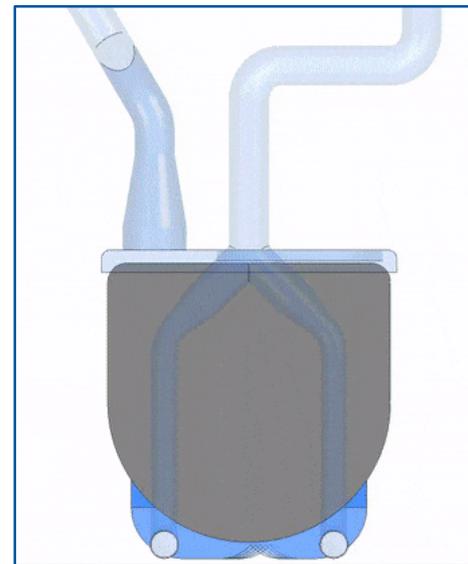
Moderators
(Aluminium 5083)

Total weight:
1900 Kg

Vessel
(St Steel 316L)



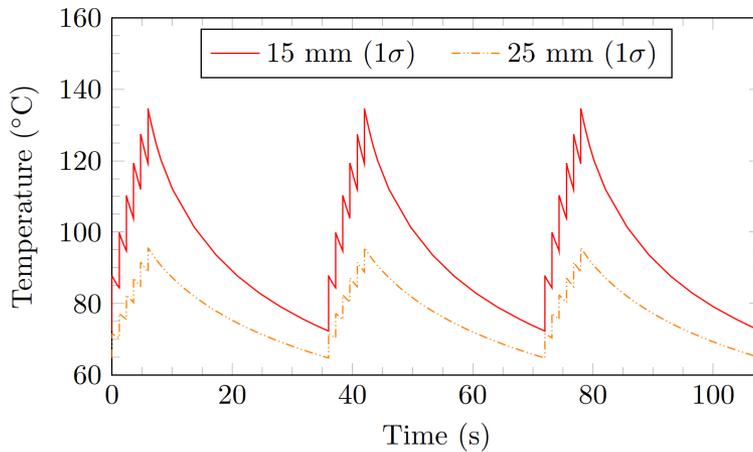
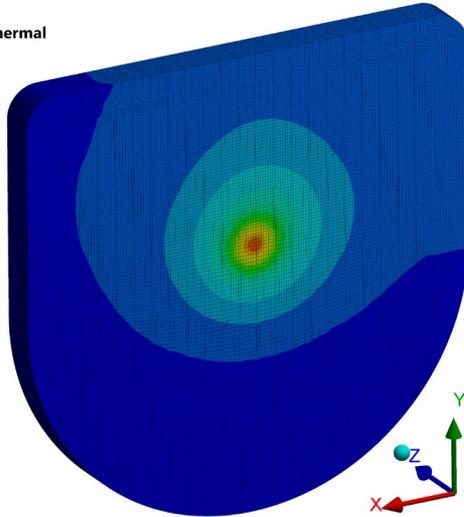
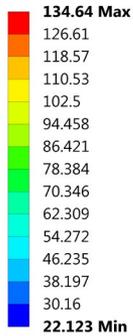
760 mm



Thermal behaviour

K: Pb transient thermal

Temperature
Unit: °C



Design parameters

Pulse intensity	10^{13} p ⁺
Beam momentum	20 GeV/c
Pulse energy	32 kJ
Pulse length	25 ns (4σ)
Beam size (Gaussian)	15 mm (1σ)
Average intensity	1.67×10^{12} p ⁺ /s
Average current	0.27 μA
Average power	5.4 kW
Peak current	91.3 A
Peak power	1.8 TW

- Peak temperature in 2nd slice: 135°C
- Lead melting temperature: 327°C

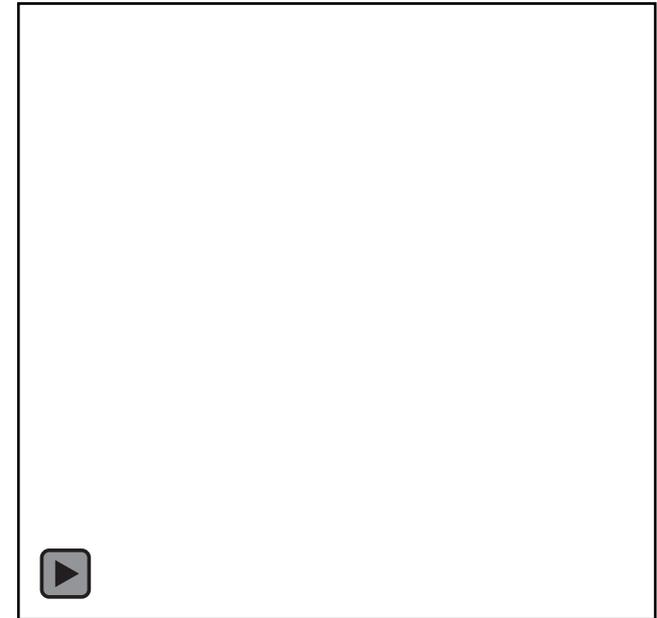
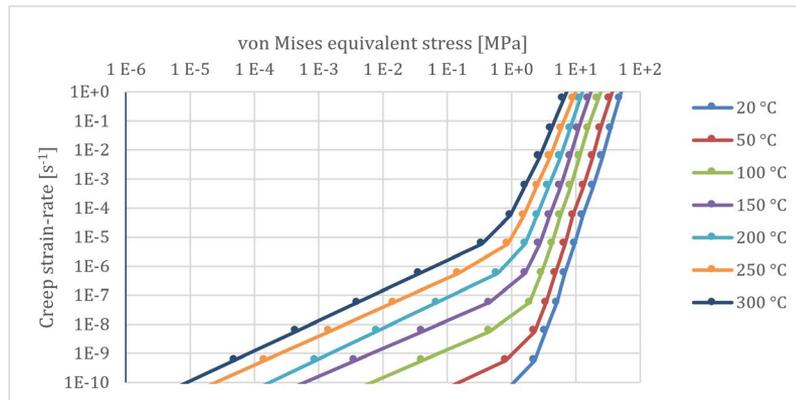
Studies on creep effect

Lead creep → risk of obstructing cooling channels

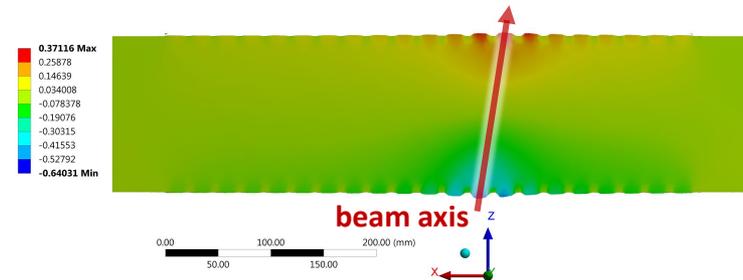
New User Programmable Feature coded in ANSYS

For each segment on a log-log plane:

$$\dot{\epsilon} = c \cdot \sigma^m$$



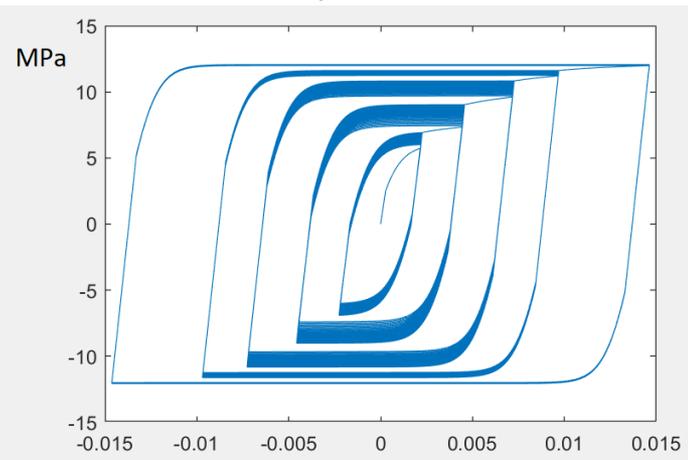
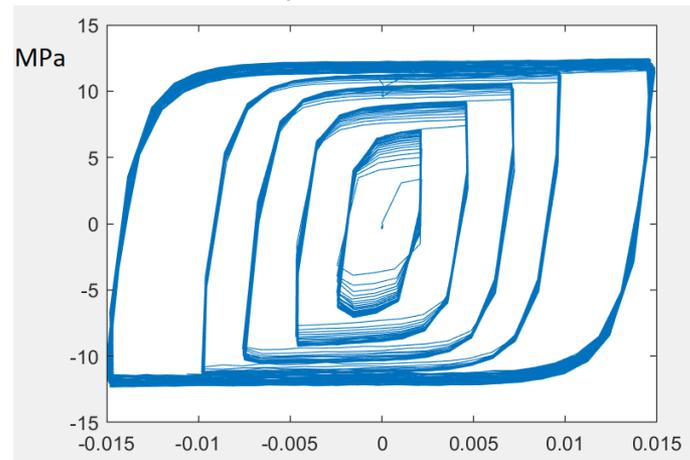
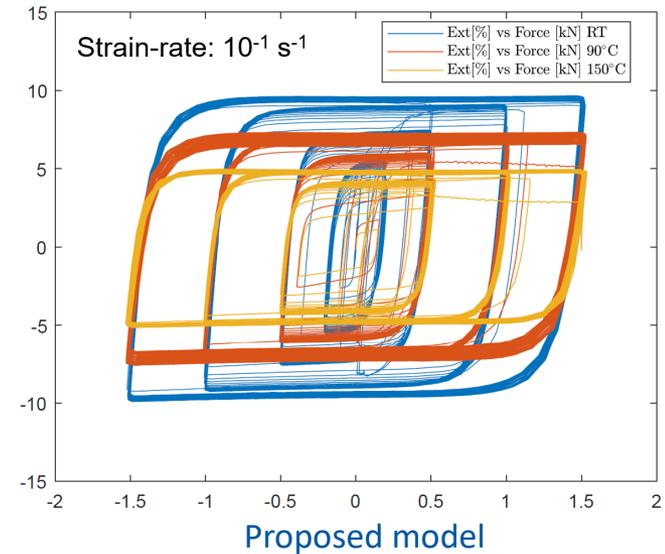
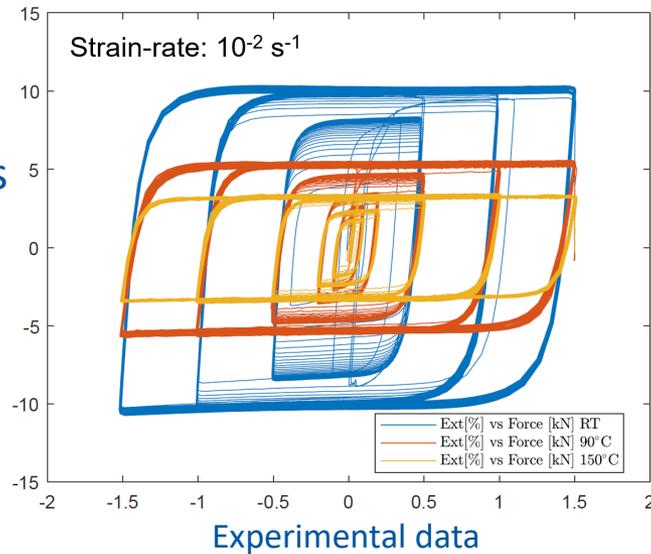
- 2×10⁸ s simulated (6 years and 4 months of continuous operation or twice the target lifetime)
- Also useful to perform CFD simulations in degraded scenarios



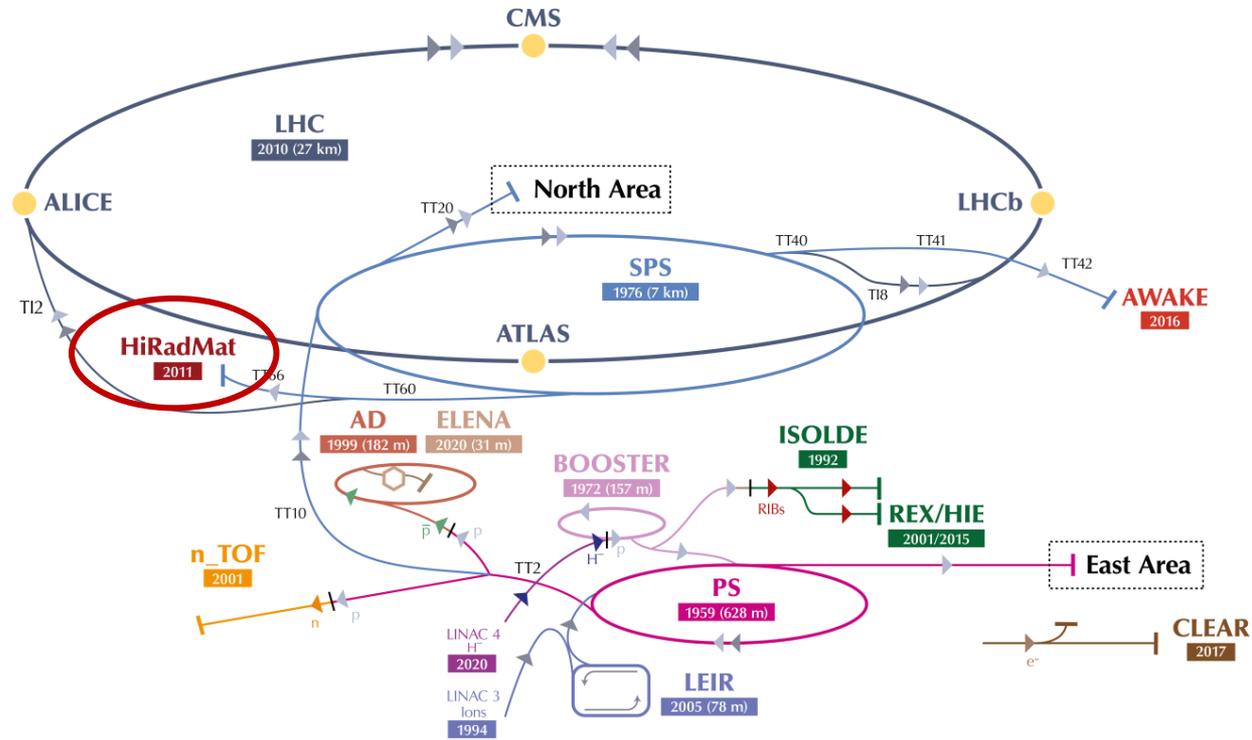
(deformations amplified for better visualization)

Pb constitutive model for cyclic plasticity

- Cyclic mechanical tests performed at NTNU



Beam irradiation tests in HiRadMat

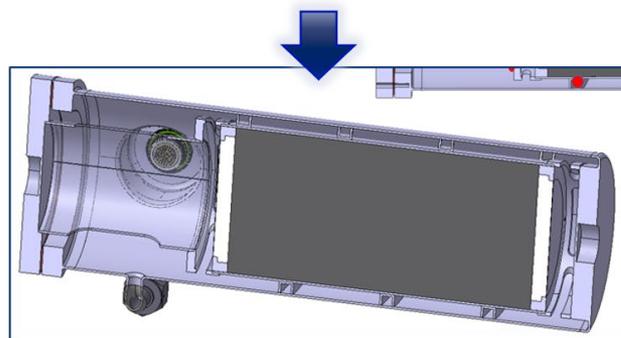
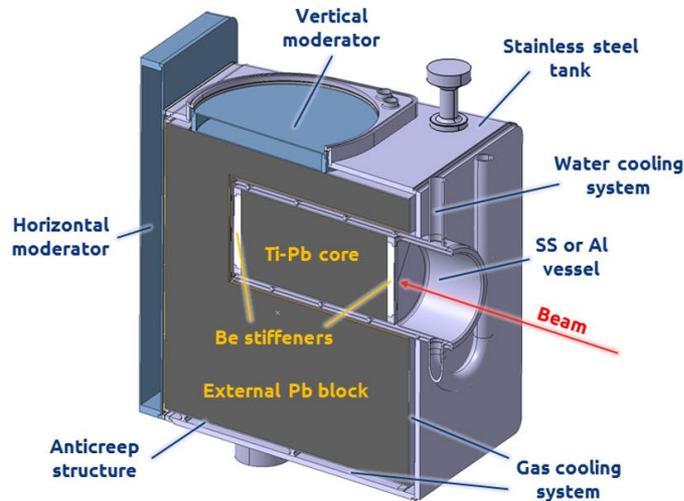


▶ H^- (hydrogen anions) ▶ p (protons) ▶ ions ▶ RIBs (Radioactive Ion Beams) ▶ n (neutrons) ▶ \bar{p} (antiprotons) ▶ e^- (electrons)

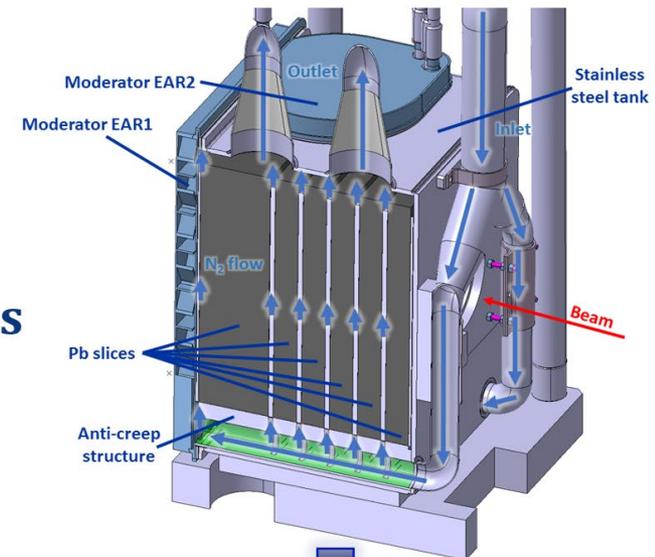
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Beam irradiation tests in HiRadMat

Ti-6Al-4V-clad lead

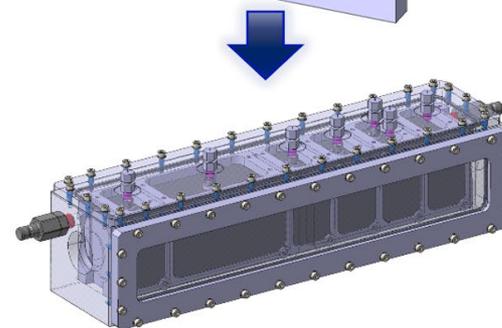


N₂-cooled lead slices



Design solutions

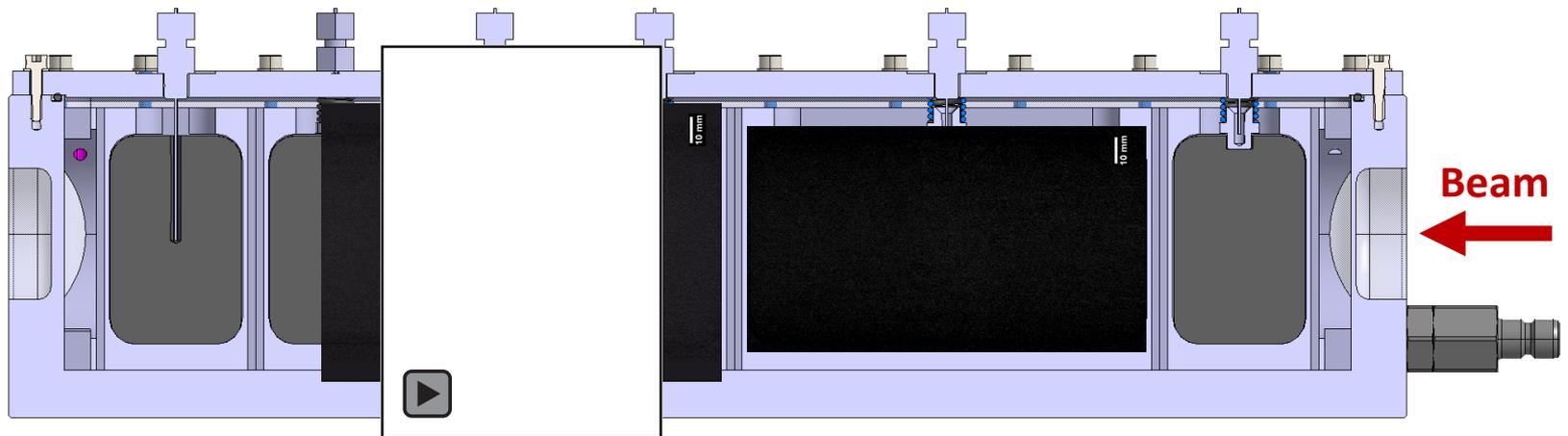
HiRadMat prototypes



Beam irradiation tests in HiRadMat

PIE N₂-cooled Pb prototype

Neutron tomography at NEUTRA (PSI)



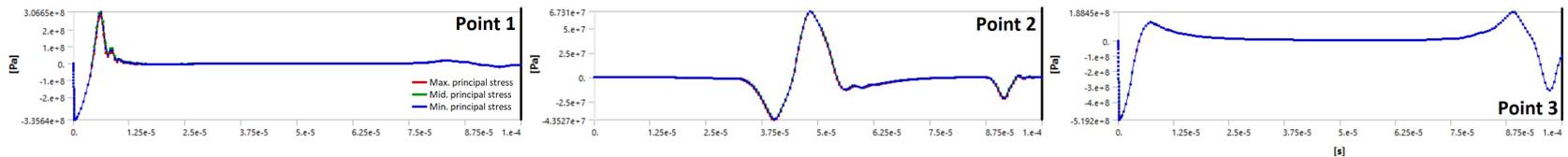
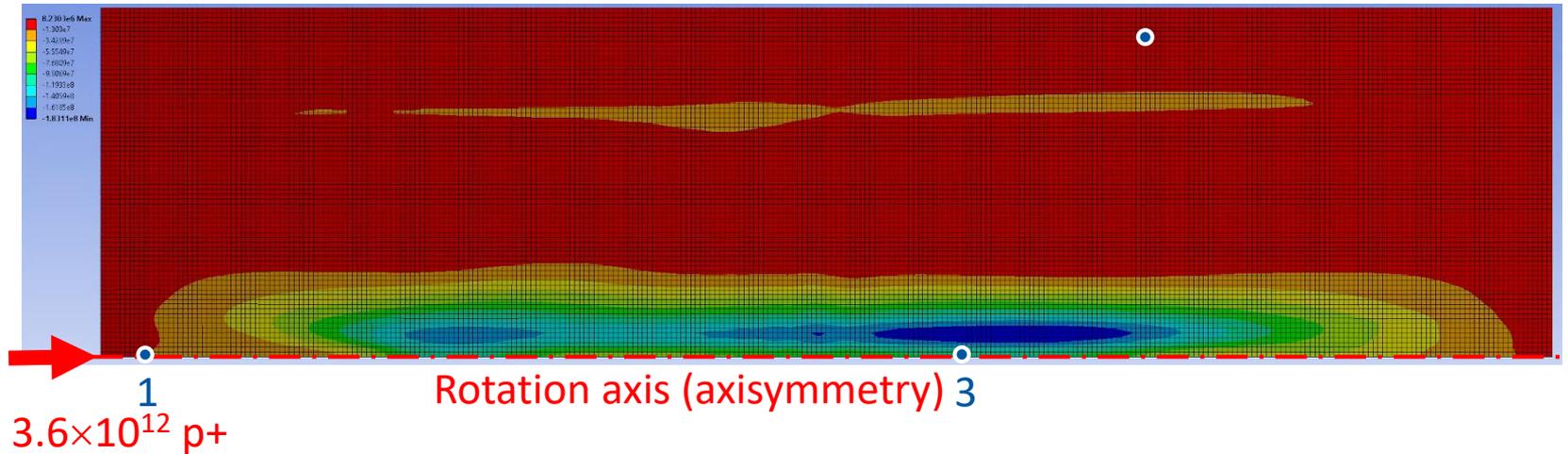
No detectable voids down to 100 μ m

Beam irradiation tests in HiRadMat

Ti64-clad Pb prototype

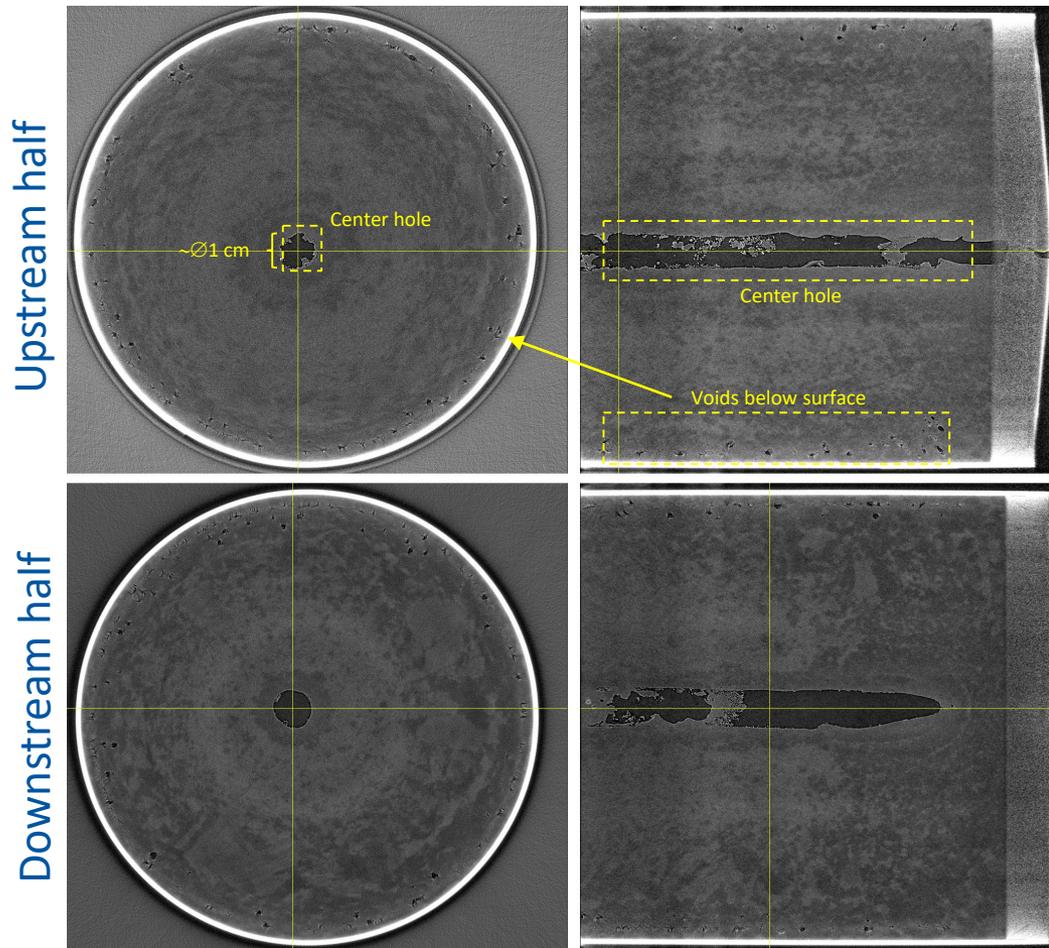
Lead cylinder

2



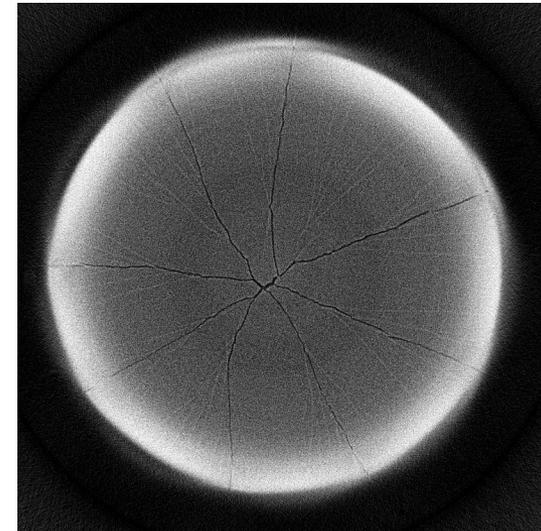
Huge oscillations of stress on the beam axis and below the cylindrical surface

Beam irradiation tests in HiRadMat

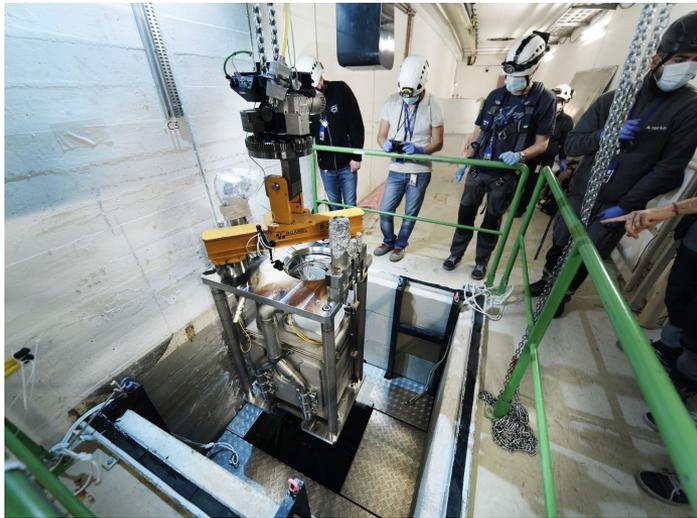


- After 1000 pulses of $3.6 \times 10^{12} \text{ p}^+$
- Neutron tomography at ILL (Grenoble)
- Voids in the lead cylinder
- Ti-6Al-4V cladding intact and content sealed

Upstream beryllium plate cracked



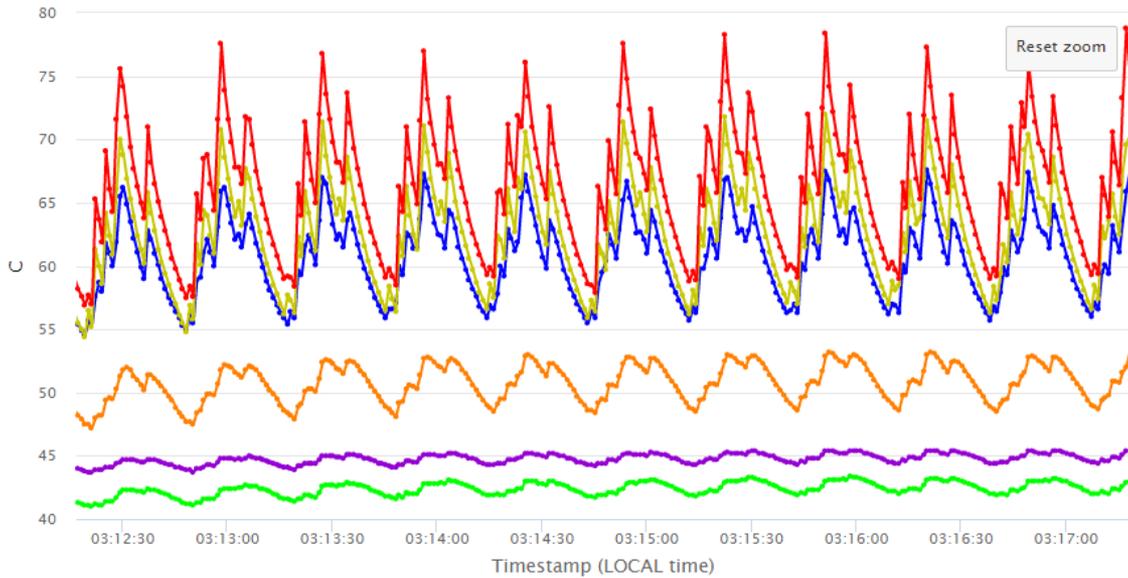
3rd gen target installed in 2021



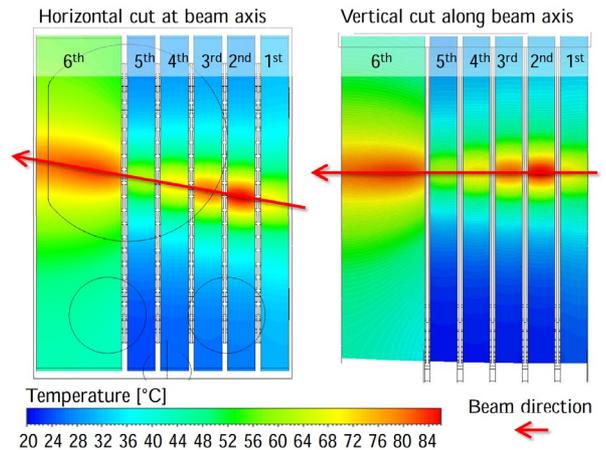
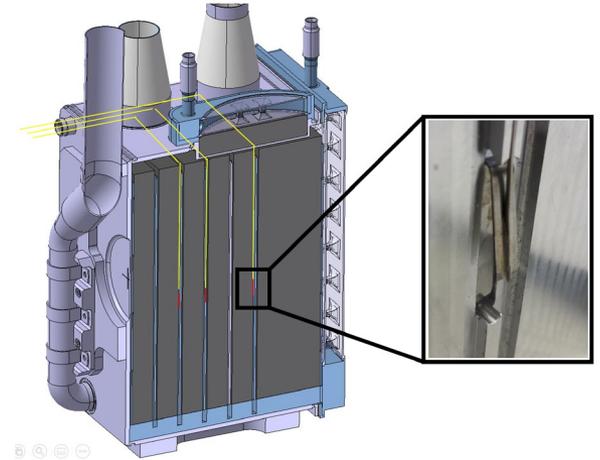
Target operation in 2021-2022

n_TOF Target Thermocouples

Numbered from proton side to neutron side

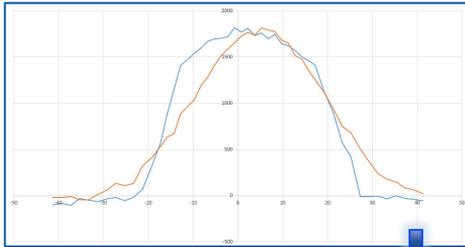


- NTOFTarget1:Temperature:thermocouple6
- NTOFTarget1:Temperature:thermocouple5
- NTOFTarget1:Temperature:thermocouple4
- NTOFTarget1:Temperature:thermocouple3
- NTOFTarget1:Temperature:thermocouple2
- NTOFTarget1:Temperature:thermocouple1

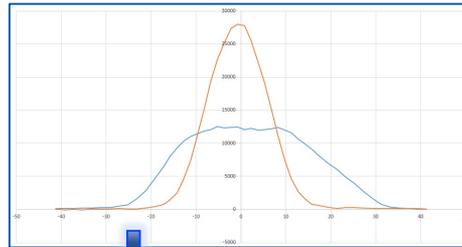


Target operation in 2021-2022

15×15 mm² RMS

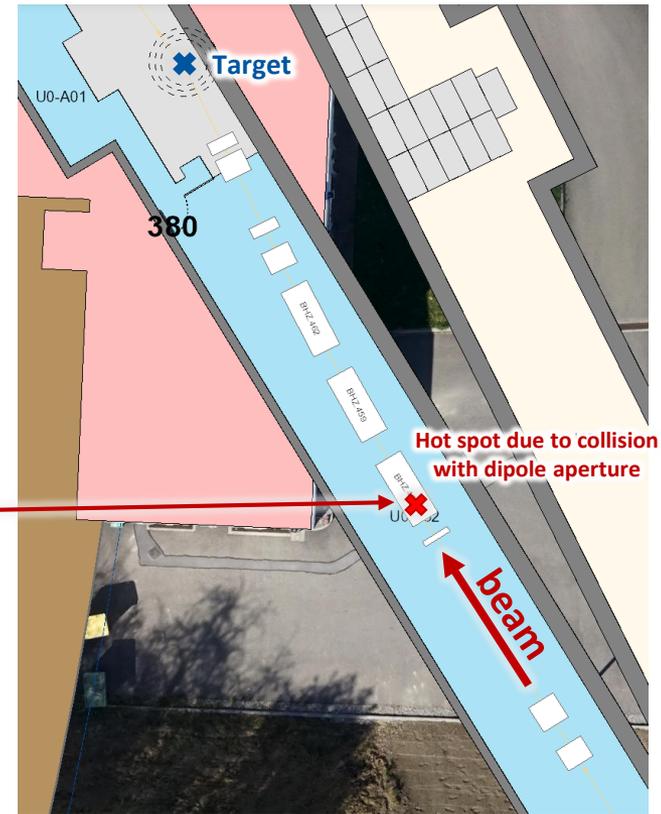


16×7 mm² RMS

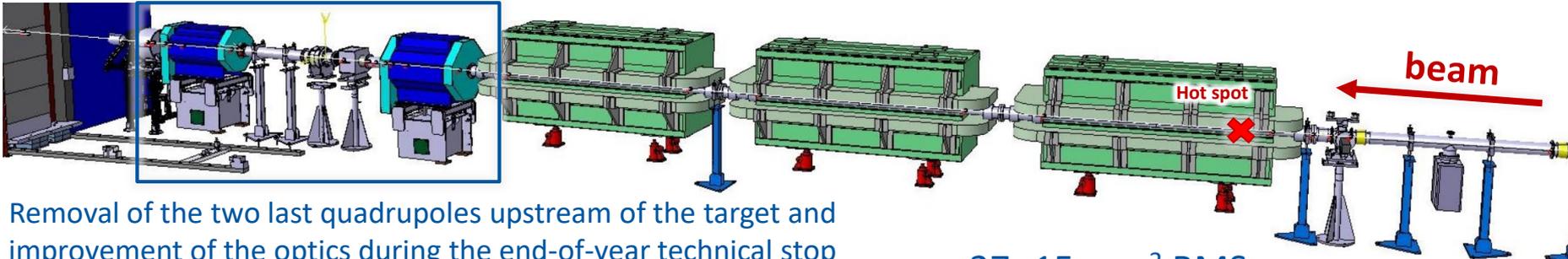


Dose rate (measured at 1 m) after modifications in the beam line with improved optics during the end-of-year technical stop

ID	Reference	Position	Dose rate [$\mu\text{Sv/h}$]				
			Date: 15-09-21	Date: 28-09-21 (8:15)	Date: 16-11-21 (14:50)	Date: 17-05-22 (13:15)	Date: 13-09-22 (17:50)
			Cool down time: 30 h	Cool down time: 31 h			
1	-	Start of FTN	3	2.5	1	0.8	4
2	QFO.435	UPSTREAM	4	2.5	2	1.7	38
3	QFO.435	DOWNSTREAM	4	3.5	2	3	46
4	DHZ.436	DOWNSTREAM	3.5	1.7	2	1.3	26
5	QDE.450	UPSTREAM	33	18	12	12	33
6	QDE.450	DOWNSTREAM	38	18.5	13	15	37
7	DVT.451	DOWNSTREAM	13	3.6	4	10	25
8	-	Between DVT.451 and FTN.BTV454	-	30 (below)	-	-	-
9	-	Between DVT.451 and FTN.BTV454	-	-	-	-	12
10	FTN.BTV454	UPSTREAM	97	32	20	15	20
11	FTN.BTV454	DOWNSTREAM	103	42	25	14	32
12	BHZ.456	MIDDLE	360	76	45	20	35
13	BHZ.456	DOWNSTREAM	116	35	25	17	22
14	BHZ.459	DOWNSTREAM	74	28.5	19	36	47
15	BHZ.462	DOWNSTREAM	70	26	20	60	100
16	old QFO.465	DOWNSTREAM	50	25	21	-	-
17	UWB.474	UPSTREAM	-	-	-	67	69
18	UWB.474	DOWNSTREAM	62	25.7	32	64	76
19	old QDE.480	UPSTREAM	83	53.5	56	-	84
20	old QDE.480	DOWNSTREAM	126	82	93	-	-
21	BSG.484	UPSTREAM	-	-	-	154	170
22	BSG.484	DOWNSTREAM	127	100	99	150	193
23	-	Vacuum chamber in the wall	-	-	-	124	170



Target operation in 2021-2022



27×15 mm² RMS

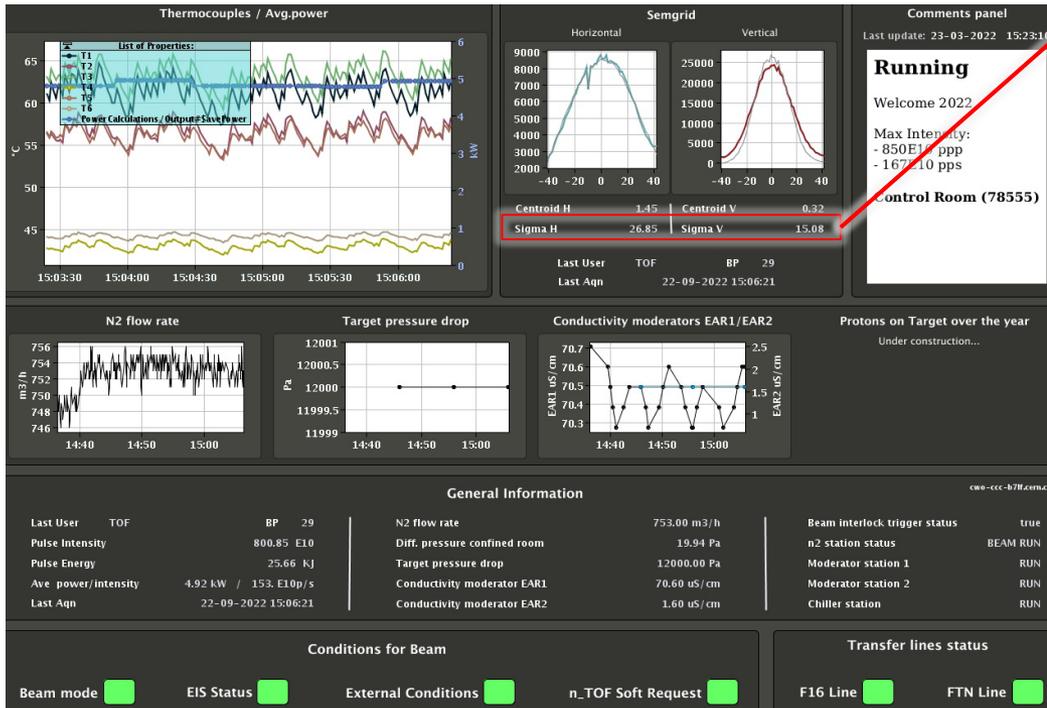
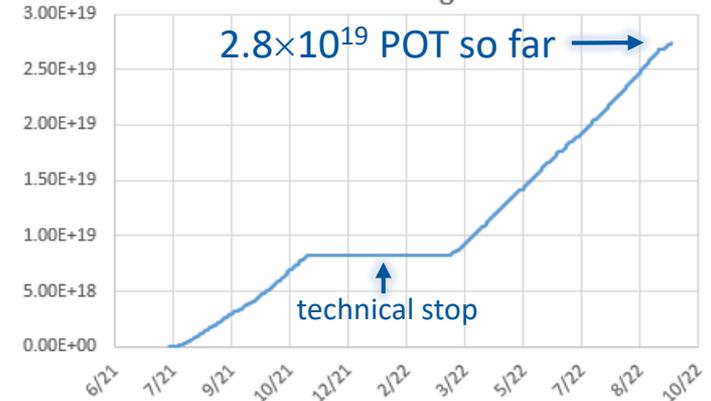
Beam spot even larger than design assumptions

possible to increase intensity

11	FTN.BT454	DOWNSTREAM	193	42	25	14	32
12	BH2.456	MIDDLE	360	76	45	20	35
13	BH2.456	DOWNSTREAM	116	35	25	17	22

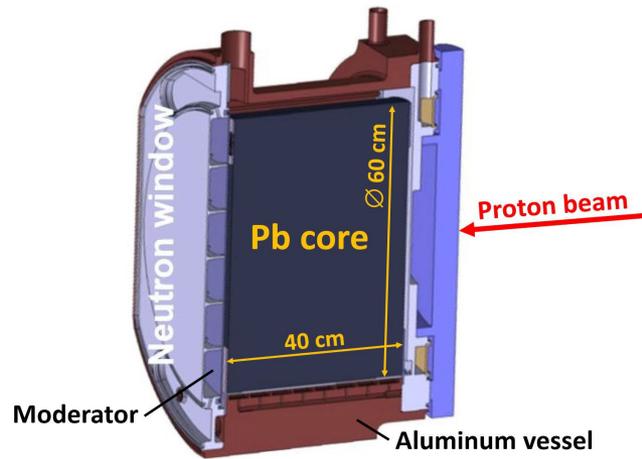
Dose rate at hotspot back to acceptable values

Protons on target

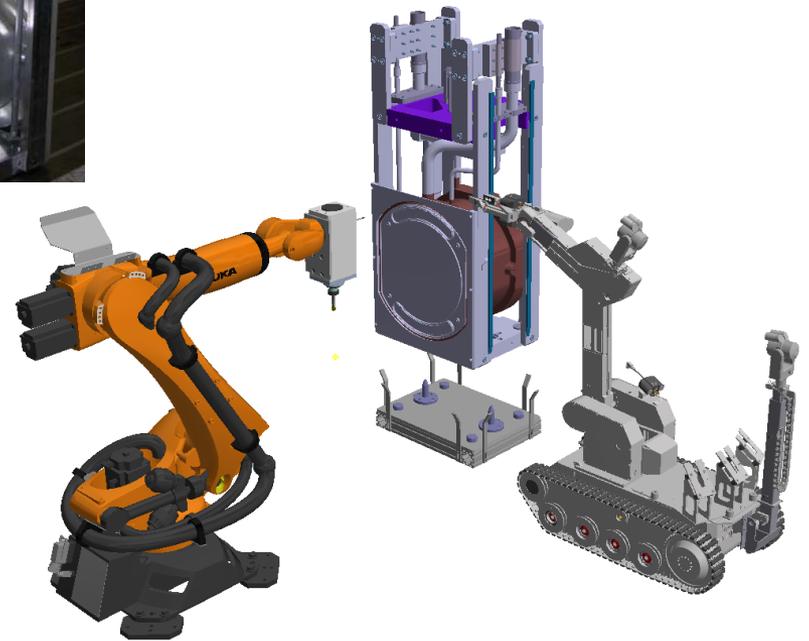


2nd gen target autopsy

- Single lead cylinder ($\text{Ø}60 \times 40 \text{ cm}^2$) in aluminium vessel, water-cooled
- In operation from 2009 to 2018

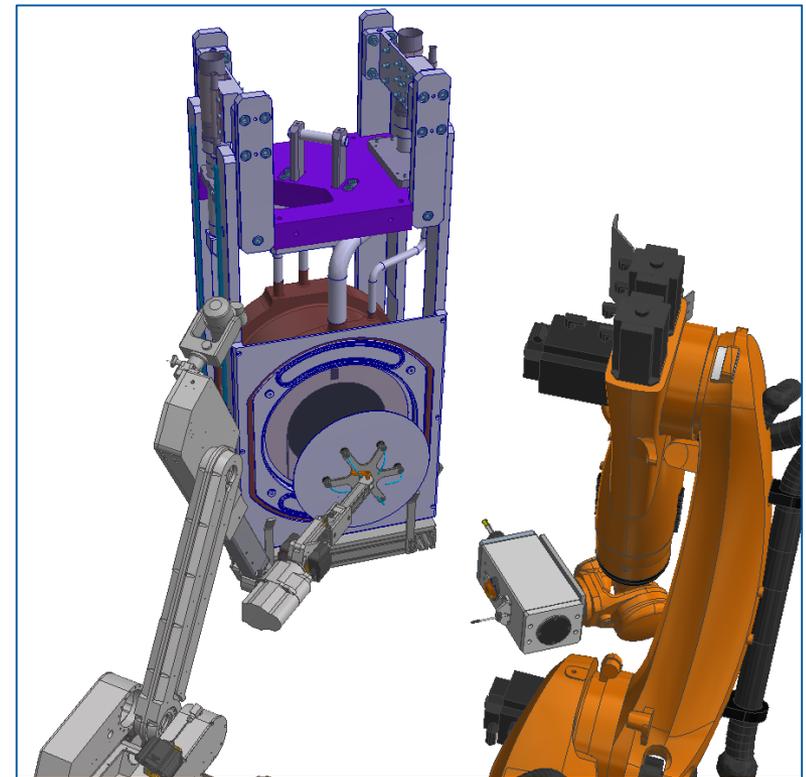
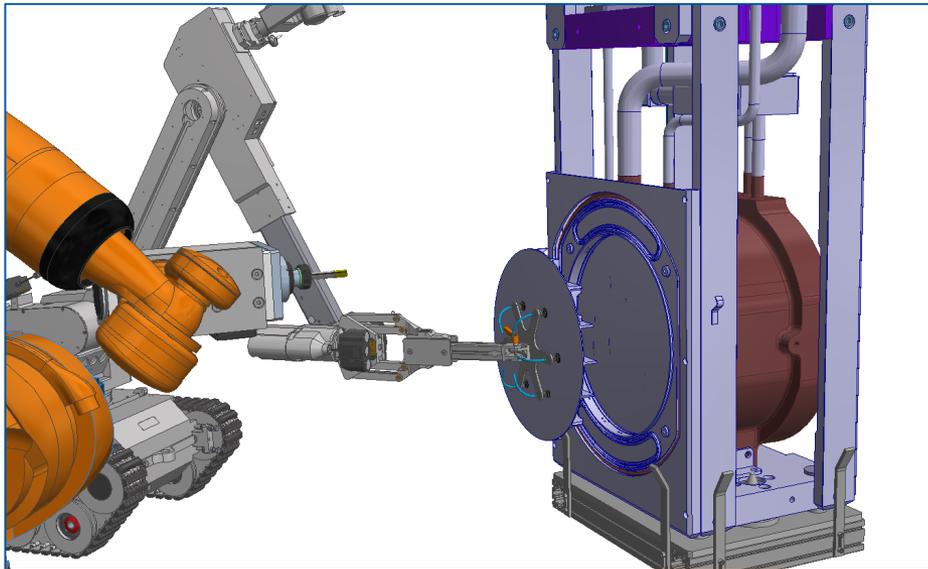


- Autopsy and radioactive waste packaging planned for summer 2023
- Executed with KUKA and Telerob robots



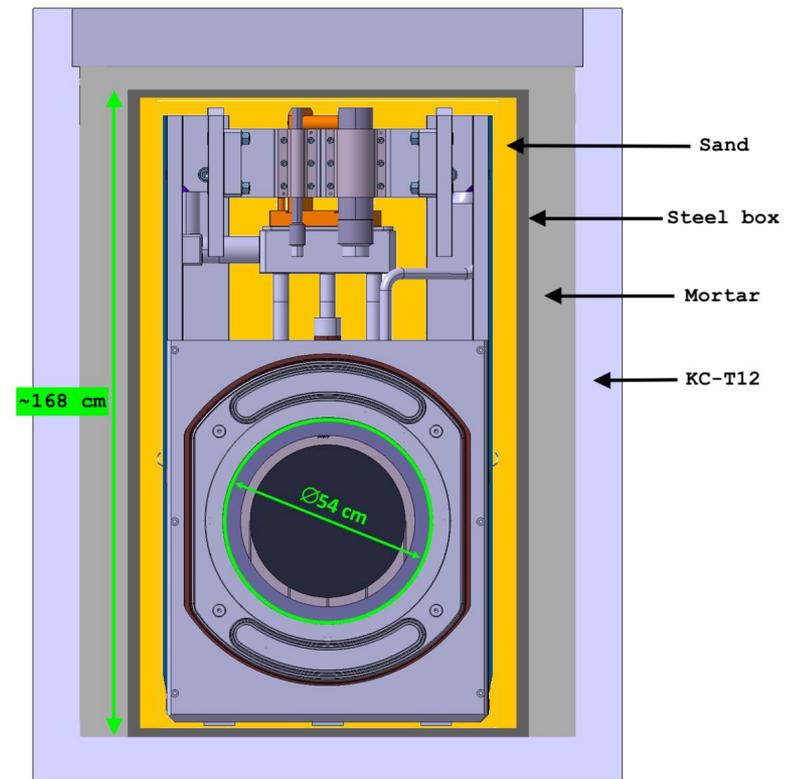
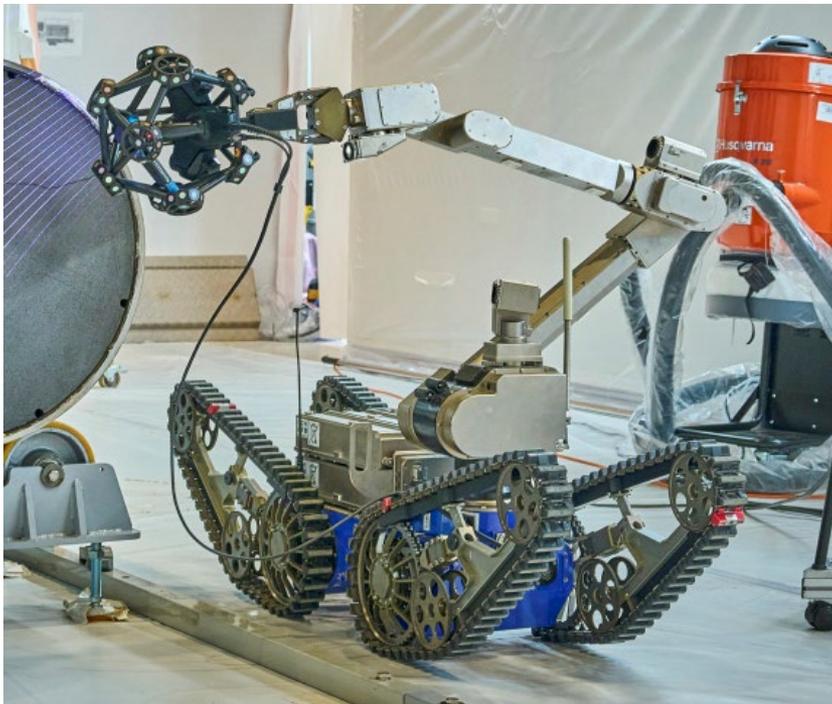
2nd gen target autopsy

- The borated-water moderator casing will be cut out and inspected to assess the presence of boron deposits
- The downstream window will also be cut out to expose the surface of the Pb core
- The upstream face of the Pb core will also be exposed with a similar procedure



2nd gen target autopsy

- Scanning of Pb surface by 3D scanner to quantify plastic deformation due to beam interaction and creep
- Cutting of the target frame for compact package in KC-T12 container for disposal in Swiss repository



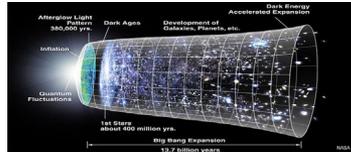
Summary

- The n_TOF Target #3 successfully operates since July 2021 with a new design based on N₂-cooled pure Pb plates. The new design is the result of 5 years of studies including material characterization activities, constitutive modelling, and beam irradiation tests.
- The new target is equipped with instruments for live monitoring of temperature, beam profile, and cooling parameters, also used for beam interlocks.
- Improvements in proton beam line and optics led to contained dose and thermo-mechanical loads opening possibility for further improvement in target performance
- An autopsy of the spent 2nd generation target is planned for summer 2023 to provide feedback on the long term structural effects on the target, after a decade of target operation
- Additional references:
 - R. Esposito et al., *Phys. Rev. Accel. Beams* **24**, 093001 (2021)
 - R. Esposito et al., *J. Neutron Res.* **22**, 221 (2020)
 - R. Esposito, *Design, prototyping, and thermo-mechanical modelling of a neutron spallation target impacted by high-energy proton-beam pulses in the n_TOF facility at CERN*, Ph.D. dissertation, EPFL, Lausanne, Switzerland (2022)

Additional slides

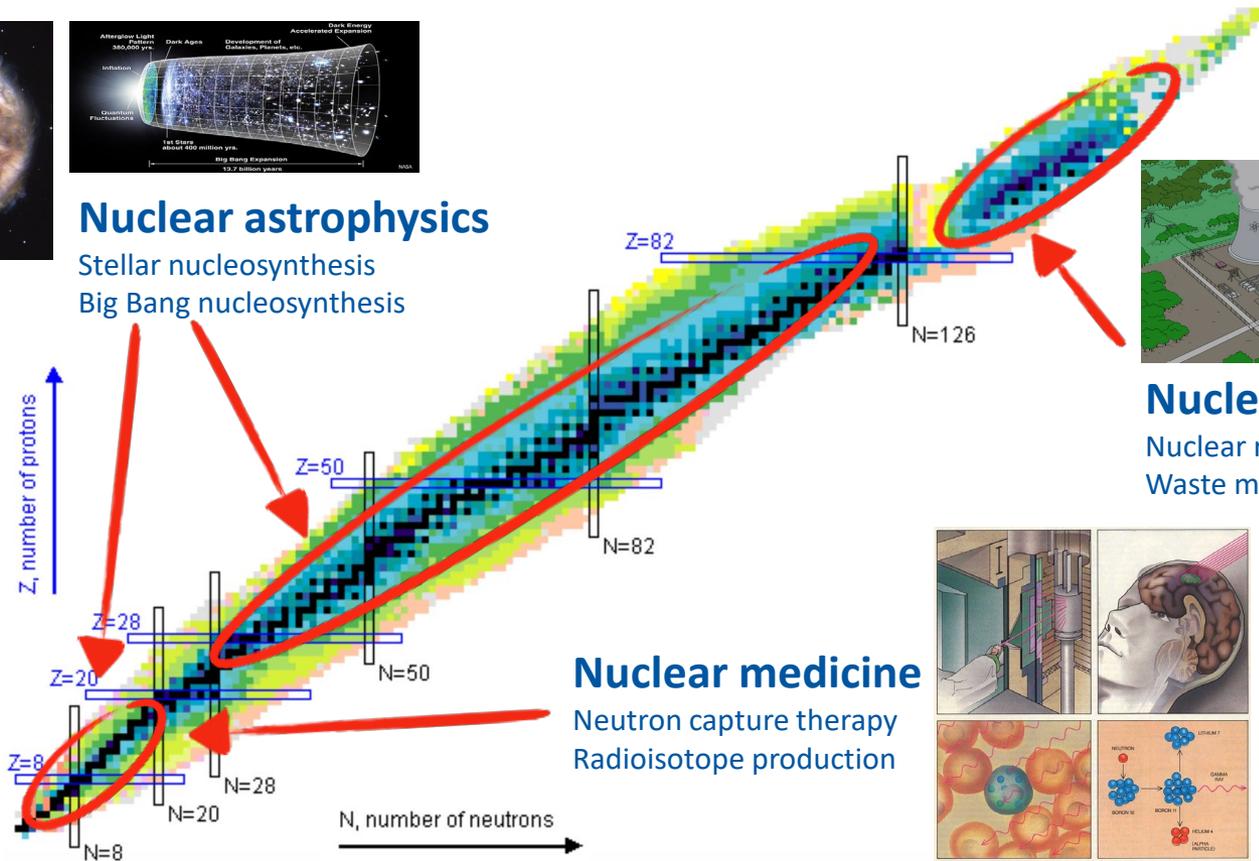
The n_TOF facility at CERN

Chart of nuclides



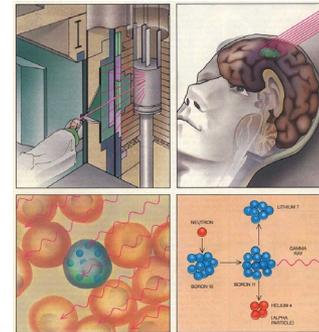
Nuclear astrophysics

Stellar nucleosynthesis
Big Bang nucleosynthesis



Nuclear technology

Nuclear reactors (energy)
Waste management



Nuclear medicine

Neutron capture therapy
Radioisotope production

The n_TOF facility at CERN

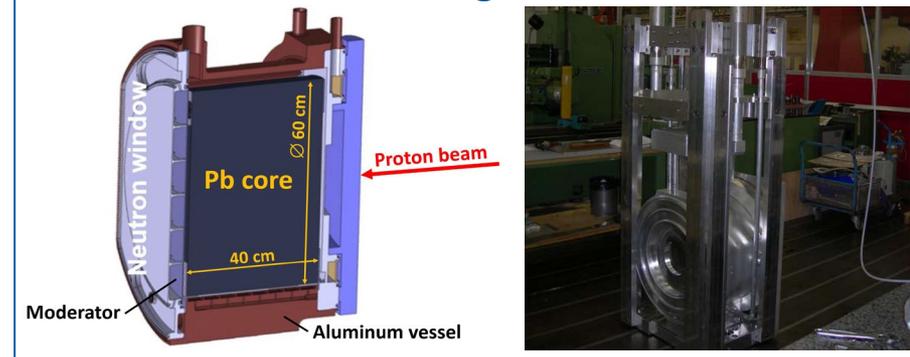
Target #1 and target #2

- Target #1 operated from 2000 to 2004
- Target #2 operated from 2009 to 2018
- Based on pure lead cooled by water
- Abnormal increase of radioactivity in the cooling circuit
- Erosion/corrosion issues
- Cooling water contamination with radioactive products from target

Target #1

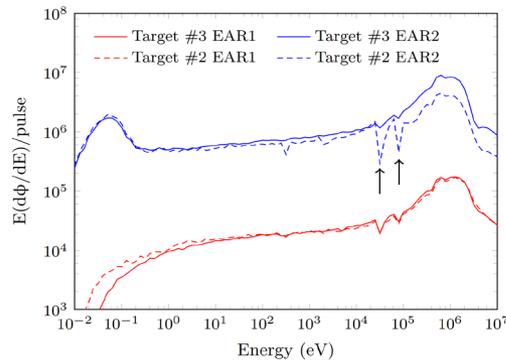


Target #2

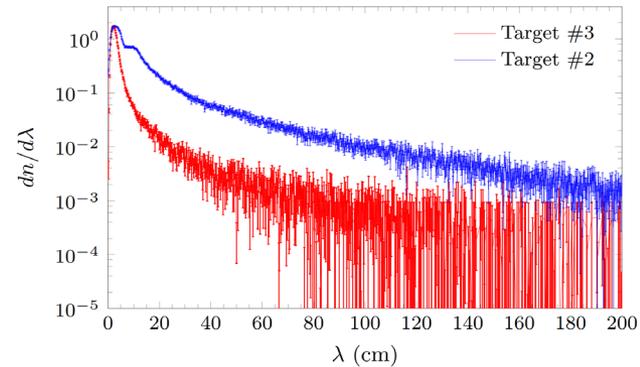


Target #3: physics performance

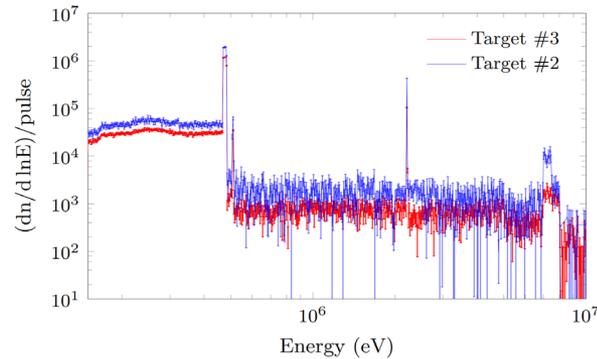
Neutron flux



Resolution function

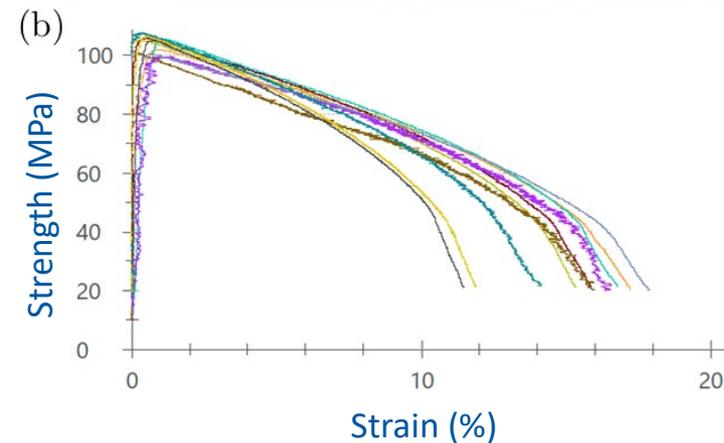
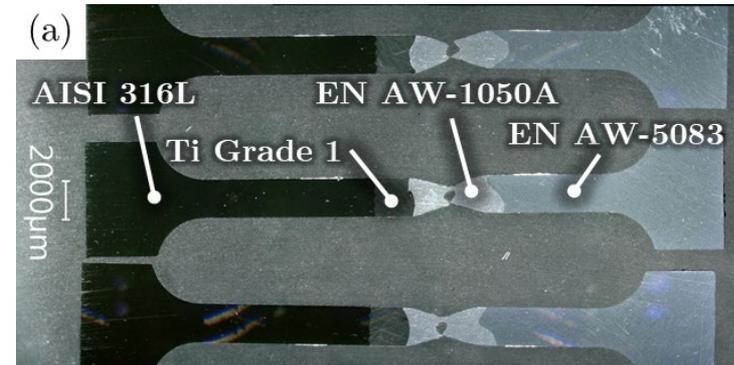
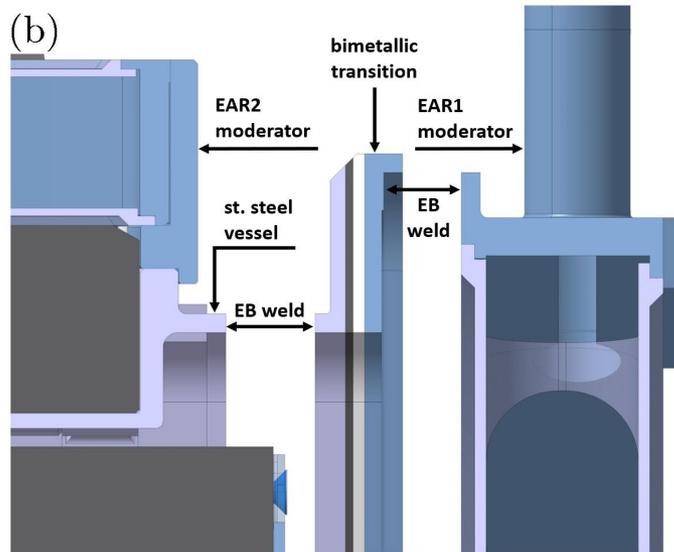
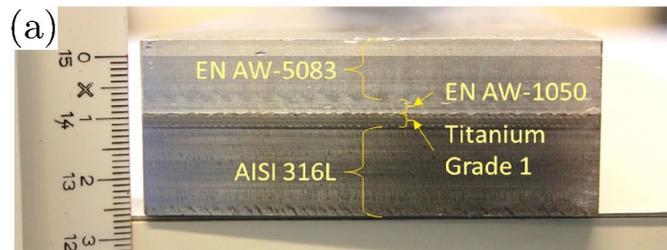


Photon background



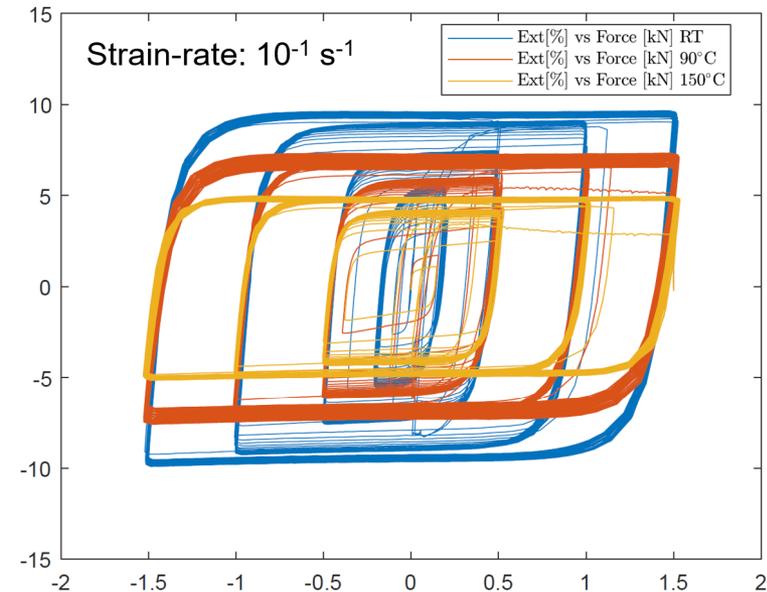
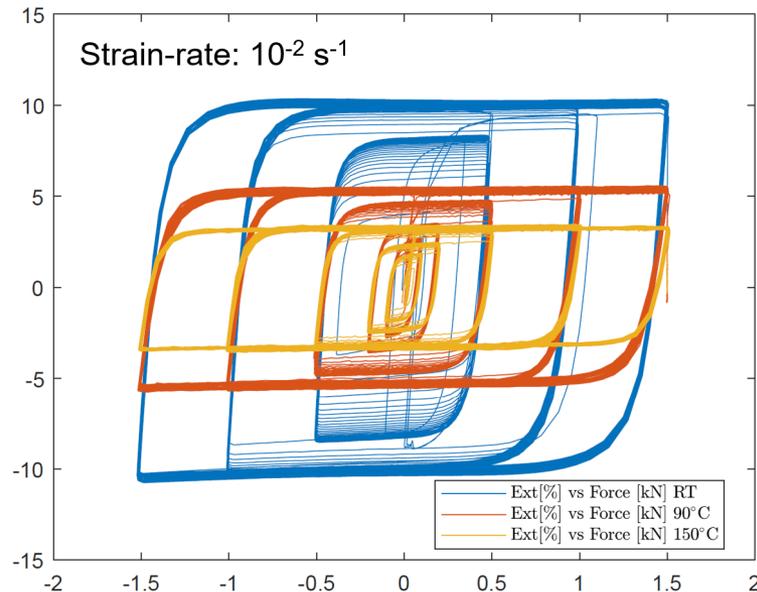
Neutron moderators

Explosive-welded bond between stainless steel vessel and Al-5083 moderator



Pb constitutive model for cyclic plasticity

- Better predictions of long term Pb behaviour → Multi-pulse simulations →
→ Pb constitutive behaviour under cyclic plasticity
- Strain-controlled cyclic tests at different temperatures and strain-rates (collaboration with Norwegian University of Science and Technology)
- Observed: Bauschinger effect, cyclic-hardening, non-Masing behaviour.
- Non reproducible by traditional models generally available in commercial FEM software



Pb constitutive model for cyclic plasticity

- *Incremental plasticity* model proposed
- Able to reproduce Bauschinger effect, cyclic hardening, and non-Masing behaviour.

$$\begin{aligned} \boldsymbol{\varepsilon} &= \boldsymbol{\varepsilon}^e + \boldsymbol{\varepsilon}^p + \boldsymbol{\varepsilon}^{th} \\ \boldsymbol{\sigma} &= \mathbb{E} : \boldsymbol{\varepsilon}^e \\ f &= \sqrt{\frac{3}{2} (\boldsymbol{\sigma}' - \mathbf{X}) : (\boldsymbol{\sigma}' - \mathbf{X})} - R - \sigma_{y0} = 0 \\ \dot{\boldsymbol{\varepsilon}}^p &= \dot{\lambda} \mathbf{N} = \dot{\lambda} \frac{\frac{3}{2} (\boldsymbol{\sigma}' - \mathbf{X})}{\sqrt{\frac{3}{2} (\boldsymbol{\sigma}' - \mathbf{X}) : (\boldsymbol{\sigma}' - \mathbf{X})}} \\ \dot{\lambda} &= \sqrt{\frac{2}{3} \dot{\boldsymbol{\varepsilon}}^p : \dot{\boldsymbol{\varepsilon}}^p} \\ \dot{\mathbf{X}} &= \frac{2}{3} C \dot{\boldsymbol{\varepsilon}}^p - \gamma \mathbf{X} \dot{\lambda} \quad \text{Bauschinger effect}^1 \\ \dot{R} &= b(Q - R) \dot{\lambda} \quad \text{Cyclic hardening} \end{aligned}$$

Strain memory model ²

$$\begin{aligned} F &= \sqrt{\frac{2}{3} (\boldsymbol{\varepsilon}^p - \boldsymbol{\zeta}) : (\boldsymbol{\varepsilon}^p - \boldsymbol{\zeta})} - q = 0 \\ \dot{q} &= \frac{1}{2} (\mathbf{N} : \mathbf{n}^*) \dot{\lambda} \\ \dot{\boldsymbol{\zeta}} &= \frac{1}{2} (\dot{\boldsymbol{\varepsilon}}^p : \mathbf{n}^*) \mathbf{n}^* \\ \mathbf{n}^* &= \frac{\sqrt{\frac{2}{3}} (\boldsymbol{\varepsilon}^p - \boldsymbol{\zeta})}{\sqrt{\frac{3}{2} (\boldsymbol{\varepsilon}^p - \boldsymbol{\zeta}) : (\boldsymbol{\varepsilon}^p - \boldsymbol{\zeta})}} \\ Q &= Q_M - (Q_M - Q_0) e^{-2\mu q} \end{aligned}$$

Non-Masing behaviour

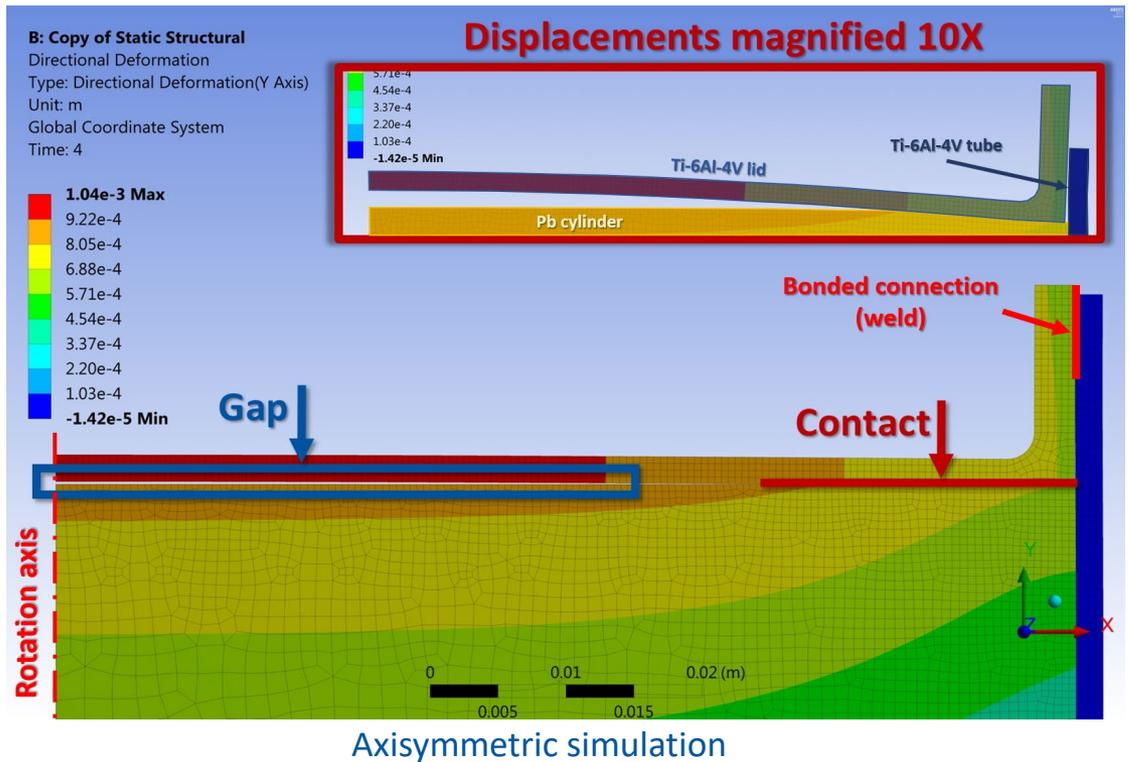
¹ P. J. Armstrong, C. O. Frederick, C.E.G.B. Report RD/B/N731, Berkeley, UK, 1966

² J. Lemaitre et al., *Mécanique des matériaux solides*, 3rd ed., Dunod, 2009

The Ti64-clad Pb prototypes

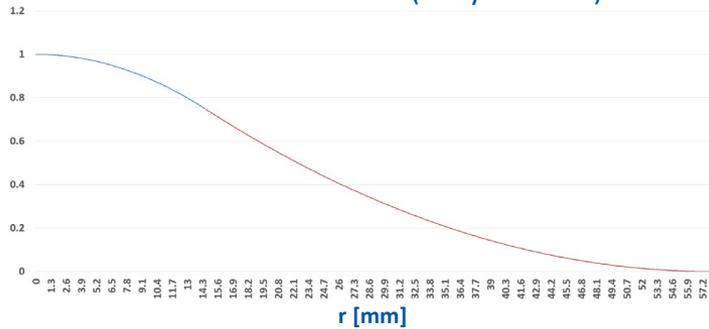
Deformation Ti-6Al-4V lid → Loss of contact with lead → Loss of conductivity and cooling efficiency

Prototypes manufactured:
Pb cylinder with
Ti-6Al-4V cladding



The Ti64-clad Pb prototypes

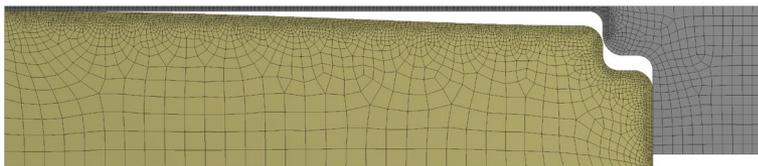
Desired contact pressure profile between Ti lid and Pb (axisymmetric)



Ti lid deformation due to desired contact pressure

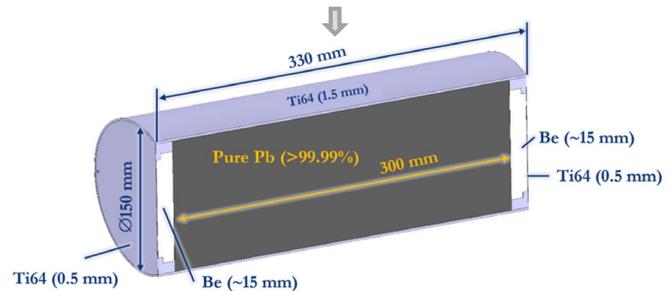
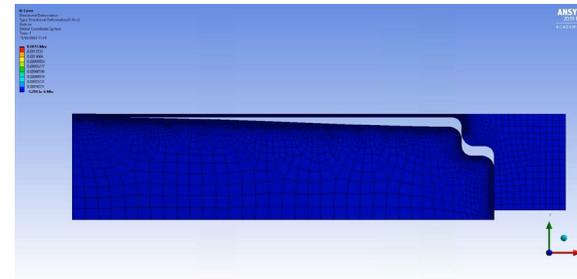


Be plate imposing desired deformation



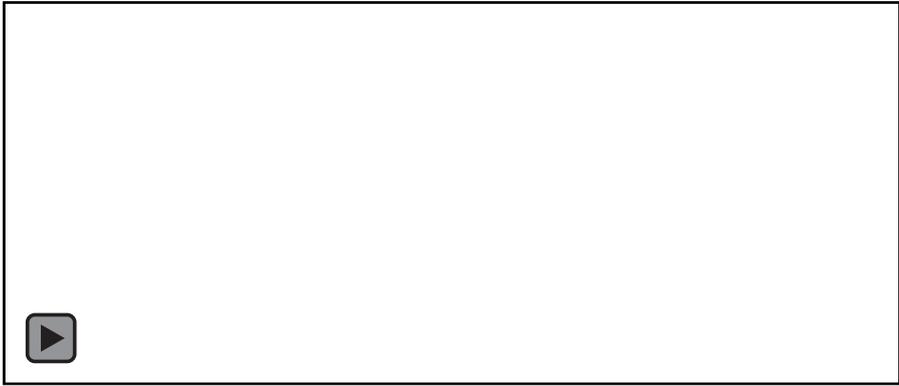
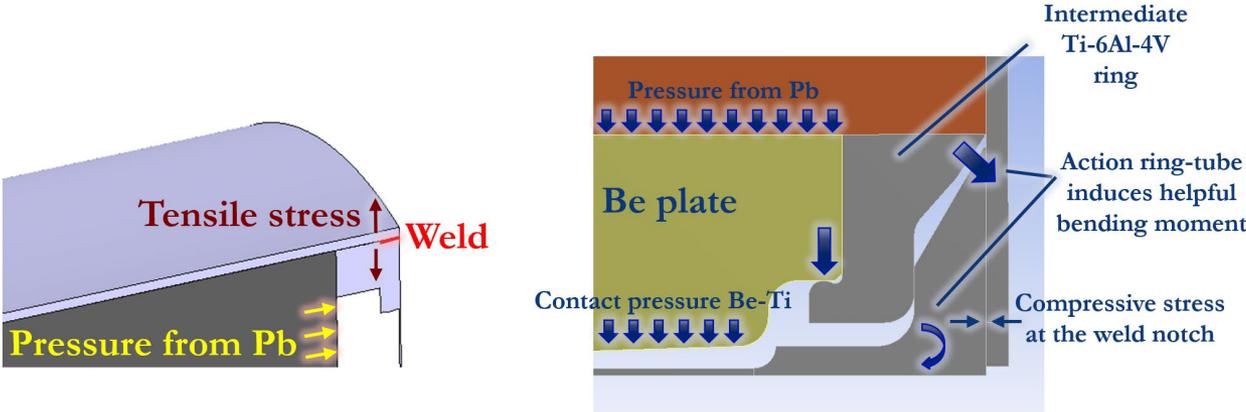
Be transparent to neutrons

Contact pressure as reaction of imposed deformation



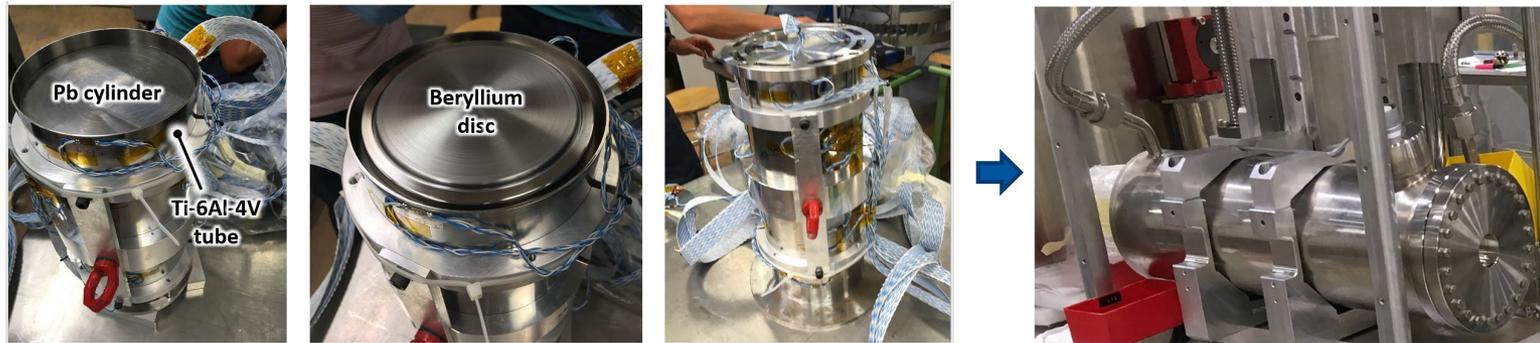
The Ti64-clad Pb prototypes

High bending stress (tensile) at the weld notch → Addition of intermediate ring to improve stress distribution



Beam irradiation tests in HiRadMat

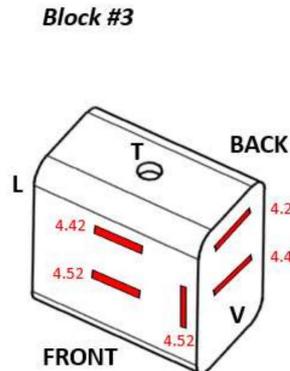
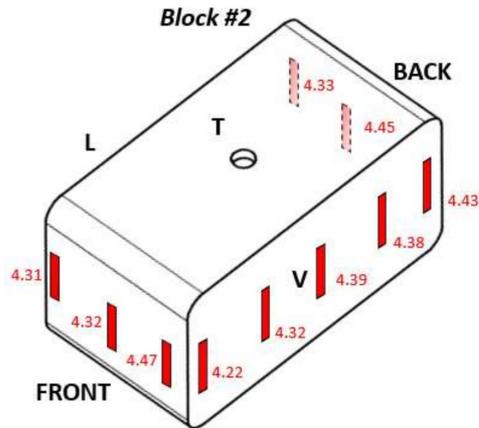
Ti-6Al-4V-clad Pb with Be plates



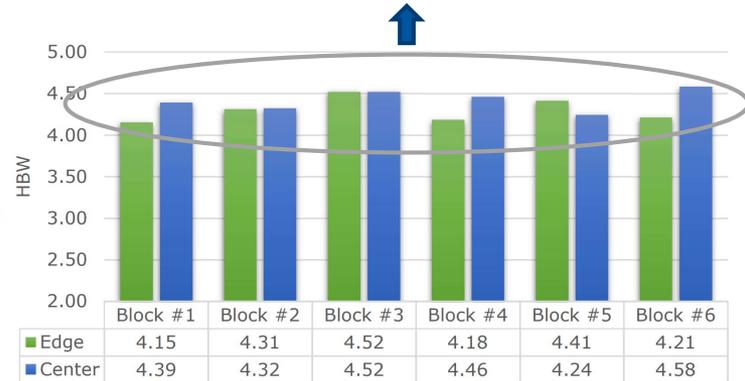
N₂-cooled Pb blocks



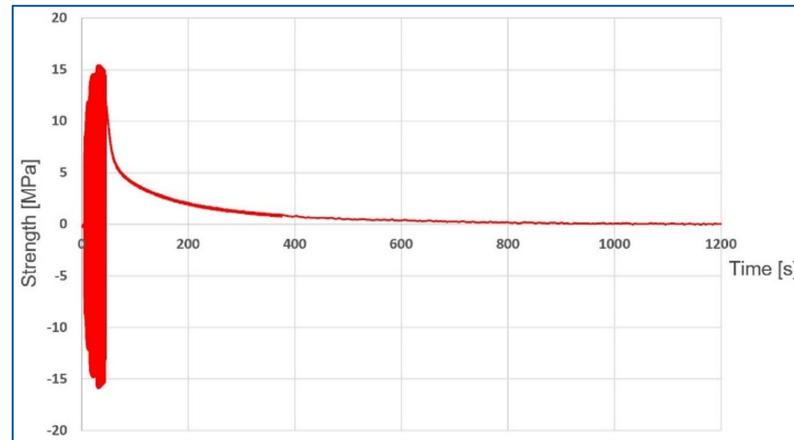
N₂-cooled Pb prototype hardness



Typical of unhardened material

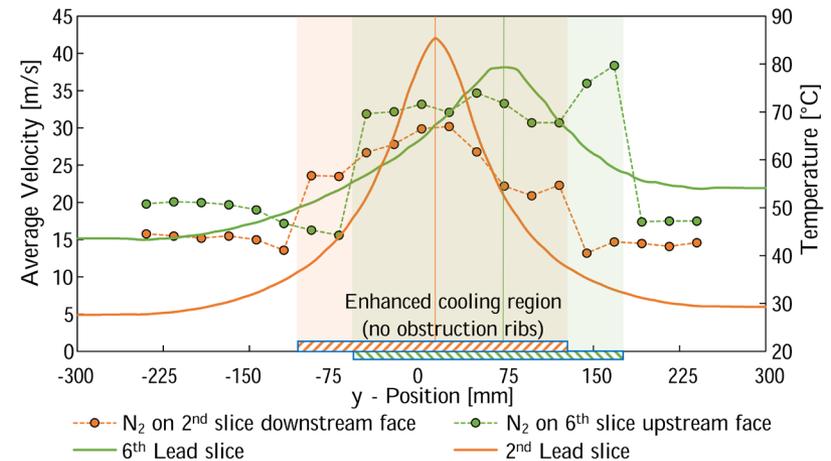
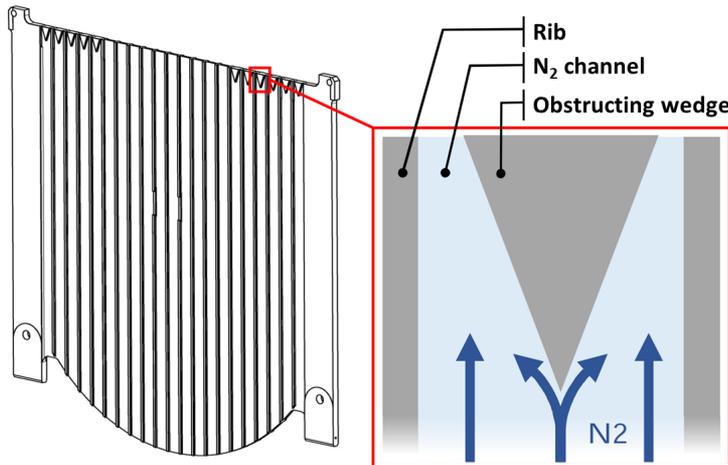


- Compatible with observations of stress relaxation tests
- Total recovery after ~10 min at RT



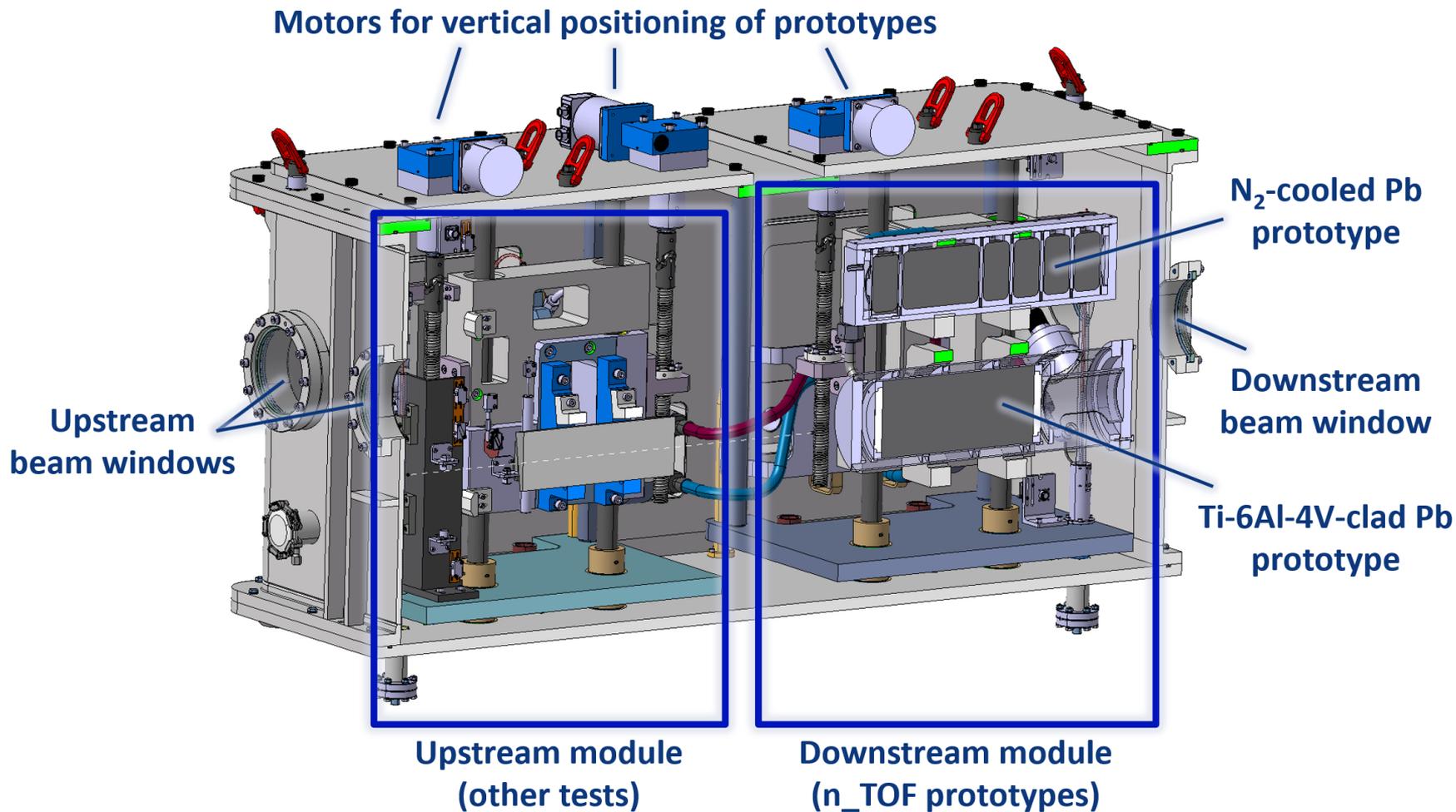
CFD and cooling optimization

Obstructing wedges to optimize N₂ flow distribution



Average HTC	63.8 W m ⁻² K ⁻¹
Peak HTC	130 W m ⁻² K ⁻¹

Beam irradiation tests



Beam irradiation tests

